VIRGINIA ELECTRIC AND POWER COMPANY RICHMOND, VIRGINIA 23261

January 26, 1993

United States Nuclear Regulatory Commission Attention: Document Control Desk Washington, D. C. 20555

Serial No. SPS/ETS

93-002

Docket Nos.

50-280

50-281

License Nos.

DPR-32 **DPR-37**

Gentlemen:

VIRGINIA ELECTRIC AND POWER COMPANY **SURRY POWER STATION UNITS 1 AND 2** SECOND TEN YEAR INSERVICE INSPECTION INTERVAL **RELIEF REQUESTS**

Surry Power Station Units 1 and 2 are currently in the third periods of their second ten year intervals. The test and inspection intervals are scheduled to end in October 1993 and May 1994 for Surry Units 1 and 2, respectively. The Code of reference for both units is the 1980 Edition, Winter 1980 Addendum of ASME Section XI. Several Code requirements have been identified as impractical and need to be addressed to close out the second interval test and inspection requirements. Thus, pursuant to 10 CFR 50.55a(g)(5), we are requesting relief from specific Code requirements for Surry Units 1 and 2. The basis for each relief request is provided in Attachment 1 of this letter.

As permitted by Paragraph IWA-2400(c) of the Code, Units 1 and 2 will be extending their inspection intervals by one year to complete remaining examinations. The required examinations will be completed in the 1994 refueling outage for both Units 1 and 2. The Unit 1 refueling outage is currently scheduled to begin in February 1994. Therefore, your review is requested by November 1, 1993 to allow scheduling of the appropriate inspection requirements for Unit 1.

These requests have been reviewed by the Station Nuclear Safety and Operating Committee.

If you have questions regarding this information, please contact us.

Very truly yours,

W. L. Stewart

Senior Vice President - Nuclear

Attachment

1. Unit 1 and 2 Relief Requests

7302020142 730

cc: U. S. Nuclear Regulatory Commission Region II 101 Marietta Street, N. W. Suite 2900 Atlanta, Georgia 30323

> Mr. M. W. Branch NRC Senior Resident Inspector Surry Power Station

Attachment 1

Surry Units 1 and 2 ISI Relief Requests

Surry Unit 1

I. Identification of Components

System: Reactor Coolant System

Components: Reactor Coolant Pump Casing internal surfaces

Component ·	<u> Item</u>	<u>Class</u>
1-RC-P-1A	Casing	1
1-RC-P-1B	Casing	1
1-RC-P-1C	Casing	1

(Drawings attached)

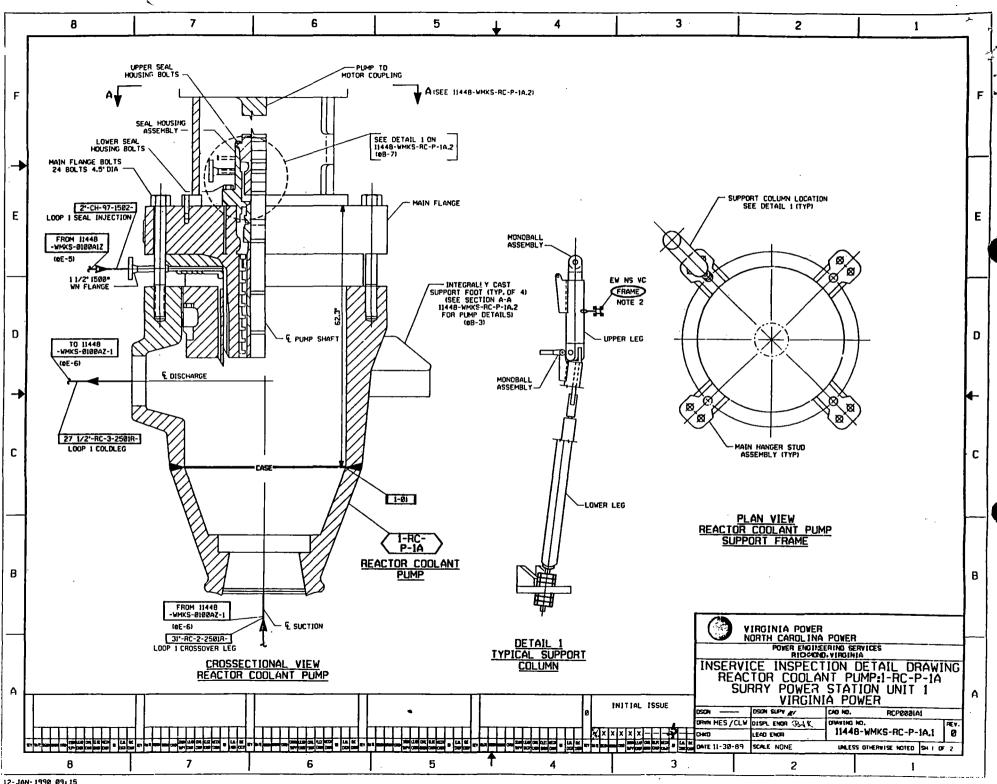
II. Impractical Code Requirements Category B-L-2, Pump Casings, Item number B12.20 requires a visual, VT-3, examination be conducted on the pump casing internal surfaces of one pump performing similar functions.

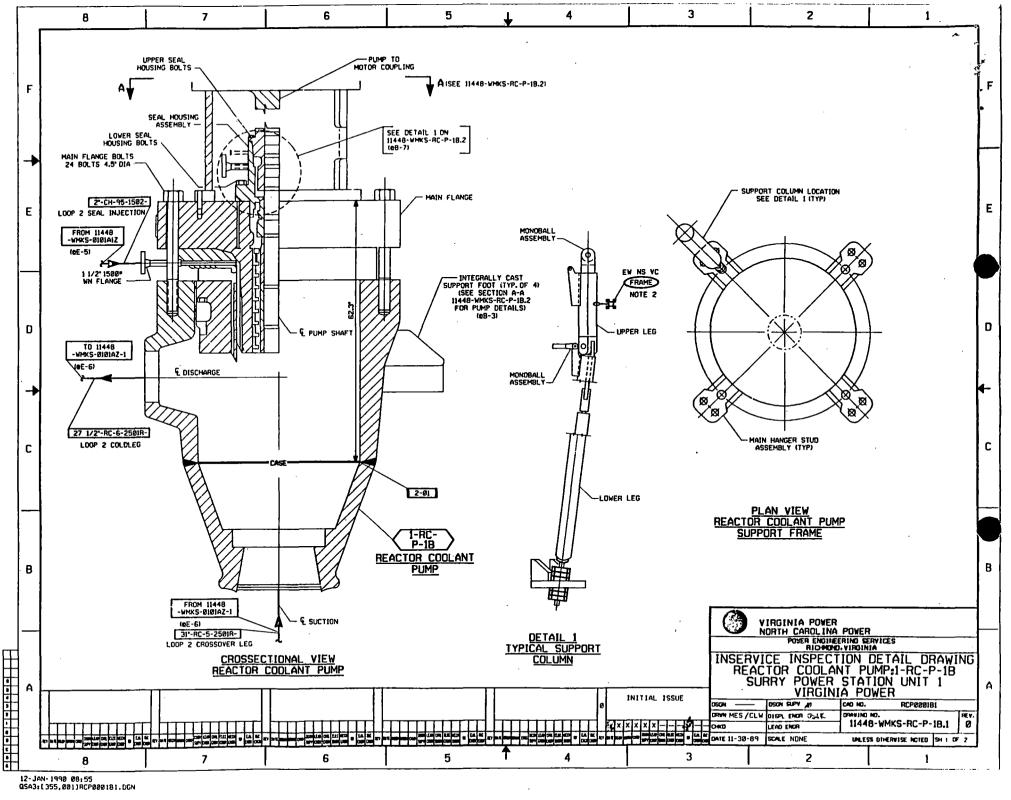
III. Basis For Relief

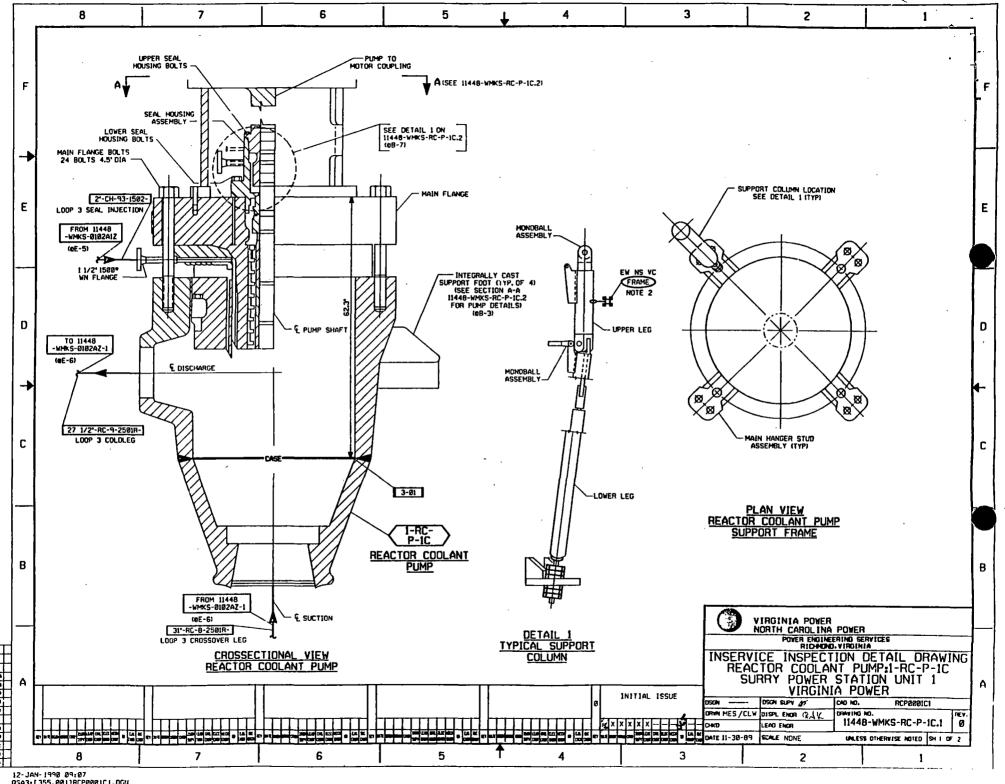
Performance of the Code required visual examination requires that the pump be disassembled to allow access to the pumps internal surfaces. Previously this examination was scheduled in conjunction with the Code required volumetric examination on the pump casing weld, which also required pump disassembly. Code Case N-481, Alternate Examination Requirements for Cast Austenitic Pump Casings Section XI, Division 1, will be used in lieu of the volumetric examination required by Table IWB 2500-1, Category B-L-1, Item B12.10. Requiring pump disassembly for the Code visual examination is impractical considering the cost and dose required to perform this action.

IV. Alternate requirements

A technical evaluation addressing the safety and serviceability of the pump casing has been performed and separately submitted to the NRC on October 26, 1992 (Serial#92-671) as required by Code Case N-481. The alternate inspection requirements will be implemented, which includes the performance of a VT-3 visual examination of the internal surfaces, whenever the pump is disassembled for maintenance. This requirement is similar to the provisions of the 1989 Edition of ASME Section XI in Table IWB-2500-1, Category B-L-2.







QSA3:[355.00]]RCP0001C].DGN

I. Identification of Components

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System: Reactor Coolant, Safety Injection, and Residual Heat Removal

Component: Class 1 valves greater than 4 inches in diameter (4 NPS)

- II. Impractical Code Requirements
 Table IWB-2500, Category B-M-2, item B12.40 requires that a
 visual, VT-3 examination be performed on the valves internal
 surfaces. As an alternative to this Code requirement we
 proposed, by previous relief request SR-001, that valves not
 disassembled for maintenance during the interval would have
 a ultrasonic (UT) wall thickness measurement performed in
 - proposed, by previous relief request SR-001, that valves not disassembled for maintenance during the interval would have a ultrasonic (UT) wall thickness measurement performed in lieu of the visual examination and valve disassembly. This relief request was approved by letter, serial# 91-189, dated March 14, 1991.
- III. Basis for Relief
 - The provision to perform an ultrasonic thickness examination on valves not disassembled for maintenance, in lieu of the required visual examination, was suggested by the NRC during initial discussions held concerning relief request SR-001. The extent and acceptance criteria of these alternative examinations were not discussed. Valves typically have an irregular interior and exterior surface by design. Correlating measurements with manufacturers drawings and then determining the acceptability of the measurement could only be described as "best effort." The meaningfulness of the examinations and the resultant exposure has called into question the practicality of performing these ultrasonic thickness examinations. The 1989 Edition of ASME Section XI has eliminated the requirement to disassemble valves for examination only. As such under the provisions of 10 CFR 50.55a(g)4(iv), we request the use of the 1989 Edition of ASME Section XI for examinations identified in Category B-M-2, item B12.50, for valve bodies exceeding NPS 4, and withdraw our previous relief request SR-001.
- IV. Alternate Requirements
 The 1989 Edition of ASME Section XI Category B-M-2, item
 B12.50 and corresponding notes 2 and 3 within the Category
 shall be followed. This will allow the visual examinations
 to coincide with valve disassembly required by maintenance,
 repair, or other required valve openings.

I. Identification of Components

Systems: Outside Recirculation Spray and Safety Injection Components: Pump casing welds identified below

Component	Weld	<u>Class</u>
1-RS-P-2A	2-01	2
1-RS-P-2A	2-02	2
1-RS-P-2A	2-03	2
1-RS-P-2A	2-04	2
1-RS-P-2B	2-01	2
1-RS-P-2B	2-02	2
1-RS-P-2B	2-03	2
1-RS-P-2B	2-04	2
1-SI-P-1A	2-01	2
1-SI-P-1A	2-02	2
1-SI-P-1A	2-03	2
1-SI-P-1A	2-04	2
1-SI-P-1B	2-01	2
1-SI-P-1B	2-02	2
1-SI-P-1B	2-03	. 2
1-SI-P-1B	. 2-04	2

(Drawings attached)

II. Impractical Code Requirements

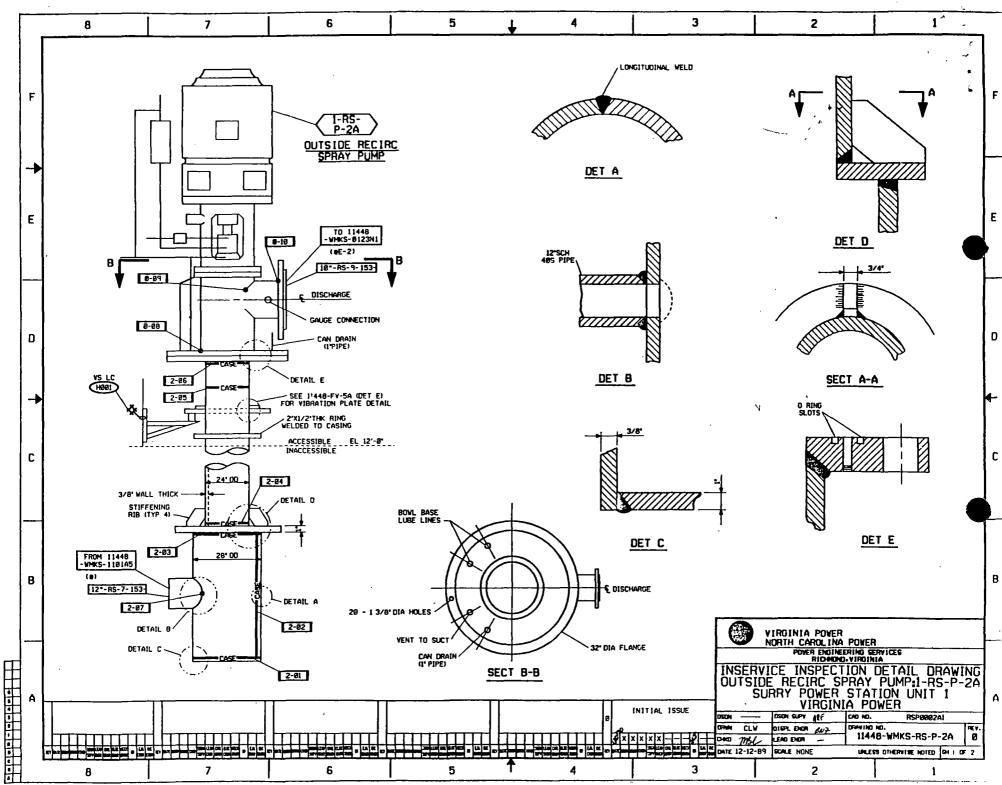
Category C-G, Item C6.10, Pump Casing Welds, requires that a surface examination be performed on 100% of the welds each interval. The examination can be limited to one pump in the case of multiple pumps of similar design, size, function, and service in a system.

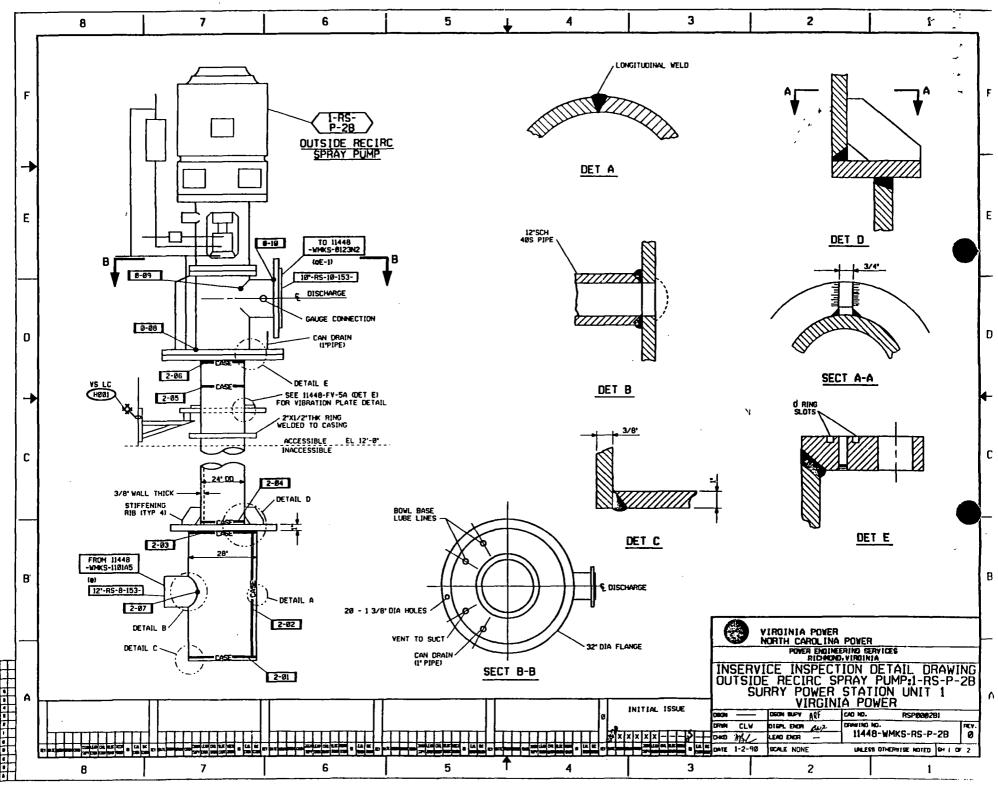
III. Basis For Relief

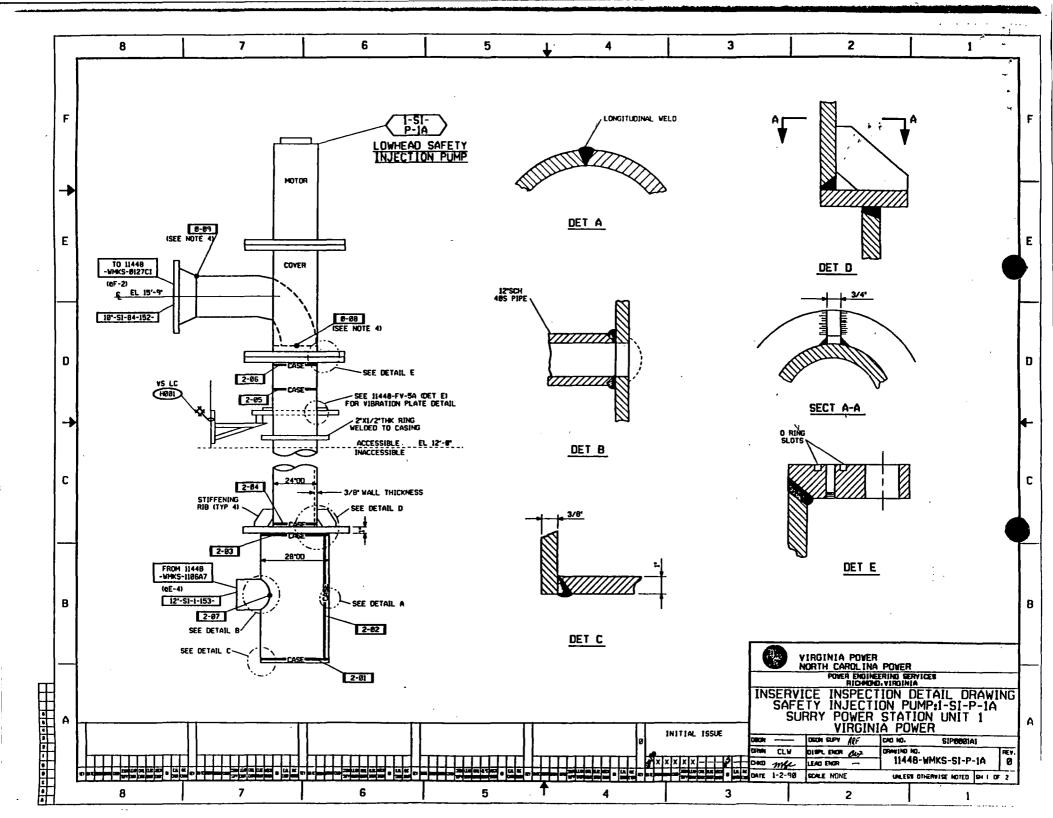
These pumps are vertical, two-stage, centrifugal pumps, with an extended shaft and casing to allow suction from the containment sump. The motor and mechanical seals of the pumps are located at about the 12 foot elevation and the bottom of the casing at about the -30 foot elevation. The welds identified are at the bottom of the pump casing, and are embedded within the concrete building structure. This makes the welds inaccessible from the outside. The small diameter of the casing (24 inch. O.D.) and the pump shaft prevent examination from the inside diameter.

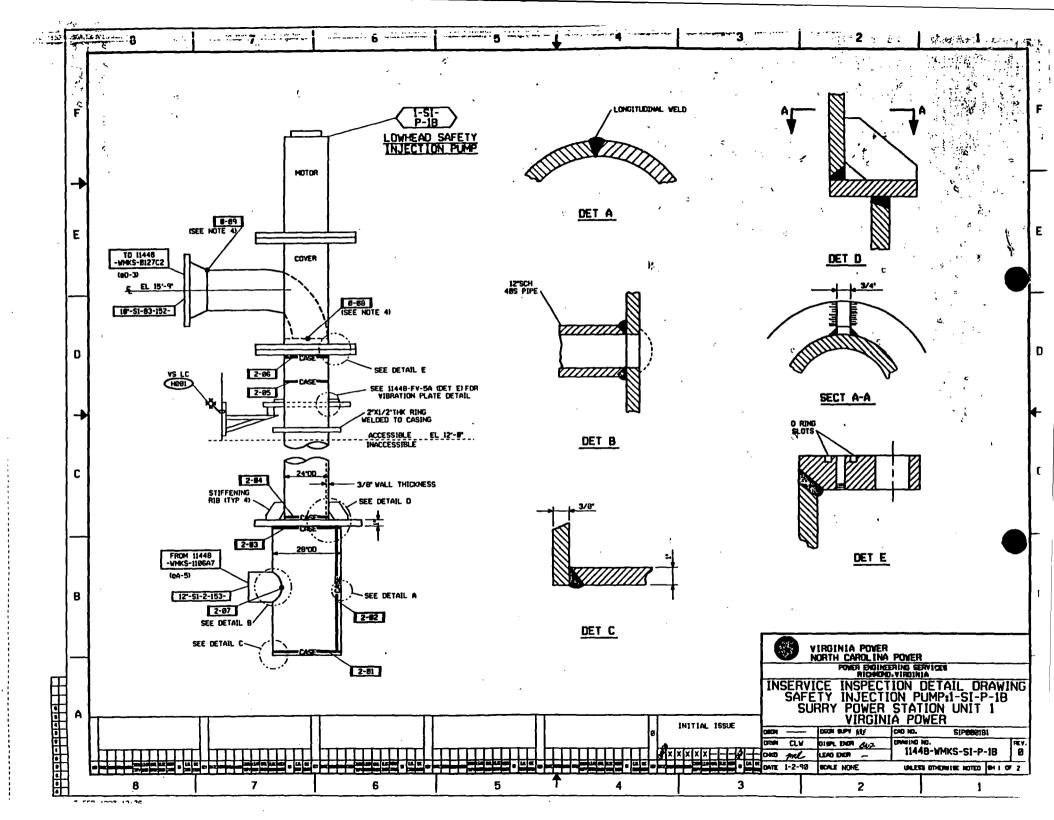
IV. Alternate Requirements

A remote visual examination (VT-1) of the accessible portions of the I.D. of the pump casing welds will be performed only if the pump is disassembled and the pump shaft removed for maintenance.









Relief Request 24

I. Identification of Components

System: Auxiliary Feedwater (AFW)

Component: Piping and components between the following

valves:

Valves	<u>Line</u>	<u>Valves</u>	Class
1-FW-145	1-WAPD-15-601	1-FW-149	3
•		1-FW-146	3
		1-FW-609	3
1-FW-160	1-WAPD-17-601	1-FW-164	3
		1-FW-161	3
		1-FW-608	3
1-FW-175	1-WAPD-20-601	1-FW-179	3
		1-FW-176	3
		1-FW-607	3

(Drawing Attached)

II. Impractical Code Requirements

ISI Class 3 System Hydrostatic Test required in IWD-5223 of ASME Section XI, where design pressure is 1432 psig and the resultant test pressure is 1576 psig.

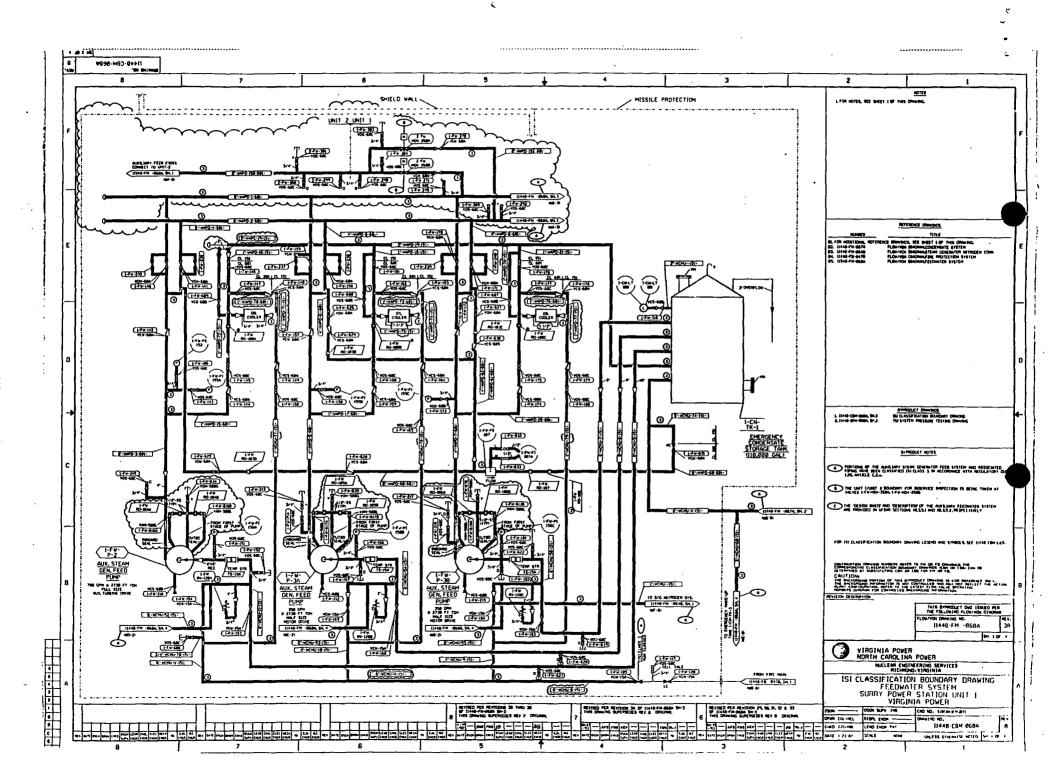
III. Basis For Relief

Three pressure reducing orifices 1-FW-RO-100A, 1-FW-RO-100B, and 1-FW-RO-100C provide during normal operation a pressure drop from approximately 1200 psig to 110 psig. The system design takes advantage of this pressure drop by incorporating lower pressure rated piping downstream of the orifices. However the higher pressure rated piping continues beyond the orifices for some distance. The actual pipe design pressure class change occurs at downstream check valves 1-FW-148, 1-FW-163, and 1-FW-178 and manual valves, 1-FW-146, 1-FW-161, and 1-FW-176. The check valve operation, however, does not allow separation of the lower pressure class system, when testing the higher class piping in accordance with IWD-5223. IWD-5223 would require a test pressure of 1576 psig on the higher pressure class components in question. The downstream connecting piping has a design pressure of 150 psig and a corresponding test pressure of only 165 psig. As such, the connecting components would be overpressurized during the required Section XI test. The test boundary could be backed up to manual isolation valves 1-FW-147, 1-FW-162, and 1-FW-177, however hydrostatically testing this test boundary would also pressurize the auxiliary feedwater pumps and their suction connection. These pumps have welded discharge connections and cannot be isolated from the test boundary due to the absence of a drain or vent valve in the area

identified above. There is a flange connection on the suction side of each pump, however using this flange for isolation purposes is considered difficult due to the piping arrangement, and susceptibility to cold spring misalignment problems. Typically centrifugal pumps are hydrostatically tested at a pressure based on the suction side of the pump as described in IWA-5224(d) of the Code, which prevents any potential overpressurization concerns, or the need to use pump flanges as isolation points. The basis for relief then is two-fold. The first impracticality is the overpressurization of piping and components downstream of the pressure reducing orifice and the design pressure class rating change. The second impracticality is the incorporation of the auxiliary feedwater pumps into the test boundary due to the lack of vent, drain, and manual isolation valves.

IV. Alternate Testing

The identified components will be tested in accordance with IWD-5222, Functional test requirements, in conjunction with the associated auxiliary feedwater pump at normal operating pressure.



Relief Request 25

I. Identification of Components

System: Circulating and Service Water

Component: Piping and components between the following

valves:

<u>Valves</u>	<u>Line#/Component</u>	<u>Valves</u>	<u>Class</u>
1-SW-499	8"-WS-480-21X/	1-SW-311/	3
and	6"-WS-483-21X/	1-SW-321/	3
2-SW-476	6"-WS-484-21X	2-SW-331	3
1-SW-317/	1-VS-S-1A	1-SW-346	3
1-SW-327/	and	and	
2-SW-337	1-VS-S-1B	2-SW-344	3

(Drawing Attached)

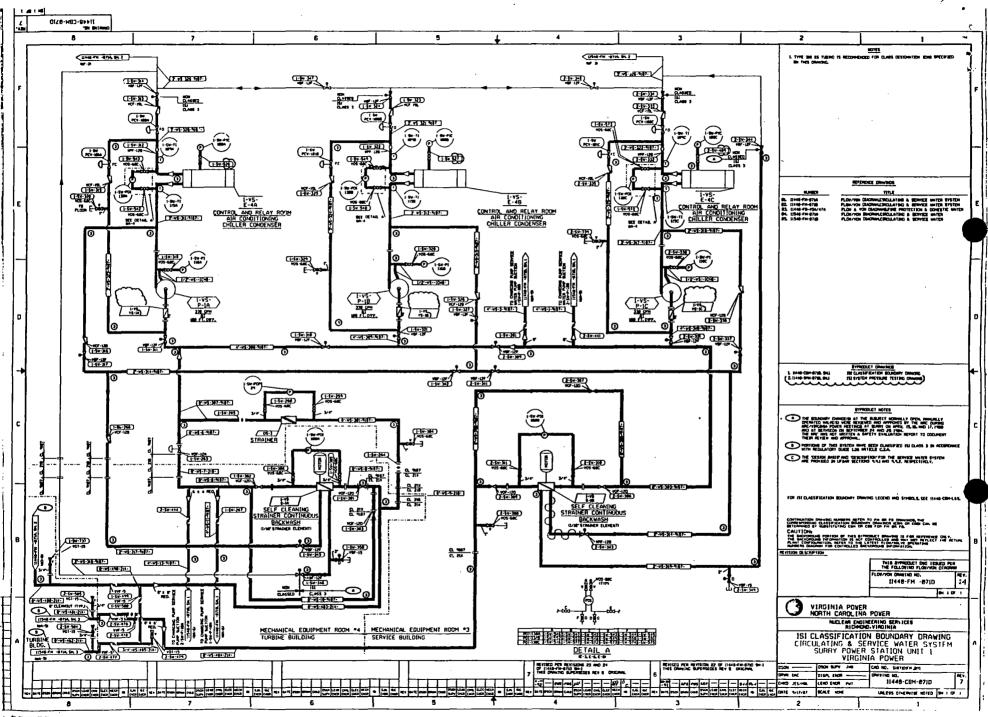
II. Impractical Code Requirements
ISI Class 3 System Hydrostatic test required by IWD-5223 of
ASME Section XI, where the design pressure is listed as 50
psig and test pressure is 55 psig.

III. Basis For Relief

Technical Specifications 3.14C requires, "There shall be an operating service water flow path to and from one operating main control and emergency switchgear rooms air conditioning condenser and at least one operable service water flow path to and from at least one operable main control and emergency switchgear rooms air conditioning condenser whenever fuel is loaded in reactor core." By design there are only two supply headers and strainers associated with this common unit air conditioning system. This Specification requires that the components identified always be operating or operable, while either of our two units have fuel in the reactor core. A technical Specification change was submitted September 4, 1992 (Serial No. 92-579), to provide a 24 hour action statement for the service water headers. If this is approved, routine maintenance could be performed within the action statement guidelines. However, challenging the proposed action statement with a hydrostatic test (ten-year or post maintenance) is seen as excessive, potentially forcing a dual unit outage should problems occur, and impractical when compared to the proposed alternative in this low pressure system.

IV. Alternate Testing

The lines and components in question are gravity fed from the in-take canal from lines providing water to both units main condensers. In lieu of the Code required hydrostatic test it is requested that a system inservice test, IWD-5221 be performed in conjunction with a visual (VT-2) examination of the accessible areas.



84-AM-1412 84:21 203-1300, 11115187101FH, 871

Relief Request 26

I. Identification of Components

System: Circulating and Service Water

Component: Piping and components between the following

valves:

<u>Valves</u>	<u>Lines</u>	<u>Valves</u>		<u>Class</u>
1-SW-MOV-102A	42"-WS-13-10	1-SW-37		3
and	and	1-SW-33	•	3
1-SW-MOV-102B	42"-WS-12-10	1-SW-29		3
		1-SW-25		3

(Drawing Attached)

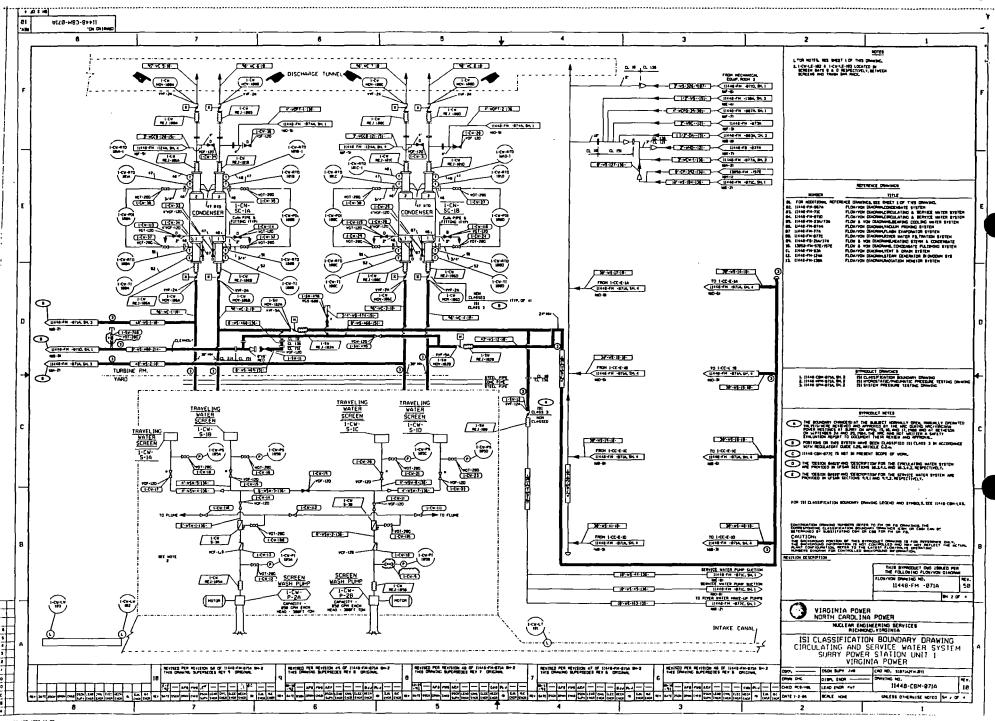
II. Impractical Code Requirements
ISI Class 3 System Hydrostatic Test as required by IWD-5223
of ASME Section XI, where the design pressure is 25 psig and
the corresponding test pressure is 28 psig.

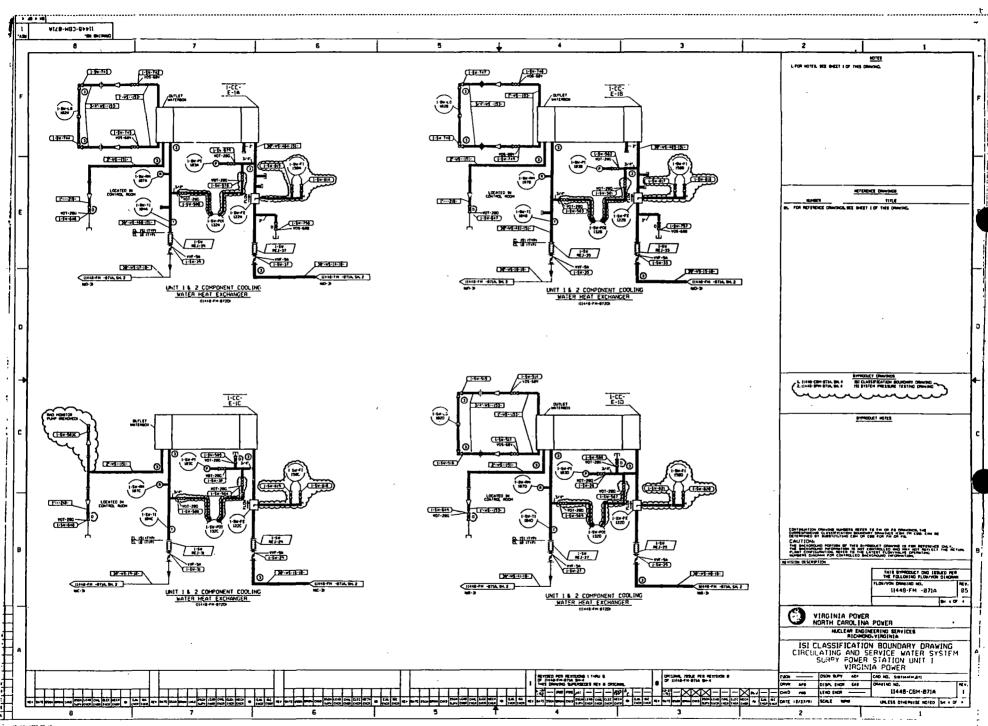
III. Basis For Relief

Technical Specification 3.14 requires service water flow to and from the component cooling water heat exchangers. One unit operation requires two component cooling water heat exchangers, while two unit operation requires three component cooling water heat exchangers. Additionally Technical Specifications 3.5 and 3.10 provide requirements associated with component cooling operability for core residual heat removal in both unit operation and refueling modes. The identified supply header to the component cooling water heat exchangers is the only source of cooling water to these components. Conducting the Code required hydrostatic test would require isolation of all four component cooling water heat exchangers, placing the unit(s) in conflict with Technical Specifications as previously discussed.

IV. Alternate Testing

The lines and components identified are gravity fed from the in-take canal from lines providing water to the main condensers. As an alternative, a system inservice test to the requirements of IWD-5221 and the corresponding visual (VT-2) examination of the accessible areas will be conducted in lieu of the Code hydrostatic test.





16-70-1992 88-16 20512 258, 11125187144FH, 812

Relief Request 27

I. Identification of Components

System: Main Steam, Auxiliary Feedwater, and Feedwater

Components: Piping and valves listed:

Component	<u>Mark#</u>	<u>Line#</u>	S/G	<u>Class</u>
Valve	1-MS-86	4"-SHP-37-601	A	2
Valve	1-MS-119	4"-SHP-38-601	В	2
Valve	1-MS-117	6"-SHP-46-601	В	2
Valve	1-MS-157	4"-SHP-39-601	С	2
Pipe	-	14"-WFPD-9-601	С	2
Valve	1-FW-92	3"-WAPD-13-601	С	2

(Drawings attached)

II. Impractical Code Requirements
Surry Unit 1 utilized Code Case N-416, Alternate Rules for
Hydrostatic Testing of Repair or Replacement of Class 2
Piping Section XI, Division 1, on the components identified
above. This Code Case defers the hydrostatic test required
by IWA-4400 of ASME Section XI until the next regularly
scheduled system hydrostatic test (IWC-5000) for that
system.

III. Basis of Relief

The identified components were replaced under the rules of ASME Section XI. IWA-4400 of the Code requires that a hydrostatic test be conducted on certain welded repairs or replacements. These replacements cannot be hydrostatically tested without also hydrostatically testing the connecting steam generator, as no intermediate isolation exists. Valve 1-MS-117 appears to have intermediate isolation, however the main steam trip valve, 1-MS-TV-101B, acts like a check valve, and would open during pressurization to the steam generator.

Prior to NRC and Code approval of Code Case N-416, relief requests were routinely written and approved for these type situations. The relief requests were based upon the difficulties associated with steam generator hydrostatic testing. The test cannot be conducted at ambient conditions due to fracture prevention concerns associated with the Surry steam generators. The Surry steam generators are required to be a minimum of 150 degrees F. on the secondary side and a minimum of 180 degrees F. on the primary side, which results in difficult monitoring and controlling requirements. Additionally normal problems, such as test boundary isolation, internal boundary leakage, placing spring hanger stops for dead weight loading concerns, and test pump size requirements further increase the difficulties associated with this particular test. The test

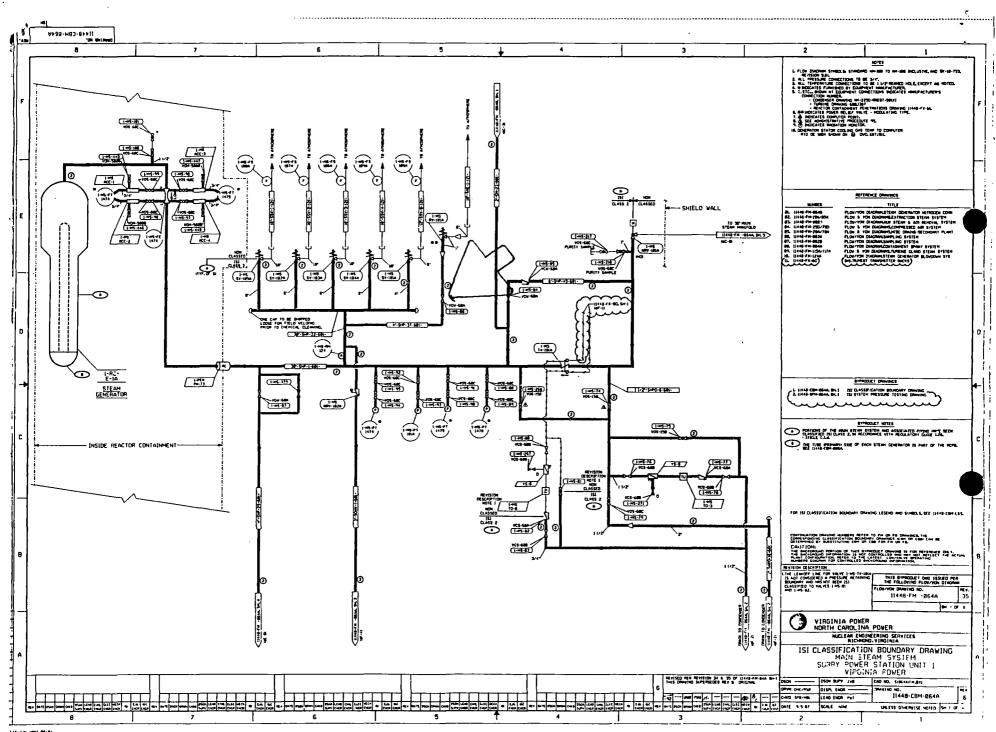
pressure of 1356 psig also requires gaging or removal of the Main Steam Safety valves, which initially lift at 1085 psig. Some examples of previous correspondence requesting relief and approval follow:

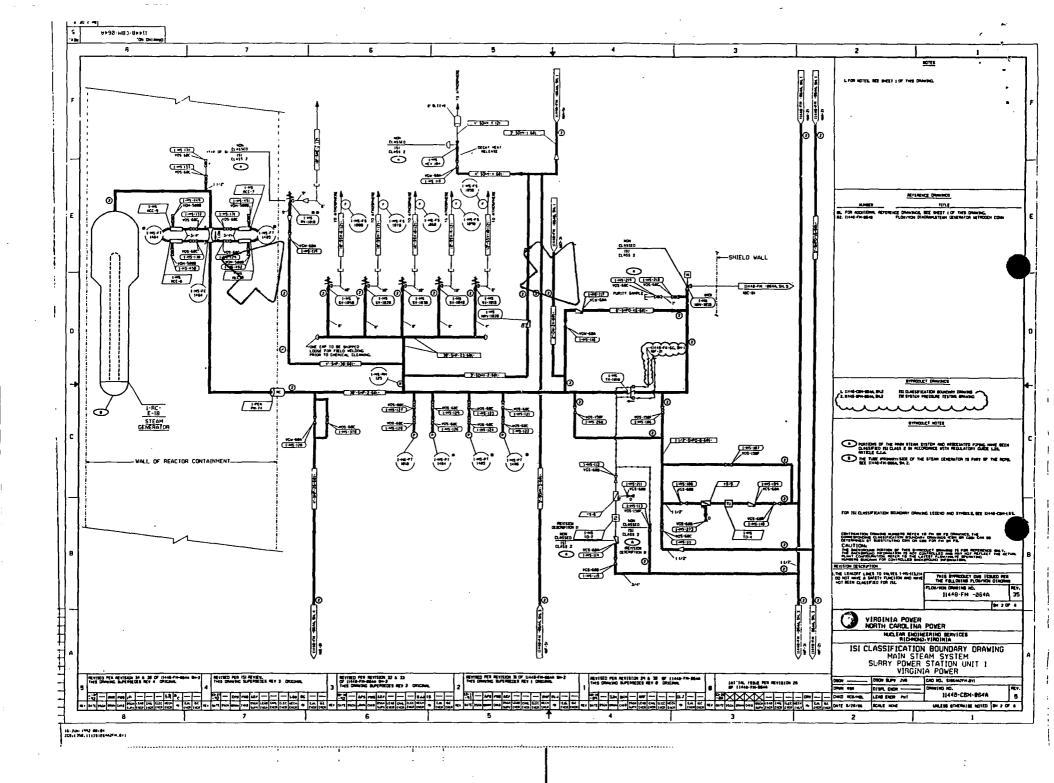
<u>VEPCO Letter/ Date</u>	NRC Letter/ Date
Serial# 90-504/ 9/10/90	Serial# 92-474/7/14/92
Serial# 88-725/ 1/9/89	Serial# 89-278/4/7/89
Serial# 87-630/ 10/6/87	Serial# 88-473/7/8/88

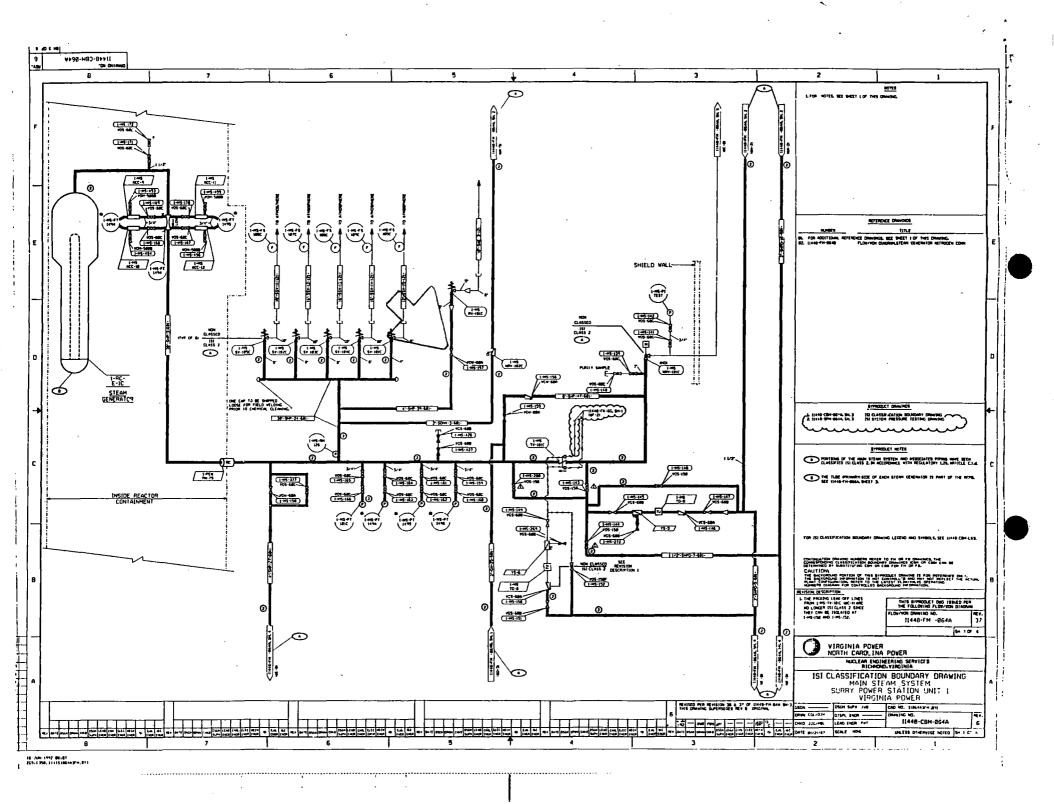
When Code Case N-416 was incorporated into Regulatory guide 1.147, "Inservice Inspection Code Case Acceptability-ASME Section XI Division 1, relief requests were no longer needed, since the hydrostatic test was deferred to the end of the interval hydrostatic test described in table IWC-2500-1. This appeared to be the minimum hydrostatic testing that could be achieved for the steam generators. Recently in Revision 9 of Regulatory Guide 1.147, you approved Code Case N-498, Alternative Rules for 10-Year Hydrostatic Pressure Testing for Class 1 and 2 Systems Section XI, Division 1. This Code Case allows testing of the class 2 steam generators at nominal operating pressure. As a result, no hydrostatic test is now required by ASME Section XI on these components under normal circumstances, when incorporating Code Case N-498. The hydrostatic test of Code Case N-416 is still required to be performed, however. As described before, the components identified above can only be hydrostatically tested by additionally testing the connecting steam generator. Requiring a full steam generator test only for these replacement activities is considered impractical, due to the difficulties of the test described previously.

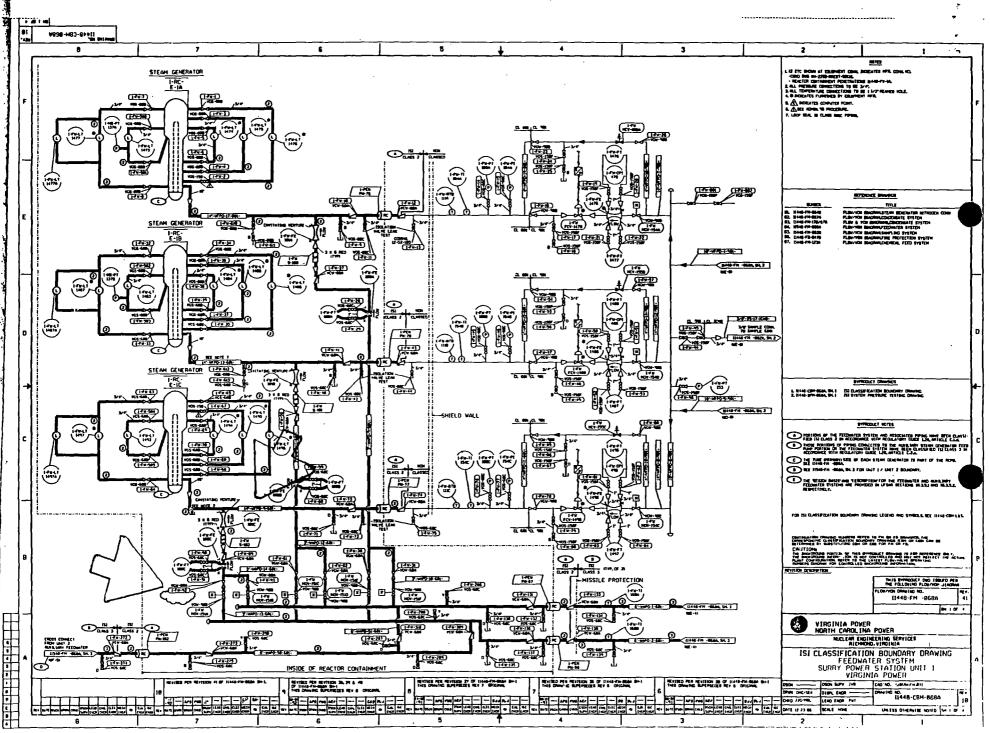
IV. Alternate testing

The alternative requirements described in Code Case N-416, a volumetric examination of the full penetration welds and a visual examination (VT-2) at nominal operating pressure was previously performed and deemed acceptable.









Surry Unit 2

I. Identification of Components

System: Reactor Coolant System

Components: Reactor Coolant Pump Casing internal surfaces

Component	<u>Item</u>	<u>Class</u>
2-RC-P-1A	Casing	1
2-RC-P-1B	Casing	1
2-RC-P-1C	Casing	1

(Drawings attached)

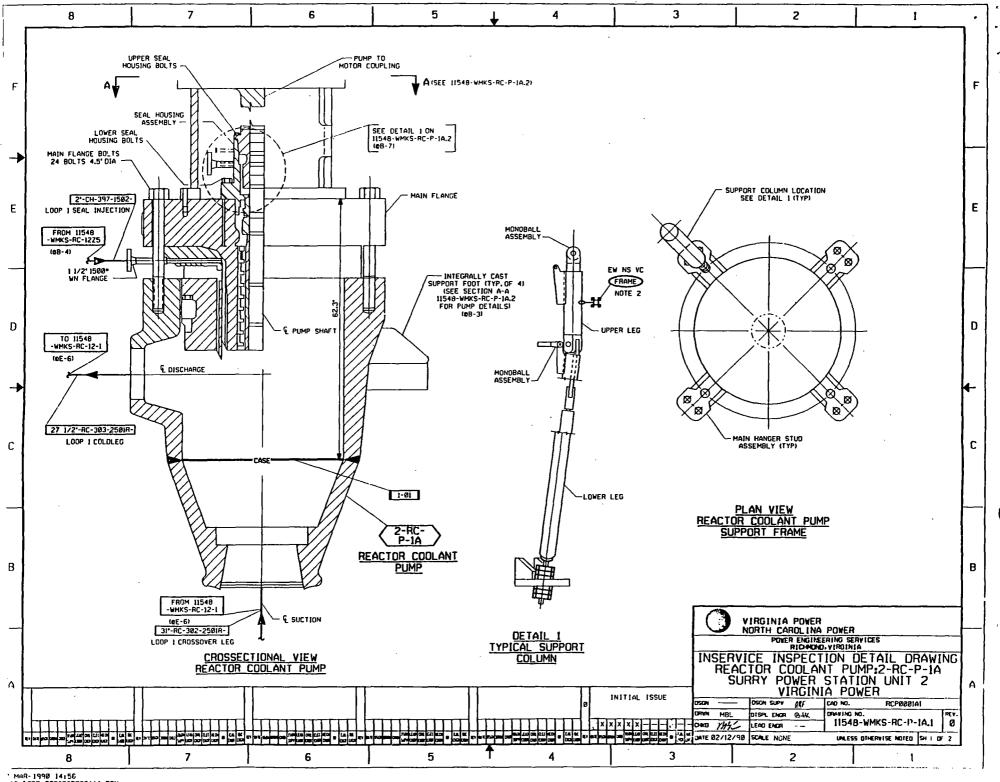
II. Impractical Code Requirements Category B-L-2, Pump Casings, Item number B12.20 requires a visual, VT-3, examination be conducted on the pump casing internal surfaces of one pump performing similar functions.

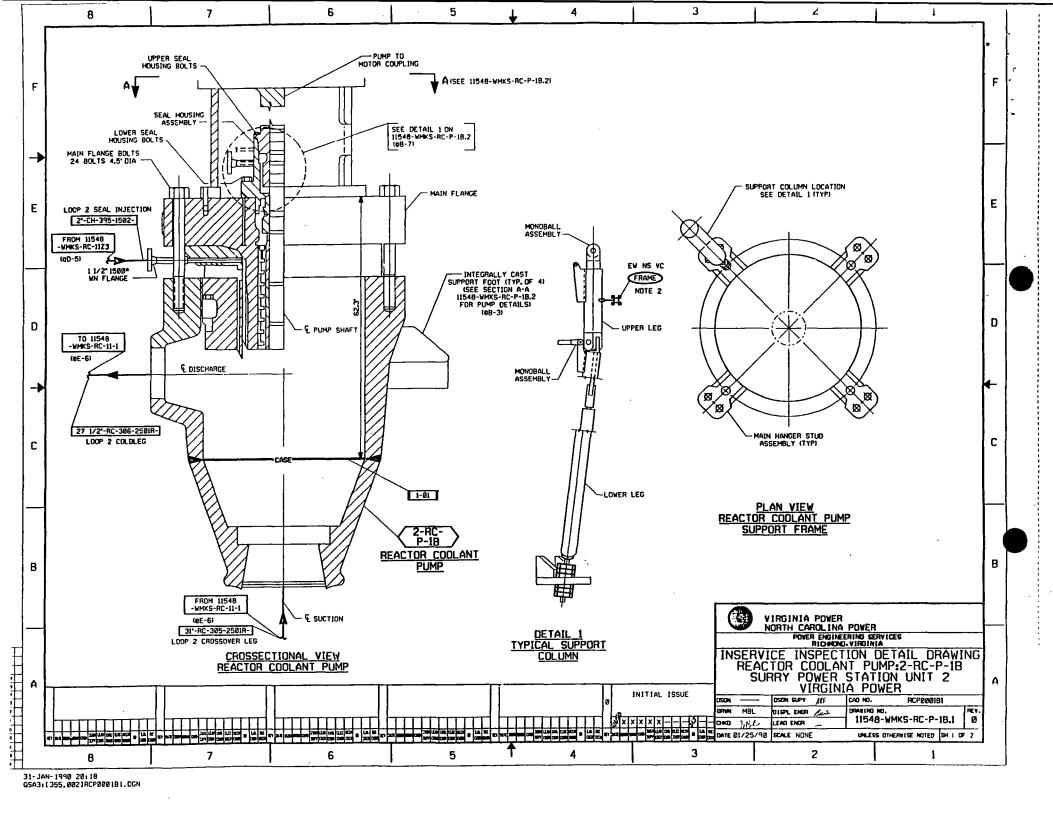
III. Basis For Relief

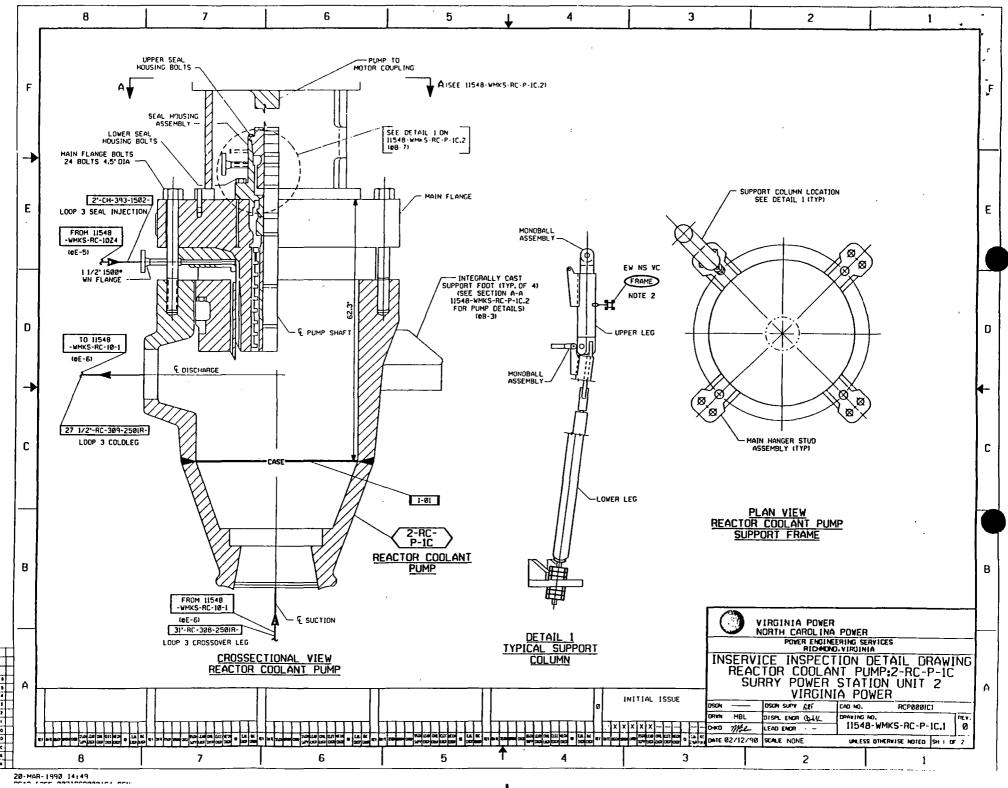
Performance of the Code required visual examination requires that the pump be disassembled to allow access to the pumps internal surfaces. Previously this examination was scheduled in conjunction with the Code required volumetric examination on the pump casing weld, which also required pump disassembly. Code Case N-481, Alternate Examination Requirements for Cast Austenitic Pump Casings Section XI, Division 1, will be used in lieu of the volumetric examination required by Table IWB 2500-1, Category B-L-1, Item B12.10. Requiring pump disassembly for the Code visual examination is impractical considering the cost and dose required to perform this action.

IV. Alternate requirements

A technical evaluation addressing the safety and serviceability of the pump casing has been performed and separately submitted to the NRC on October 26, 1992 (Serial#92-671) as required by Code Case N-481. The alternate inspection requirements will be implemented, which includes the performance of a VT-3 visual examination of the internal surfaces, whenever the pump is disassembled for maintenance. This inspection is similar to the provisions of the 1989 Edition of ASME Section XI in Table IWB-2500-1, Category B-L-2.







- I. Identification of Components
 - System: Reactor Coolant, Safety Injection, and Residual Heat Removal

Component: Class 1 valves greater than 4 inches in diameter (4 NPS)

- II. Impractical Code Requirements
 - Table IWB-2500, Category B-M-2, item B12.40 requires that a visual, VT-3 examination be performed on the valves internal surfaces. As an alternative to this Code requirement we proposed, by previous relief request SR-001, that valves not disassembled for maintenance during the interval would have a ultrasonic (UT) wall thickness measurement performed in lieu of the visual examination and valve disassembly. This relief request was approved by letter, serial# 91-189, dated March 14, 1991.
- III. Basis for Relief
 - The provision to perform an ultrasonic thickness examination on valves not disassembled for maintenance, in lieu of the required visual examination, was suggested by the NRC during initial discussions held concerning relief request SR-001. The extent and acceptance criteria of these alternative examinations were not discussed. Valves typically have an irregular interior and exterior surface by design. Correlating measurements with manufacturers drawings and then determining the acceptability of the measurement could only be described as "best effort." The meaningfulness of the examinations and the resultant exposure has called into question the practicality of performing these ultrasonic thickness examination. The 1989 Edition of ASME Section XI has eliminated the requirement to disassemble valves for examination only. As such under the provisions of 10 CFR 50.55a(g)4(iv), we request the use of the 1989 Edition of ASME Section XI for examinations identified in Category B-M-2, item B12.50, for valve bodies exceeding NPS 4, and withdraw our previous relief request SR-001.
- IV. Alternate Requirements
 The 1989 Edition of ASME Section XI Category B-M-2, item
 B12.50 and corresponding notes 2 and 3 within the Category
 shall be followed. This will allow the visual examinations
 to coincide with valve disassembly required by maintenance,
 repair, or other required valve openings.

I. Identification of Components

System: Chemical and Volume Control (CH)

Component: Regenerative Heat Exchanger (2-CH-E-3)

Welds/Components	<u>Description</u>	<u>Class</u>
1-06	nozzle-to-vessel	1
NIR-06	nozzle inside radius	1
1-08	nozzle-to-vessel	1
NIR-08	nozzle inside radius	1
1-09	nozzle-to-vessel	1
NIR-09	nozzle inside radius	1
1-11	nozzle-to-vessel	1
NIR-11	nozzle inside radius	1
1-13	nozzle-to-vessel	. 1
NIR-13	nozzle inside radius	1
1-15	nozzle-to-vessel	1
NIR-15	nozzle inside radius	1

II. Impractical Code Requirements Examination Category B-D (Inspection Program B) requires in item numbers B3.150 and B3.160 a volumetric examination of the nozzle-to-vessel weld and nozzle inside radius section.

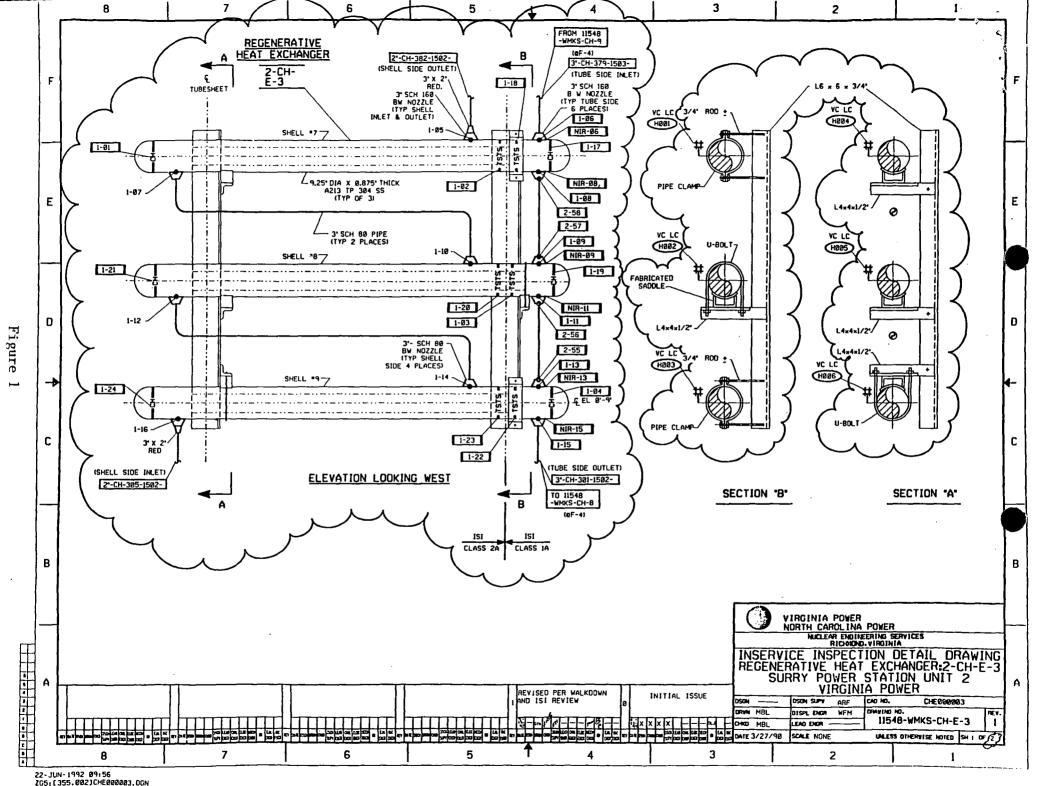
III. Basis For Relief

The joint design of the above nozzle welds specifies a 3" schedule 160 weldolet joined to a 9.25" O.D. X .875" thick vessel. These welds were not designed to be volumetrically examined from the outside diameter. The configuration of the weldolet precludes axial ultrasonic examination from the nozzle side and circumferential examination in either direction. This limits volumetric examination to a single axial scan from the vessel side of the nozzle. It is our opinion that a meaningful ultrasonic examination cannot be performed on the weld or inner radius with a single axial scan from the vessel side. This is due to the small diameter of the vessel and weldolet, the change in dihedral around the joint results in a corresponding change in the ultrasonic beam angle. This makes position measurements unreliable. It would also be necessary to extend the beam path to at least two full Vee paths, which will further complicate this examination. These limitations would substantially limit our ability to discriminate flaw indications from geometry existing around the joint. configuration also precludes placement of film on the outside diameter for radiography, and the inside surfaces are inaccessible. It is our opinion that the gain in assurance of component integrity from this limited examination is not commensurate with the anticipated dose expenditure. Figures 1,2,3, and 4 are provided to support

this request.

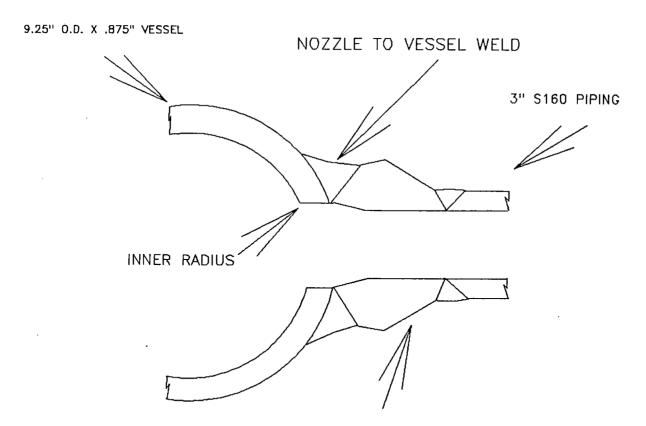
IV. Alternate Requirements

The outside surface of the nozzle-to-vessel welds shall receive a surface (liquid penetrant) examination. In addition a visual (VT-2) examination shall be performed in conjunction with the pressure testing required by IWB-5000.



SR-018 FIGURE 2

TYPICAL NOZZLE TO HT. XCHANGER WELD



10" x 3" S160 WELDOLET

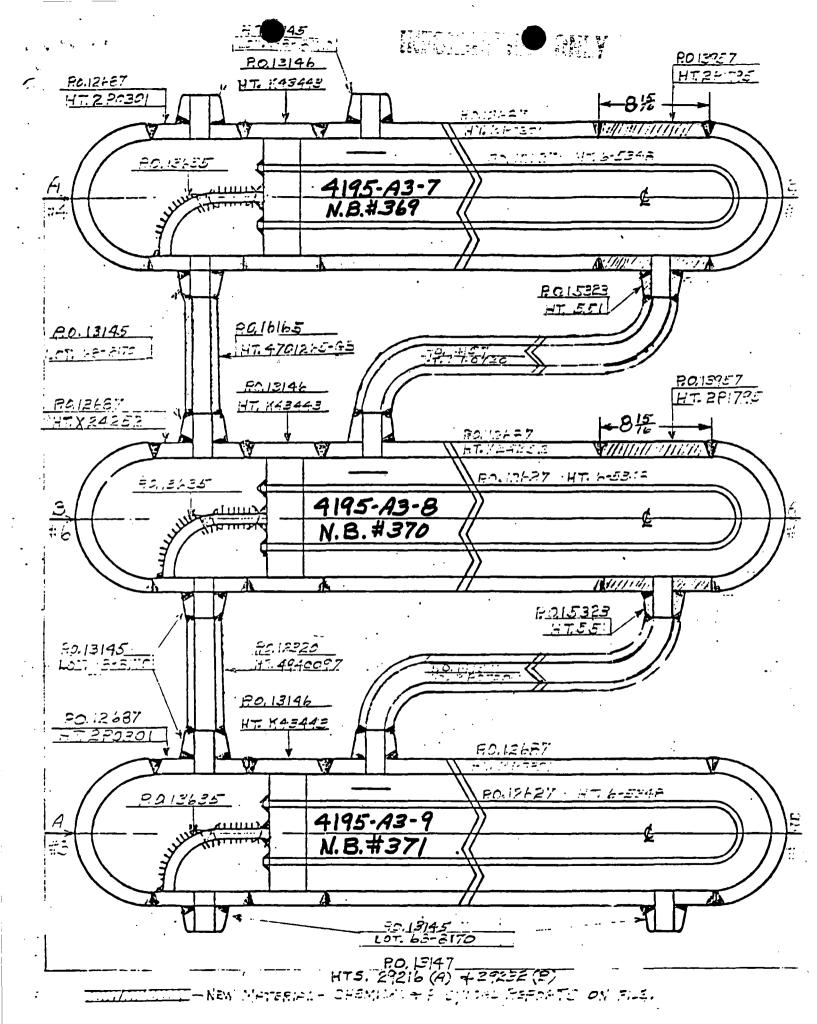


Figure 3

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Tormey 2000# Welkolot (for outt Welding) 10 x 3° for Schwinle LóO Pipe SA 1827 304 52.00

(4 copies chemical and physical test reports required)

Required 5/6/68 - TAG: A3 #4

Required 6/15/58 (not before) TAG: 13 #5

Required 7/8/62 (not before) TAG: 14 #2

Confirming phone order to May Mosor
DO NOT DUPLICATE

TAG: 8/c 554 A04195

Relief Request SR-019

I. Identification of Components

Systems: Outside Recirculation Spray and Safety Injection Components: Pump casing welds identified below

Component 2-RS-P-2A 2-RS-P-2A 2-RS-P-2A	<u>Weld</u> 2-01 2-02 2-03	<u>Class</u> 2 2 2
2-RS-P-2A	2-04	2
2-RS-P-2B	2-01	2
2-RS-P-2B	2-02	2
2-RS-P-2B	2-03	2
2-RS-P-2B	2-04	2
2-SI-P-1A	2-01	2
2-SI-P-1A	2-02	2
2-SI-P-1A	2-03	. 2
2-SI-P-1A	2-04	. 2
2-SI-P-1B	2-01	2
2-SI-P-1B	2-02	2 .
2-SI-P-1B	2-03	2 -
2-SI-P-1B	2-04	2

(Drawings attached)

II. Impractical Code Requirements

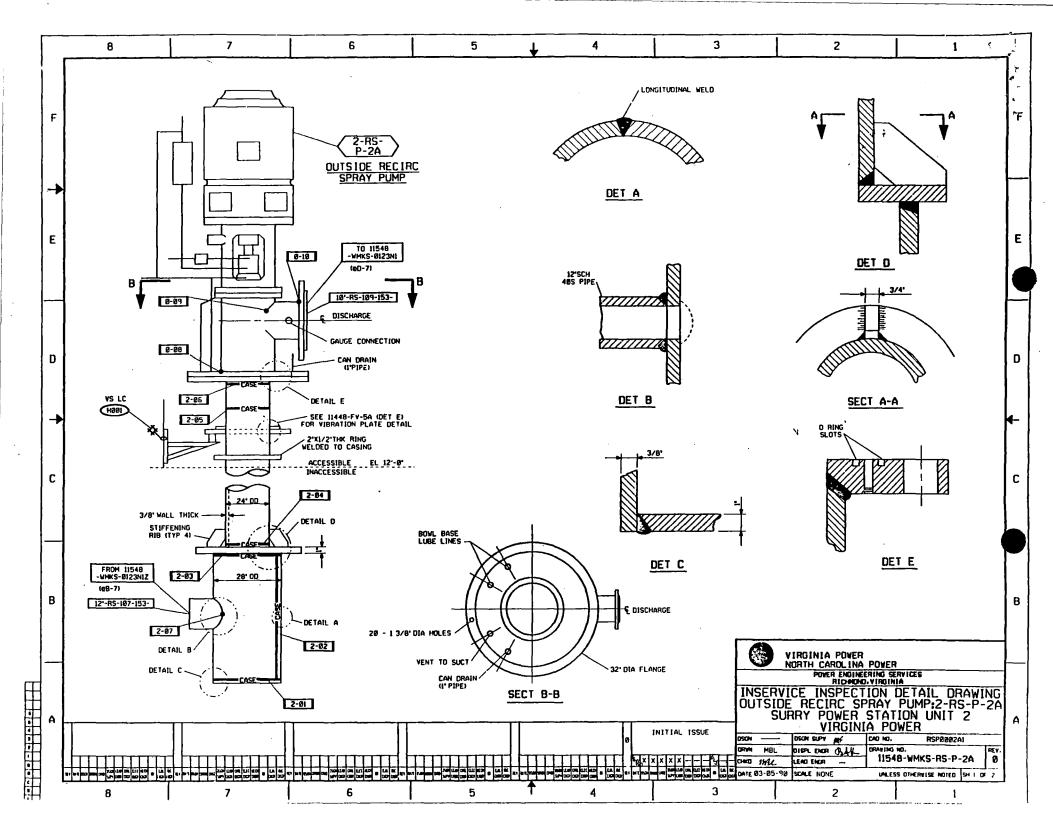
Category C-G, Item C6.10, Pump Casing Welds, requires that a surface examination be performed on 100% of the welds each interval. The examination can be limited to one pump in the case of multiple pumps of similar design, size, function, and service in a system.

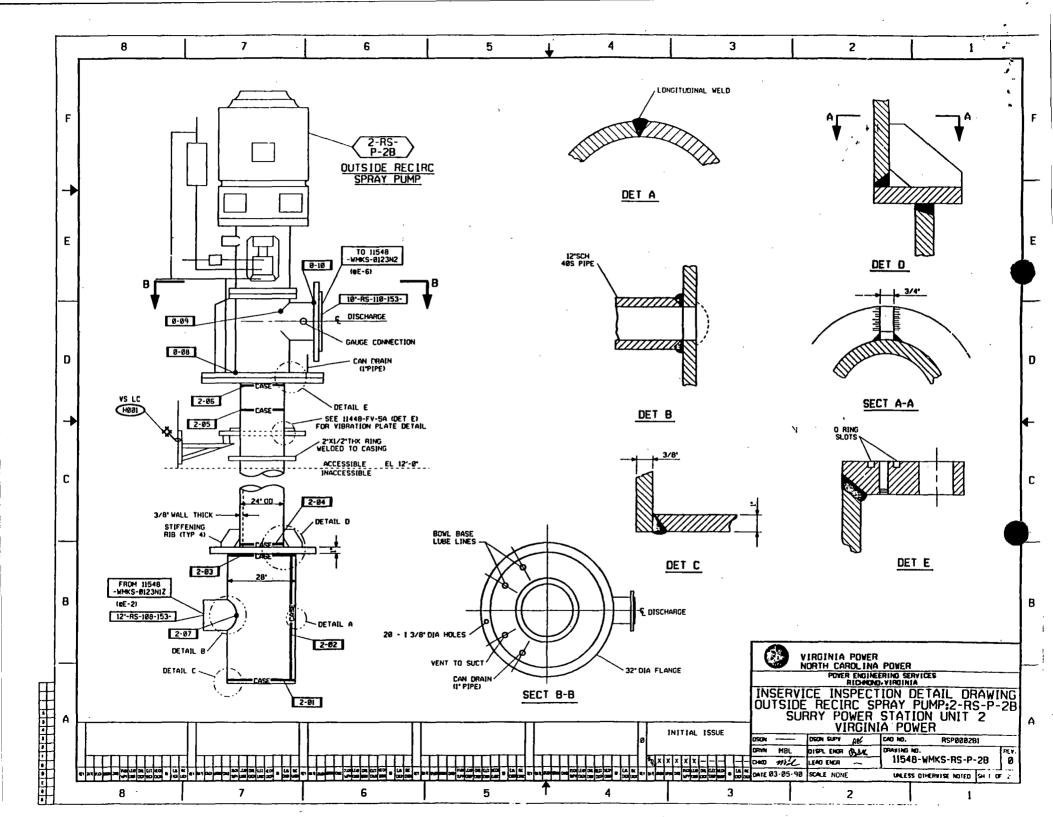
III. Basis For Relief

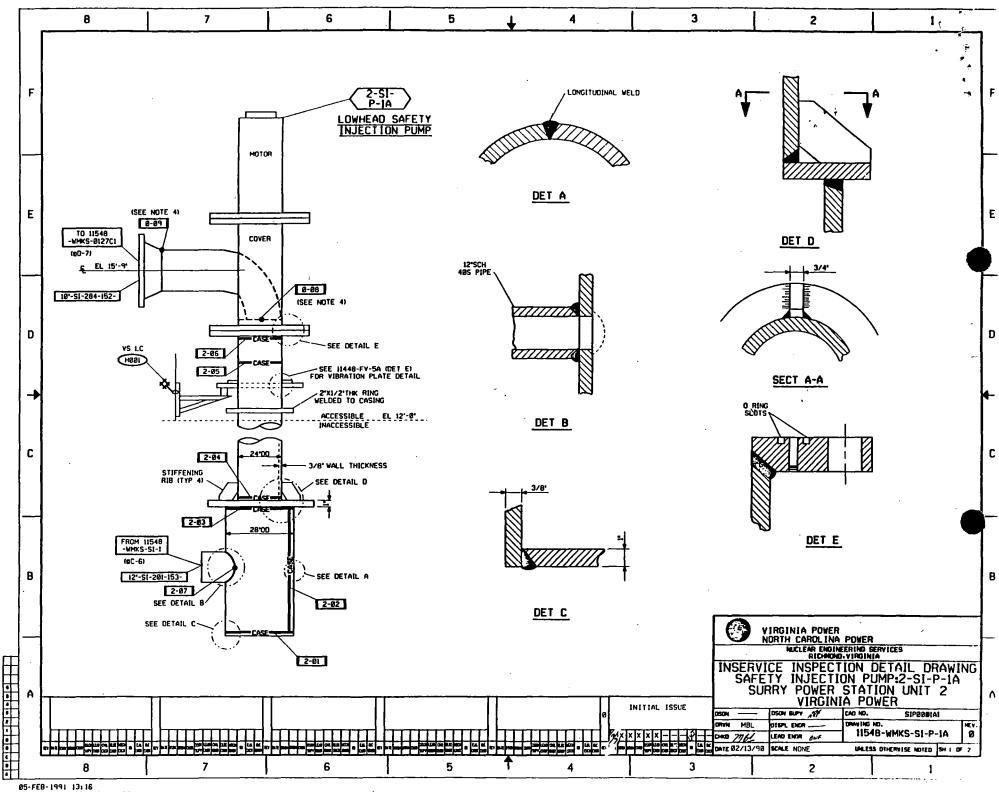
These pumps are vertical, two-stage, centrifugal pumps, with an extended shaft and casing to allow suction from the containment sump. The motor and mechanical seals of the pumps are located at about the 12 foot elevation and the bottom of the casing at about the -30 foot elevation. The welds identified are at the bottom of the pump casing, and are embedded within the concrete building structure. This makes the welds inaccessible from the outside. The small diameter of the casing (24 inch. O.D.) and the pump shaft prevent examination from the inside diameter.

IV. Alternate Requirements

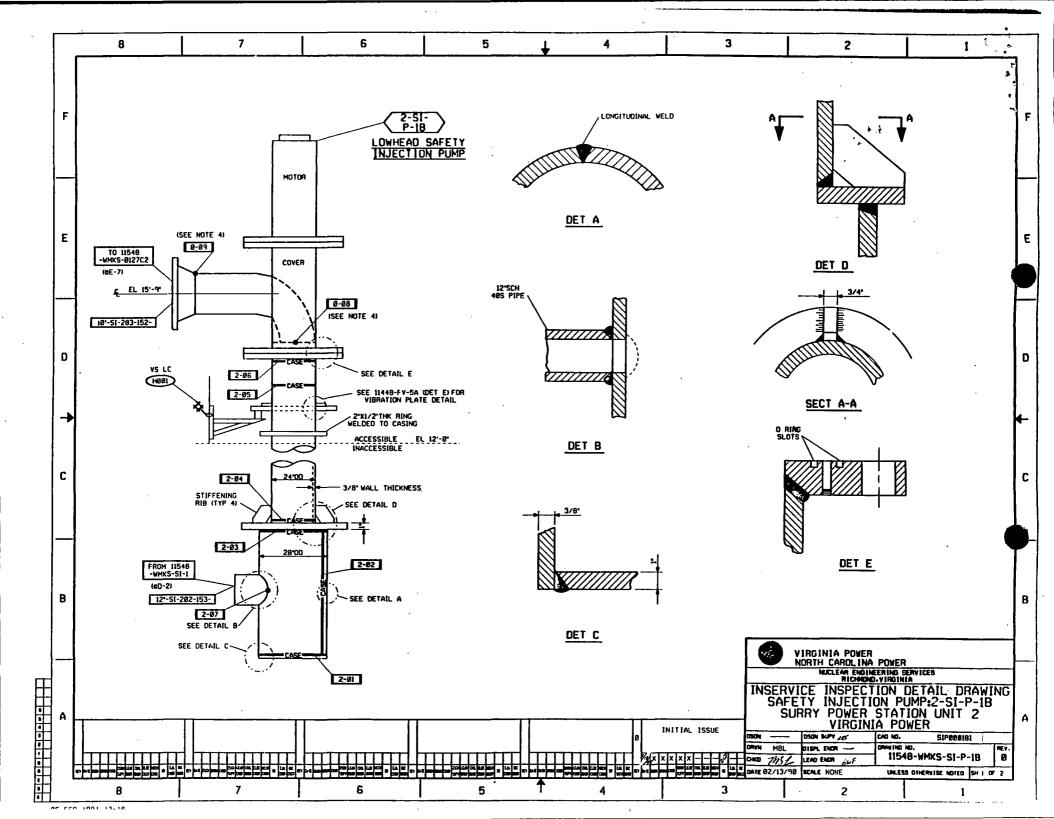
A remote visual examination (VT-1) of the accessible portions of the I.D. of the pump casing welds will be performed only if the pump is disassembled and the pump shaft removed for maintenance.







05-FEB-1991 13:16 ZGA5:[355,802]S[P000]A1.DGN



Relief Request 23

I. Identification of Components

System: Auxiliary Feedwater (AFW)

Component: Piping and components between the following

valves:

Valves	<u>Line</u>	<u>Valves</u>	<u>Class</u>
2-FW-145	1-WAPD-115-601	2-FW-149	3
		2-FW-146	3
		2-FW-629	3
2-FW-160	1-WAPD-117-601	2-FW-164	3
		2-FW-161	3
		2-FW-628	3
2-FW-175	1-WAPD-120-601	2-FW-179	3
		2-FW-176	. 3
		2-FW-627	3

(Drawing Attached)

II. Impractical Code Requirements

ISI Class 3 System Hydrostatic Test required in IWD-5223 of ASME Section XI, where design pressure is 1432 psig and the resultant test pressure is 1576 psig.

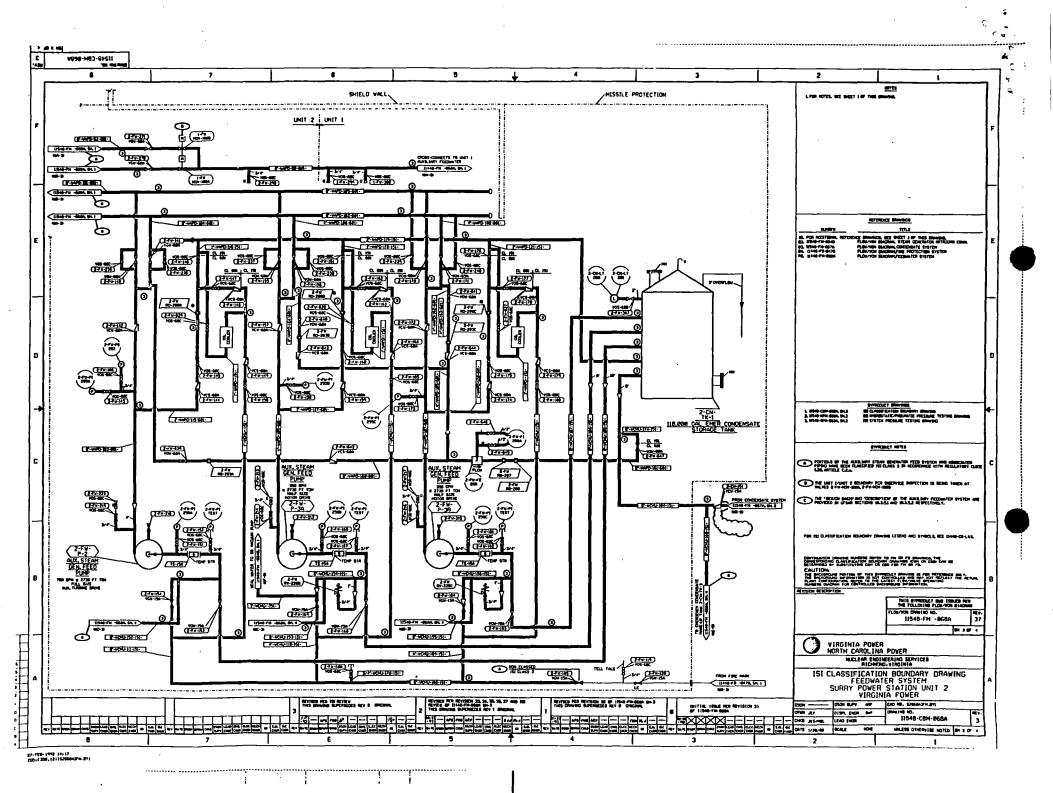
III. Basis For Relief

Three pressure reducing orifices 2-FW-RO-200A, 2-FW-RO-200B, and 2-FW-RO-200C provide during normal operation a pressure drop from approximately 1200 psig to 110 psig. The system design takes advantage of this pressure drop by incorporating lower pressure rated piping downstream of the orifices. However the higher pressure rated piping continues beyond the orifices for some distance. The actual pipe design pressure class change occurs at downstream check valves 2-FW-148, 2-FW-163, and 2-FW-178 and manual valves, 2-FW-146, 2-FW-161, and 2-FW-176. The check valve operation, however, does not allow separation of the lower pressure class system, when testing the higher class piping in accordance with IWD-5223. IWD-5223 would require a test pressure of 1576 psig on the higher pressure class components in question. The downstream connecting piping has a design pressure of 150 psig and a corresponding test pressure of only 165 psig. As such, the connecting components would be overpressurized during the required Section XI test. The test boundary could be backed up to manual isolation valves 2-FW-147, 2-FW-162, and 2-FW-177, however hydrostatically testing this test boundary would also pressurize the auxiliary feedwater pumps and their suction connection. These pumps have welded discharge connections and cannot be isolated from the test boundary due to the absence of a drain or vent valve in the area

identified above. There is a flange connection on the suction side of each pump, however using this flange for isolation purposes is considered difficult due to the piping arrangement, and susceptibility to cold spring misalignment problems. Typically centrifugal pumps are hydrostatically tested at a pressure based on the suction side of the pump as described in IWA-5224(d) of the Code, which prevents any potential overpressurization concerns, or the need to use pump flanges as isolation points. The basis for relief is then two-fold. The first impracticality is the overpressurization of piping and components downstream of the pressure reducing orifice and the design pressure class rating change. The second impracticality is the incorporation of the auxiliary feedwater pumps into the test boundary due to the lack of vent, drain, and manual isolation valves.

IV. Alternate Testing

The identified components will be tested in accordance with IWD-5222, Functional test requirements, in conjunction with the associated auxiliary feedwater pump at normal operating pressure.



Relief Request 24

I. Identification of Components

System: Main Steam

Components: Valve listed:

<u>Component</u> Valve <u>Mark#</u> 2-MS-119 <u>Line#</u> 4"-SHP-138-601 S/G Class

(Drawing attached)

II. Impractical Code Requirements
Surry Unit 2 utilized Code Case N-416, Alternate Rules for
Hydrostatic Testing of Repair or Replacement of Class 2
Piping Section XI, Division 1, on the components identified
above. This Code Case defers the hydrostatic test required
by IWA-4400 of ASME Section XI until the next regularly
scheduled system hydrostatic test (IWC-5000) for that
system.

III. Basis of Relief

The identified component was replaced under the rules of ASME Section XI. IWA-4400 of the Code requires that a hydrostatic test be conducted on certain welded repairs or replacements. This replacement cannot be hydrostatically tested without hydrostatically testing the connecting steam generator, as no intermediate isolation exists.

Prior to NRC and Code approval of Code Case N-416, relief requests were routinely written and approved for this type situation. The relief requests were based upon the difficulties associated with steam generator hydrostatic testing. The test cannot be conducted at ambient conditions due to fracture prevention concerns associated with the Surry steam generators, which results in difficult monitoring and controlling requirements. The Surry steam generators are required to be a minimum of 150 degrees F. on the secondary side and a minimum of 180 degrees F. on the primary side. Additionally normal problems, such as test boundary isolation, internal boundary leakage, placing spring hanger stops for dead weight loading concerns, and test pump size requirements further increase the difficulties associated with this particular test. The test pressure of 1356 psig also requires gaging or removal of the Main Steam Safety valves, which initially lift at 1085 psiq. Some examples of previous correspondence requesting relief and approval follow:

VEPCO Letter/ Date Serial# 88-725/ 1/9/89 Serial# 89-636/ 8/29/89 Serial# 87-056/ 2/13/87 NRC Letter/ Date
Serial# 89-278/ 4/7/89
Serial# 89-734/10/2/89
Serial# 88-419/6/17/88

When Code Case N-416 was incorporated into Regulatory guide 1.147, "Inservice Inspection Code Case Acceptability-ASME Section XI Division 1, relief requests were no longer needed, since the hydrostatic test was deferred to the end of the interval hydrostatic test described in table IWC-2500-1. This appeared to be the minimum hydrostatic testing that could be achieved for the steam generators. Recently in Revision 9 of Regulatory Guide 1.147, you approved Code Case N-498, Alternative Rules for 10-Year Hydrostatic Pressure Testing for Class 1 and 2 Systems Section XI, Division 1. This Code Case allows testing of the class 2 steam generators at nominal operating pressure. As a result, no hydrostatic test is now required by ASME Section XI on these components under normal circumstances, when incorporating Code Case N-498. The hydrostatic test of Code Case N-416 is

still required to be performed, however. As described before, the component identified above can only be hydrostatically tested by additionally testing the

test only for this replacement activity is considered

IV. Alternate testing

previously.

The alternative requirements described in Code Case N-416, a volumetric examination of the full penetration welds and a visual examination (VT-2) at nominal operating pressure was previously performed and deemed acceptable.

connecting steam generator. Requiring a full steam generator

impractical, due to the difficulties of the test described

