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1CAN101408

October 28, 2014

U.S. Nuclear Regulatory Commission
Attn: Document Control Desk
Washington, DC 20555

Subject: ANO-1 Cycle 25 COLR, Revision 2
Arkansas Nuclear One - Unit 1
Docket No. 50-313
License No. DPR-51

- References:
1. Entergy letter dated June 20, 2013, "ANO-1 Cycle 25 COLR" (1CAN061303)(ML13172A083)
 2. Entergy letter dated August 12, 2013, "ANO-1 Cycle 25 COLR, Revision 1" (1CAN081301)(ML13224A303)

Dear Sir or Madam:

Entergy Operations, Inc. (Entergy) Arkansas Nuclear One, Unit 1 (ANO-1) Technical Specification 5.6.5 requires the submittal of the Core Operating Limits Report (COLR) for each reload cycle, including submittal of any revisions or supplements that may occur following initial issuance. Attached is Revision 2 of the ANO-1 Cycle 25 COLR.

Early in Cycle 25 operation, examination of the ZW quadrant power tilt at each of the seven individual incore detector levels illustrated unexpected behavior. Based on comparisons of measured-to-predicted data coupled with some Axial Power Shaping Rod (APSR) manipulations, it was determined that an APSR in core location L04 was disconnected from the leadscrew and residing at the fully inserted position. Revision 2 of the Cycle 25 COLR permits this APSR to remain in the fully inserted position when the remaining seven APSRs are fully withdrawn at 480 ± 10 EFPD (Effective Full Power Days). This evaluation of this condition also results in an update to Reference 6 in Section 2.0 of the Cycle 25 COLR. No core operating limits, Technical Specification setpoints or safety limits, or insertion limits are challenged by permitting the subject APSR to remain fully inserted in the core for the remainder of Cycle 25 operation, currently scheduled to end January 25, 2015. See Page 15 of the attached revision to the ANO-1 Cycle 25 COLR for APSR changes.

Please note that the latest approved revision number of the Babcock and Wilcox Topical Report BAW-10179P-A is identified in the COLR as Revision 8, May 2010. This completes the reporting requirement for the referenced specification.

This submittal contains no regulatory commitments. Should you have any questions, please contact me.

Sincerely,

ORIGINAL SIGNED BY DAVID B. BICE

DBB

Attachment: ANO-1 Cycle 25 Core Operating Limits Report (COLR), Revision 2

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Attachment to

1CAN101408

ANO-1 Cycle 25 Core Operating Limits Report (COLR), Revision 2

ENTERGY OPERATIONS

ARKANSAS NUCLEAR ONE
UNIT ONE

CYCLE 25

CORE OPERATING LIMITS REPORT

1.0 CORE OPERATING LIMITS

This Core Operating Limits Report for ANO-1 Cycle 25 has been prepared in accordance with the requirements of Technical Specification 5.6.5. The core operating limits have been developed using the methodology provided in the references.

The following cycle-specific core operating limits are included in this report:

- 1) 2.1.1.3 Variable Low RCS Pressure – Temperature Protective Limits
- 2) 3.1.1 SHUTDOWN MARGIN (SDM)
- 3) 3.1.8 PHYSICS TESTS Exceptions – MODE 1
- 4) 3.1.9 PHYSICS TEST Exceptions – MODE 2
- 5) 3.2.1 Regulating Rod Insertion Limits
- 6) 3.2.2 AXIAL POWER SHAPING RODS (APSR) Insertion Limits
- 7) 3.2.3 AXIAL POWER IMBALANCE Operating Limits
- 8) 3.2.4 QUADRANT POWER TILT (QPT)
- 9) 3.2.5 Power Peaking
- 10) 3.3.1 Reactor Protection System (RPS) Instrumentation
- 11) 3.4.1 RCS Pressure, Temperature, and Flow DNB Limits
- 12) 3.4.4 RCS Loops – MODES 1 and 2
- 13) 3.9.1 Boron Concentration

2.0 REFERENCES

1. "Safety Criteria and Methodology for Acceptable Cycle Reload Analyses," BAW-10179P-A, Rev. 8, Framatome ANP, Inc., Lynchburg, Virginia, May 2010.
2. Letter dated 4/9/02 from L.W. Barnett, USNRC, to J.M. Mallay, FRA-ANP, "Safety Evaluation of Framatome Technologies Topical Report BAW-10164P Revision 4, 'RELAP5/MOD2- B&W, An Advanced Computer Program for Light Water Reactor LOCA and Non-LOCA Transient Analysis' (TAC Nos. MA8465 and MA8468)," USNRC ADAMS Accession Number ML013390204.
3. RELAP5/MOD2-B&W – An Advanced Computer Program for Light Water Reactor LOCA Transient Analysis, BAW-10164PA, Rev. 6, Framatome Technologies, Inc., Lynchburg, Virginia, June 2007.
4. "Qualification of Reactor Physics Methods for the Pressurized Water Reactors of the Entergy System," ENEAD-01-P, Rev. 0, Entergy Operations, Inc., Jackson, Mississippi, December 1993.
5. "ANO-1 Cycle 25 Limits and Setpoints," Areva Doc. No. 86-9187139-000, December 6, 2012.
6. "Arkansas Nuclear One, Unit 1, Cycle 25 Reload Report," ANP-3185, Rev. 2, April, 2014 (CALC-ANO1-NE-12-00001).
7. "ANO-1 Refueling Boron for 1R24," CALC-NEAD-SR-13/004, Rev. 0.
8. "IC (Initial Condition) DNB RCS Protection Criteria," CALC-96-E-0023-02, Rev. 7.

2.0 REFERENCES (continued)

9. "Arkansas Nuclear One Unit 1, Cycle 25 Reload Technical Document (RTD)," Areva Doc. No. 51-9194170-000, January, 2013 (CALC-ANO1-NE-12-00003).
10. "Calc – ANO-1 Cycle 25 Maneuvering Analysis Safety Related," Areva Doc. No. FS1-0012430, Rev. 1.0, August 10, 2013.

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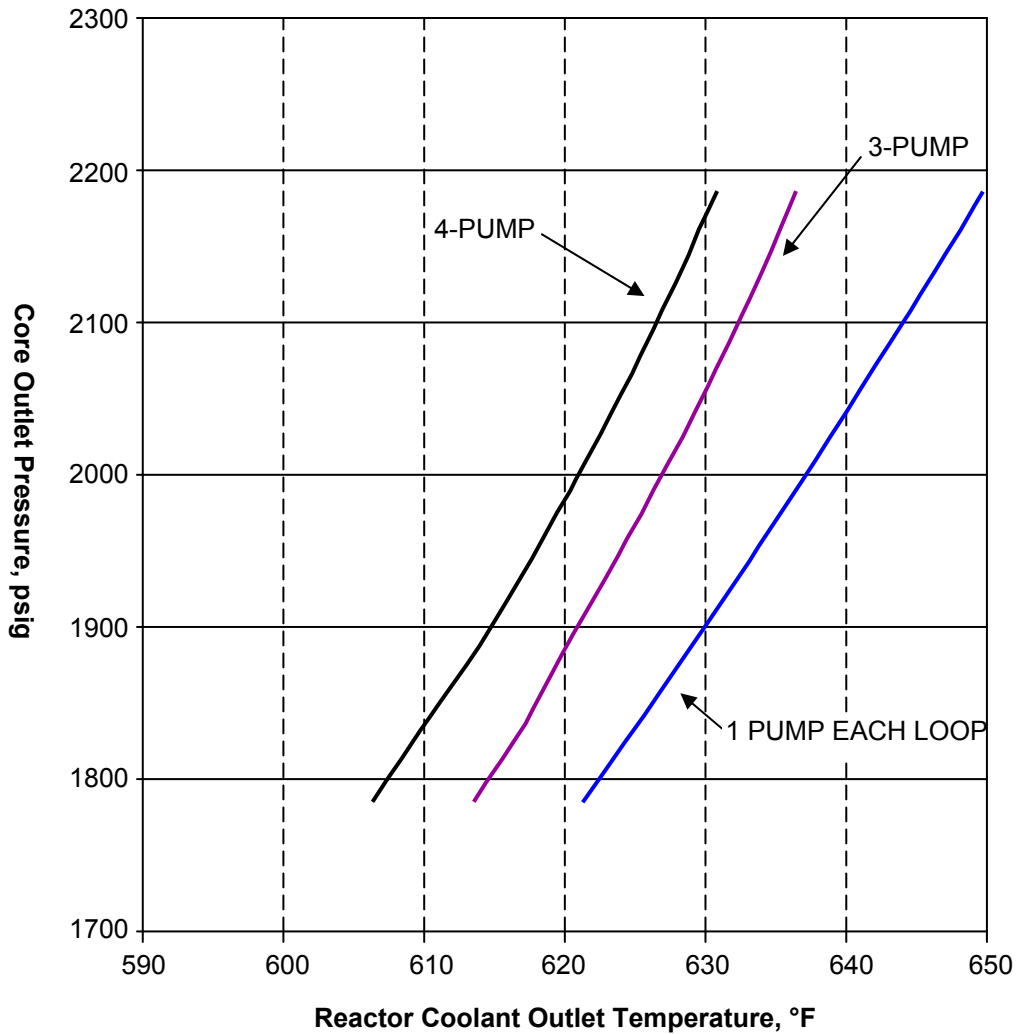
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FIGURE 1

Variable Low RCS Pressure – Temperature Protective Limits

(Figure is referred to by Technical Specification 2.1.1.3)



<u>PUMPS OPERATING (TYPE OF LIMIT)</u>	<u>GPM*</u>	<u>POWER**</u>
FOUR PUMPS (DNBR LIMIT)	383,680 (100%)	110%
THREE PUMPS (DNBR LIMIT)	284,307 (74.1%)	89%
ONE PUMP IN EACH LOOP (DNBR LIMIT)	188,003 (49%)	62.2%

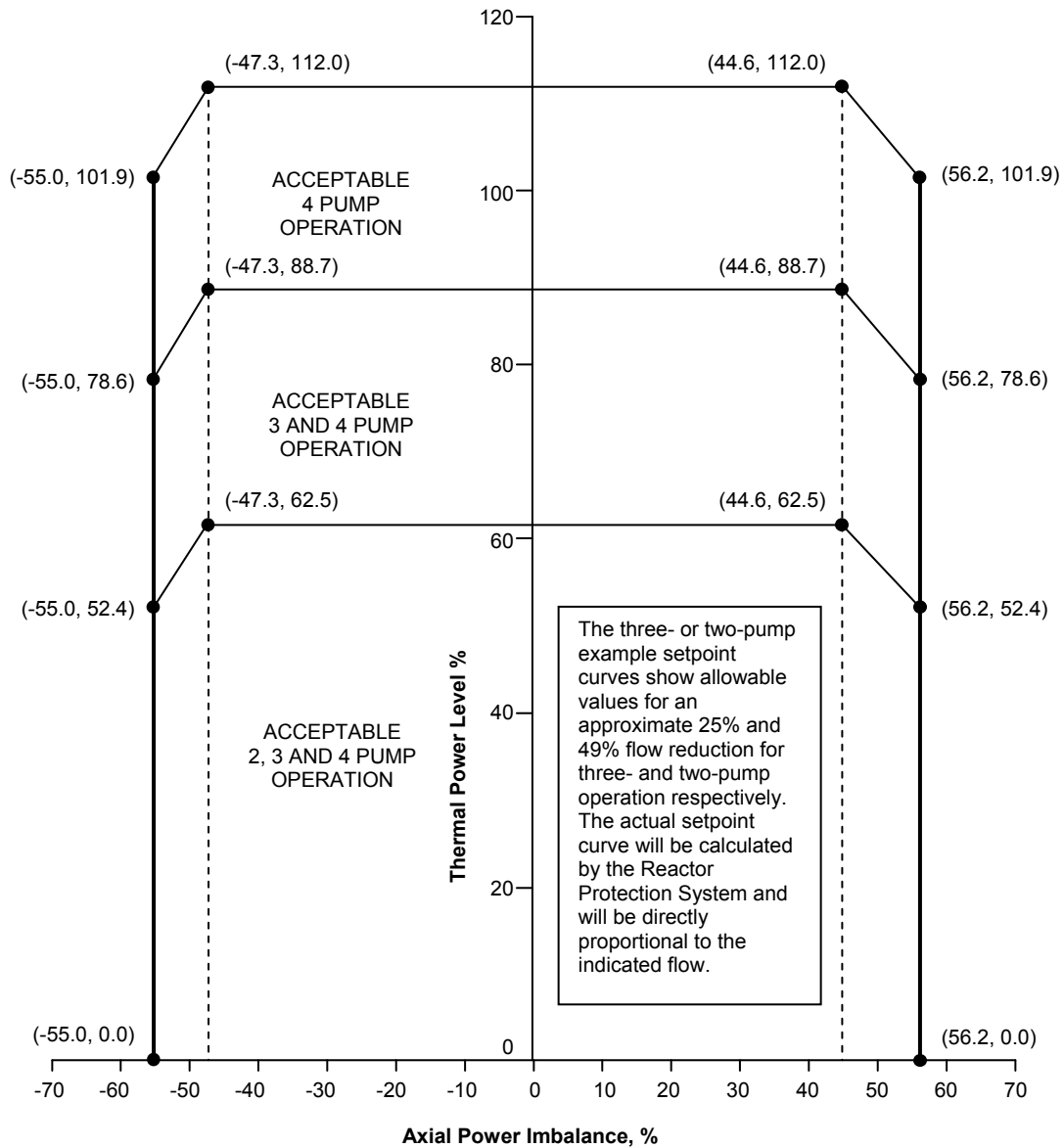
* 109% OF DESIGN FLOW (2.5% UNCERTAINTY INCLUDED IN STATISTICAL DESIGN LIMIT)

** AN ADDITIONAL 2% POWER UNCERTAINTY IS INCLUDED IN STATISTICAL DESIGN LIMIT

Figure 2

AXIAL POWER IMBALANCE Protective Limits
(measurement system independent)

(Figure is referred to by Technical Specification 2.1.1 Bases)



SHUTDOWN MARGIN (SDM)

(Limits are referred to by Technical Specifications 3.1.1, 3.1.4, 3.1.5, 3.1.8, 3.1.9, and 3.3.9)

Verify SHUTDOWN MARGIN per the table below.

APPLICABILITY	REQUIRED SHUTDOWN MARGIN	TECHNICAL SPECIFICATION REFERENCE
MODE 1*	$\geq 1 \text{ \%}\Delta k/k$	3.1.4, 3.1.5
MODE 2*	$\geq 1 \text{ \%}\Delta k/k$	3.1.4, 3.1.5, 3.3.9
MODE 3	$\geq 1 \text{ \%}\Delta k/k$	3.1.1, 3.3.9
MODE 4	$\geq 1 \text{ \%}\Delta k/k$	3.1.1, 3.3.9
MODE 5	$\geq 1 \text{ \%}\Delta k/k$	3.1.1, 3.3.9
MODE 1 PHYSICS TESTS Exceptions**	$\geq 1 \text{ \%}\Delta k/k$	3.1.8
MODE 2 PHYSICS TESTS Exceptions	$\geq 1 \text{ \%}\Delta k/k$	3.1.9

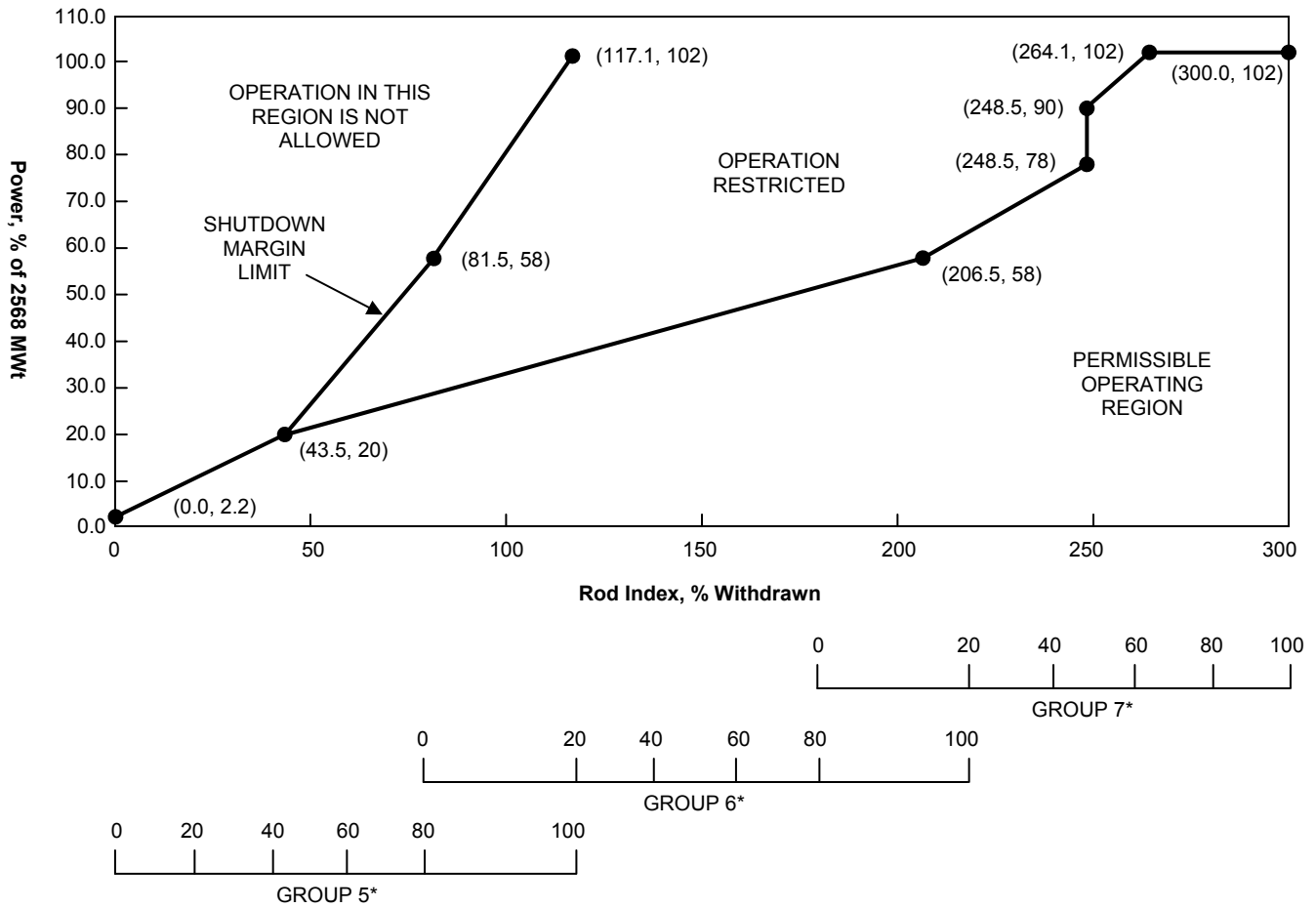
* The required Shutdown Margin capability of $1 \text{ \%}\Delta k/k$ in MODE 1 and MODE 2 is preserved by the Regulating Rod Insertion Limits specified in Figures 3-A&B, 4-A&B, and 5-A&B, as required by Technical Specification 3.2.1.

** Entry into Mode 1 Physics Tests Exceptions is not supported by existing analyses and as such requires actual shutdown margin to be $\geq 1 \text{ \%}\Delta k/k$.

Figure 3-A

Regulating Rod Insertion Limits for Four-Pump Operation From 0 to 200 ± 10 EFPD

(Figure is referred to by Technical Specification 3.2.1)

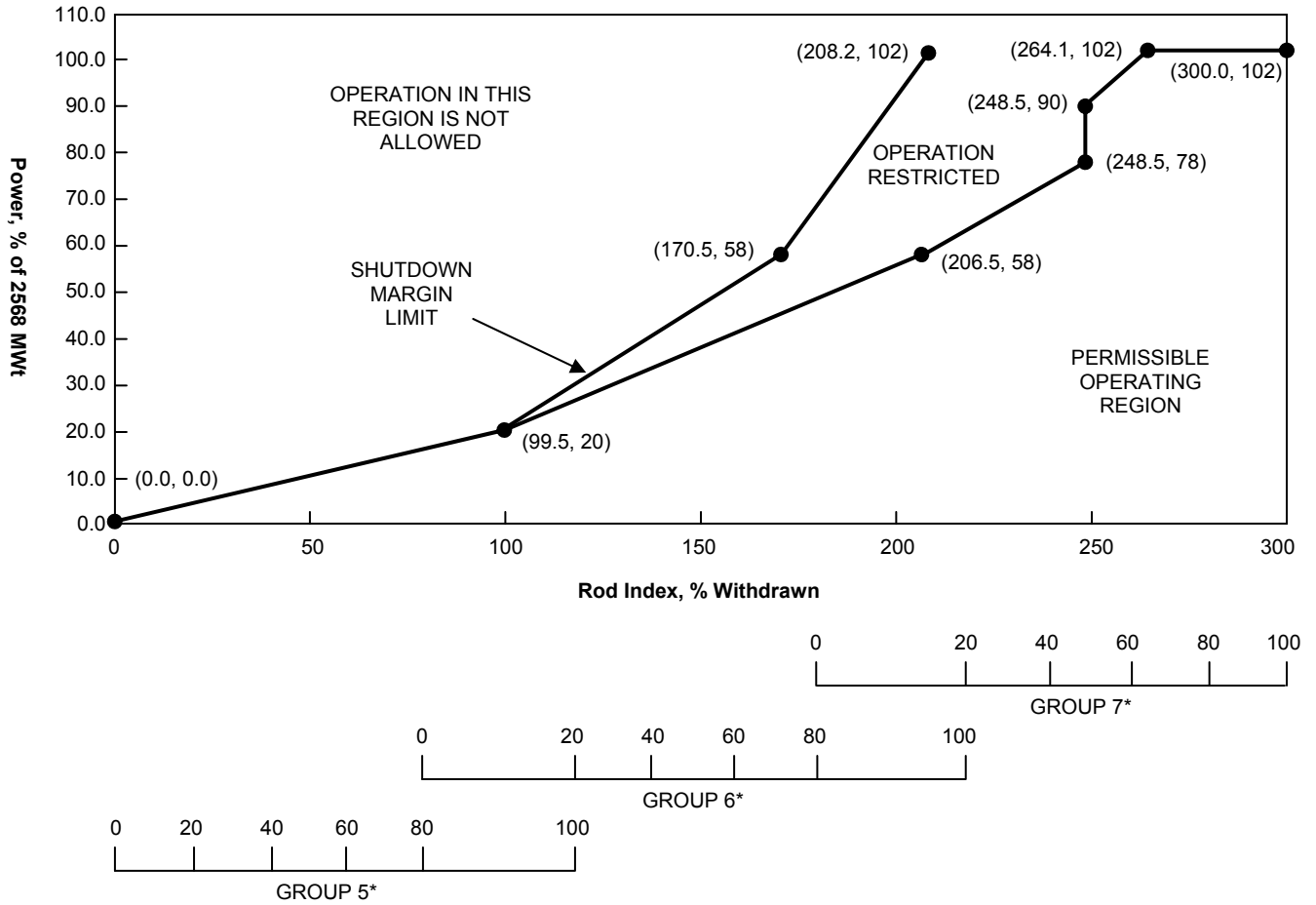


* Operating rod group overlap is 20% ± 5% between two sequential groups, except for physics tests.

Figure 3-B

Regulating Rod Insertion Limits for Four-Pump Operation From 200 ± 10 EFPD to EOC

(Figure is referred to by Technical Specification 3.2.1)

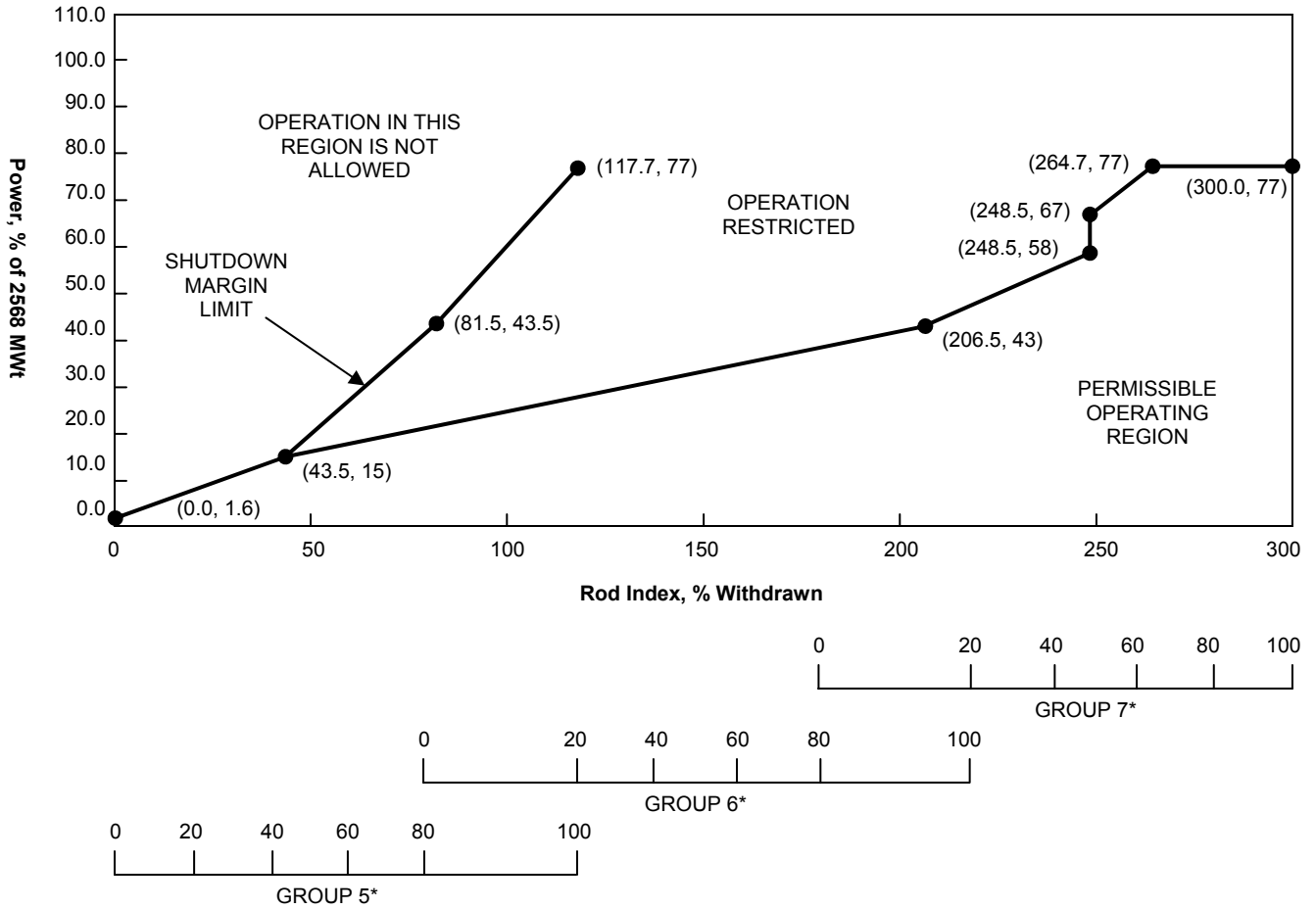


* Operating rod group overlap is $20\% \pm 5\%$ between two sequential groups, except for physics tests.

Figure 4-A

Regulating Rod Insertion Limits for Three-Pump Operation From 0 to 200 ± 10 EFPD

(Figure is referred to by Technical Specification 3.2.1)

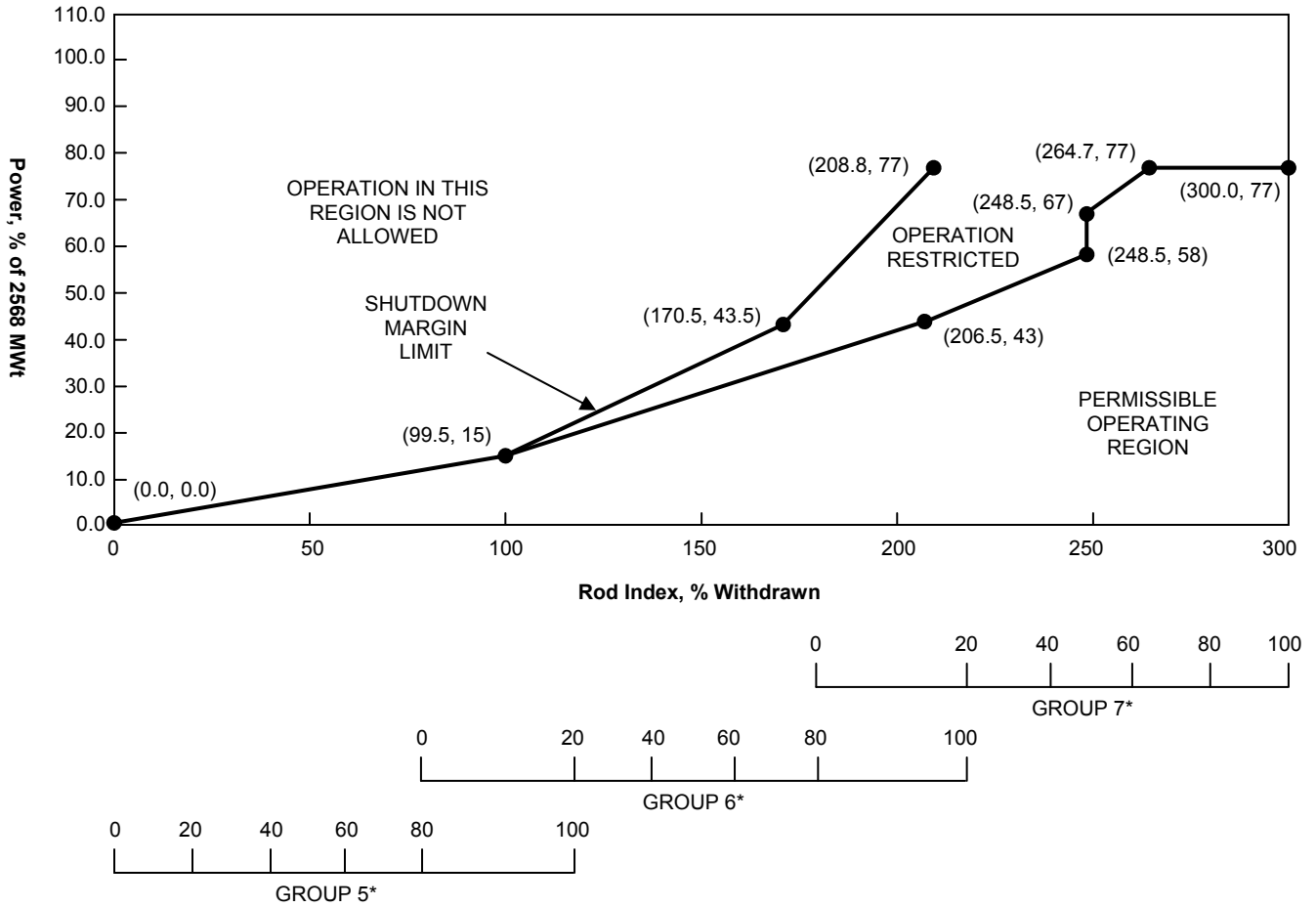


* Operating rod group overlap is 20% ± 5% between two sequential groups, except for physics tests.

Figure 4-B

Regulating Rod Insertion Limits for Three-Pump Operation From 200 ± 10 EFPD to EOC

(Figure is referred to by Technical Specification 3.2.1)

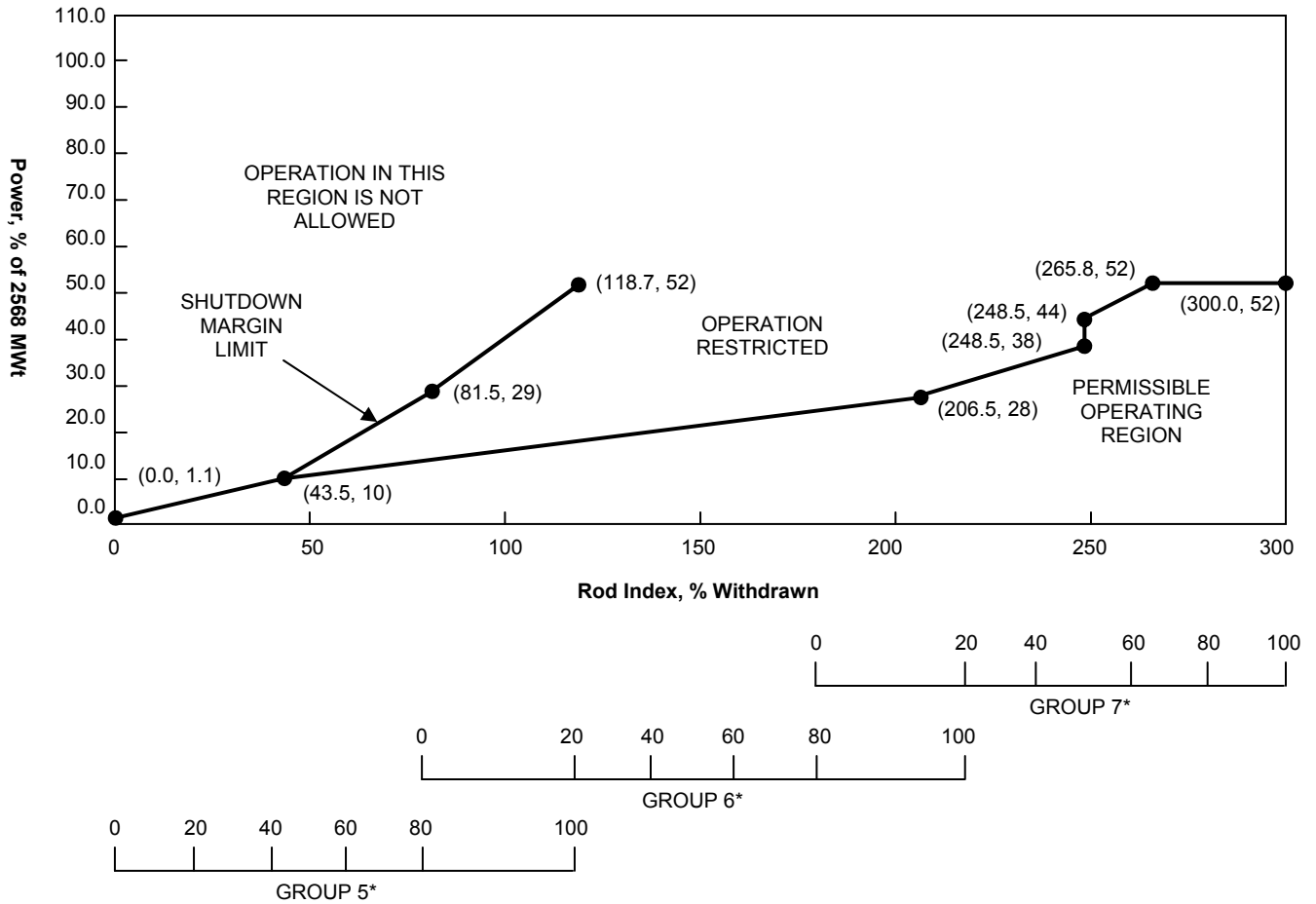


* Operating rod group overlap is $20\% \pm 5\%$ between two sequential groups, except for physics tests.

Figure 5-A

Regulating Rod Insertion Limits for Two-Pump Operation From 0 to 200 ± 10 EFPD

(Figure is referred to by Technical Specification 3.2.1)

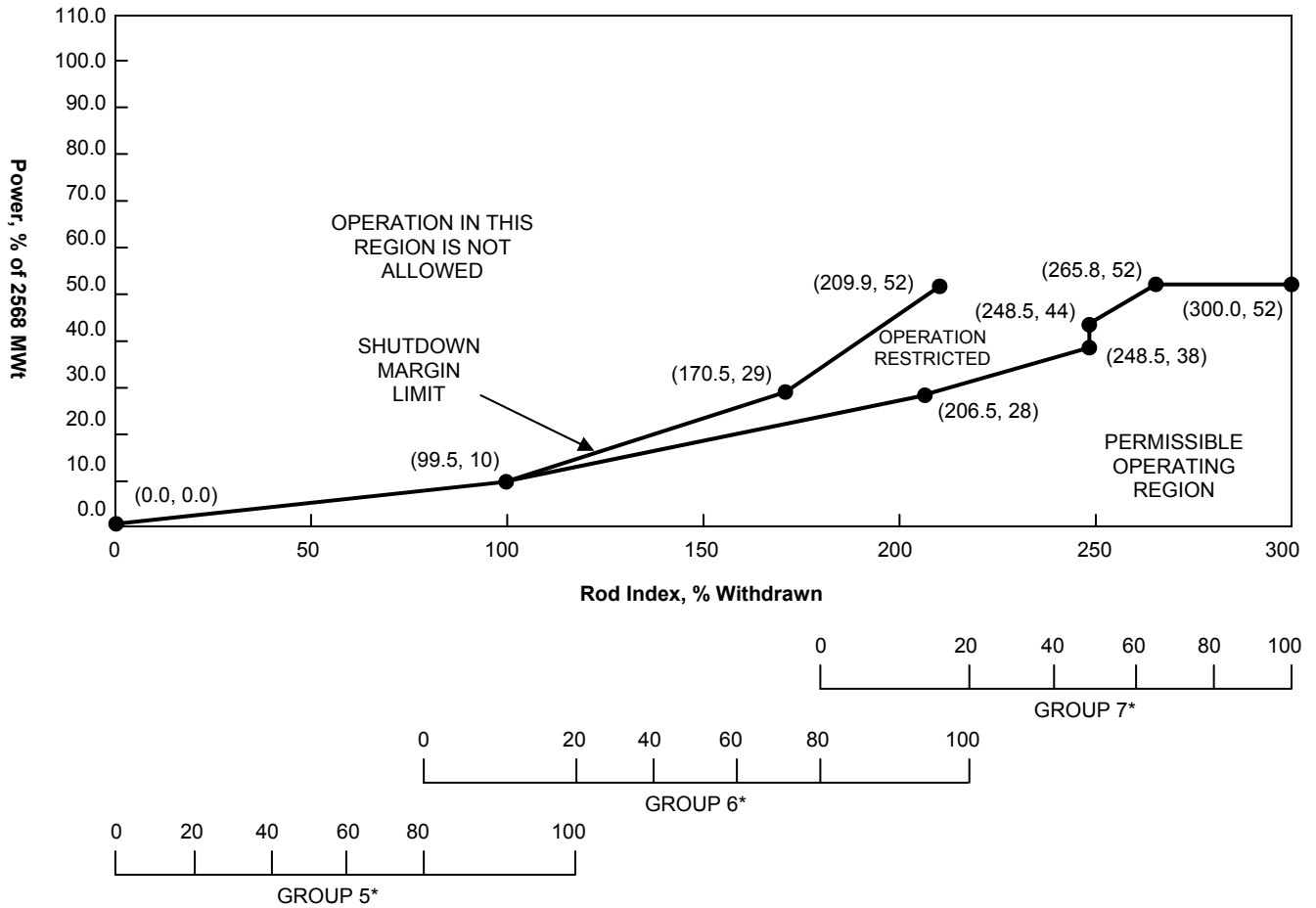


* Operating rod group overlap is 20% ± 5% between two sequential groups, except for physics tests.

Figure 5-B

Regulating Rod Insertion Limits for Two-Pump Operation From 200 ± 10 EFPD to EOC

(Figure is referred to by Technical Specification 3.2.1)



* Operating rod group overlap is $20\% \pm 5\%$ between two sequential groups, except for physics tests.

AXIAL POWER SHAPING RODS (APSR) INSERTION LIMITS

(Limits referred to by Technical Specification 3.2.2)

Up to 480 ± 10 EFPD, the APSRs, excluding the disconnected APSR in location L04, may be positioned as necessary for transient imbalance control; however, the APSRs, excluding the disconnected APSR in location L04, shall be fully withdrawn by 490 EFPD. After the APSR withdrawal at 480 ± 10 EFPD, the APSRs, excluding the disconnected APSR in location L04, shall not be reinserted, except during the end of cycle shutdown when the reactor power is equal to, or less than, 30% FP.

Figure 6-A

AXIAL POWER IMBALANCE Setpoints for Full In-Core Conditions for Four-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)

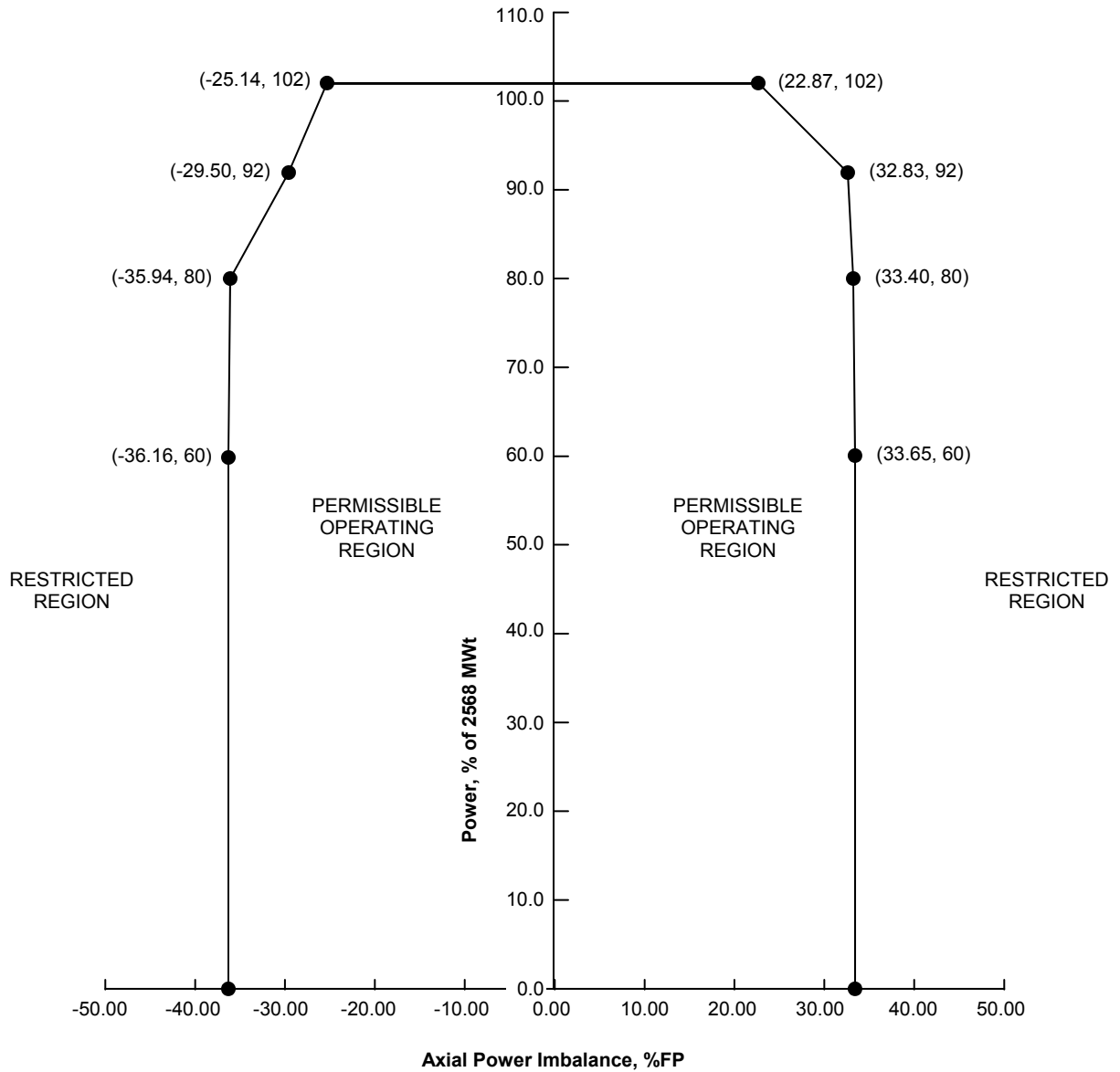
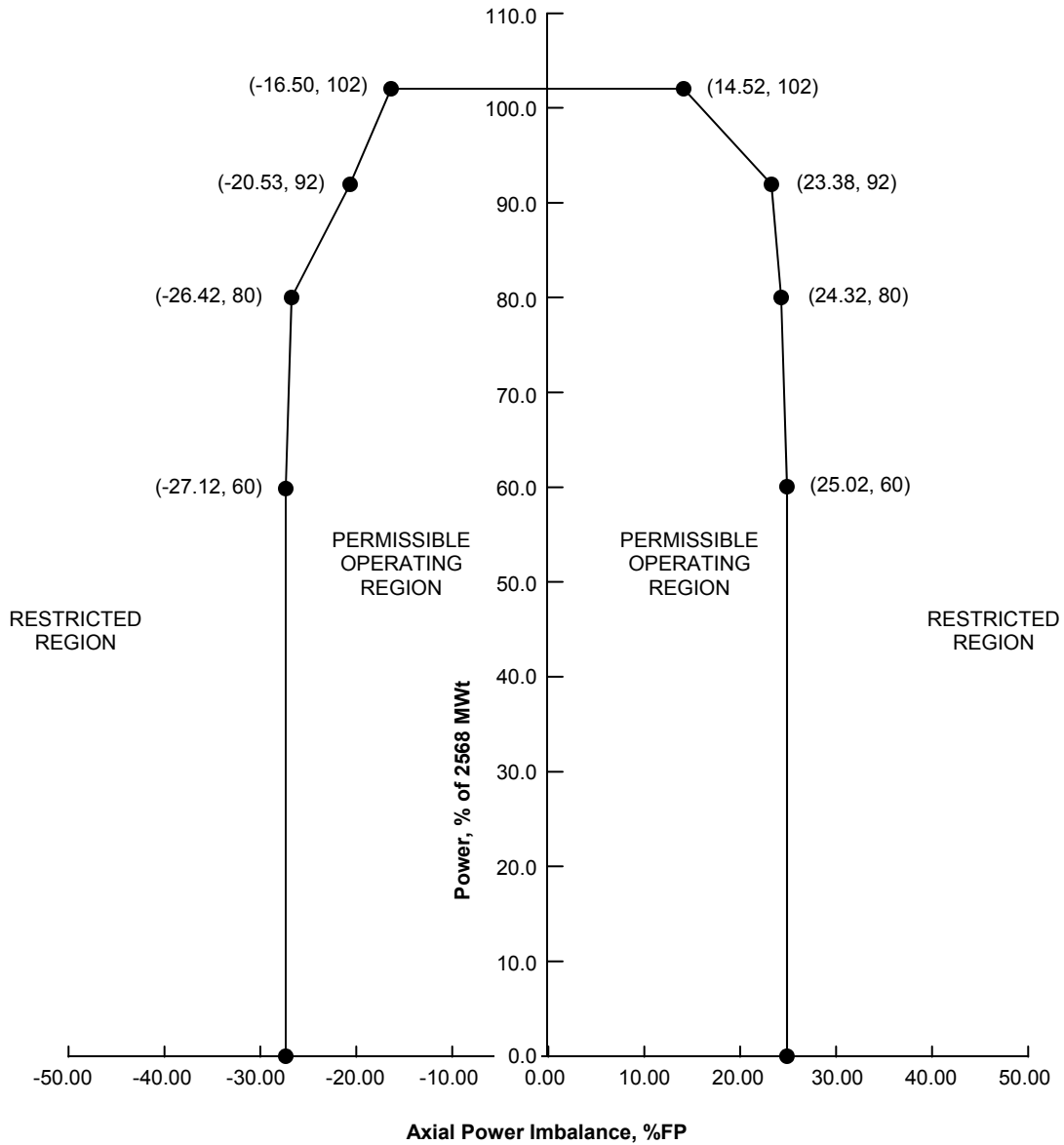


Figure 6-B

AXIAL POWER IMBALANCE Setpoints for Minimum In-Core Conditions* for Four-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)



* Assumes that no individual long emitter detector affecting the minimum incore imbalance calculation exceeds 73% sensitivity depletion. The imbalance setpoints for the minimum incore system must be reduced to 2.8% FP at the earliest time-in-life this assumption is no longer valid.

Figure 6-C

AXIAL POWER IMBALANCE Setpoints for Ex-Core Conditions for Four-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)

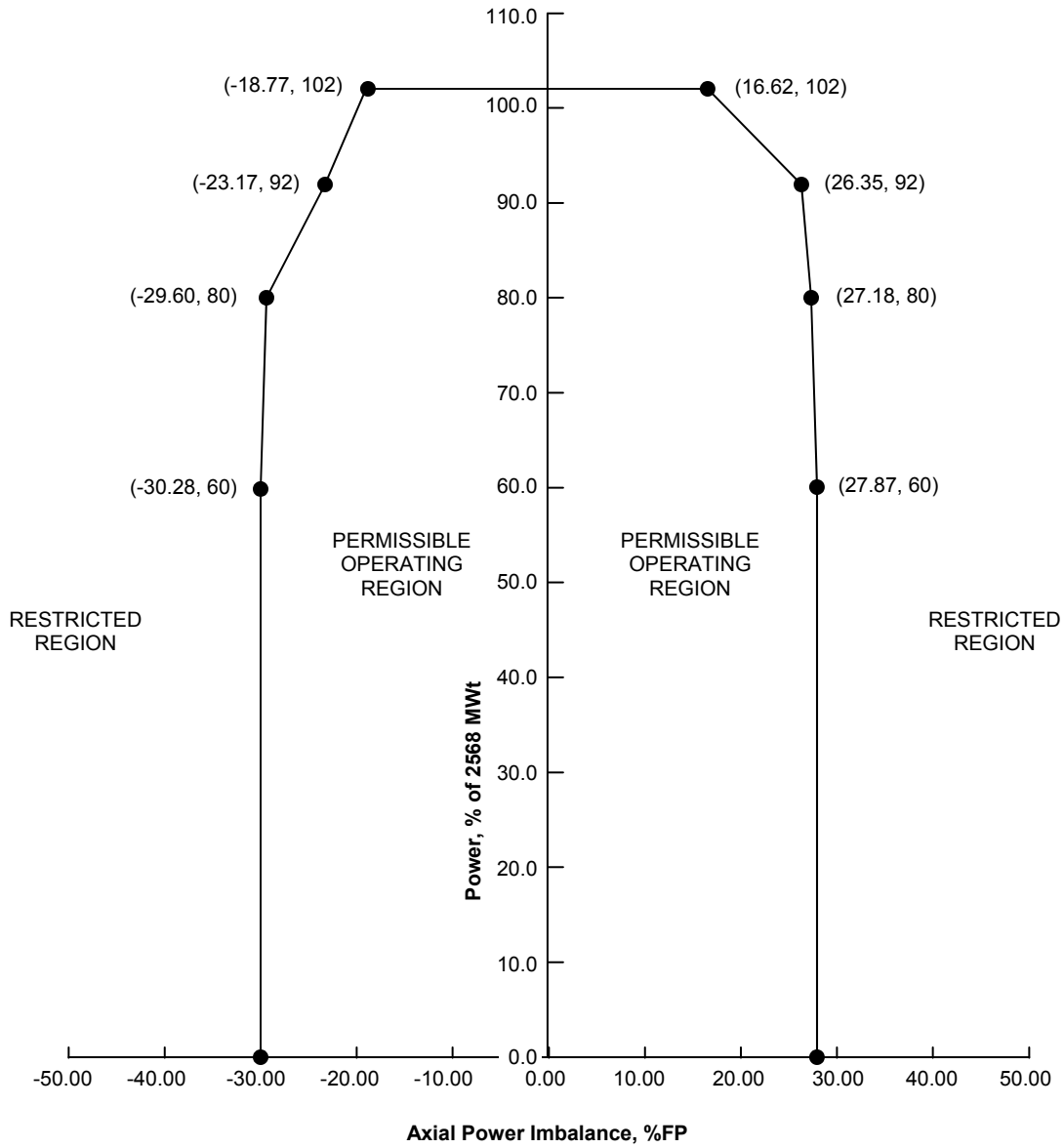


Figure 7-A

AXIAL POWER IMBALANCE Setpoints for Full In-Core Conditions for Three-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)

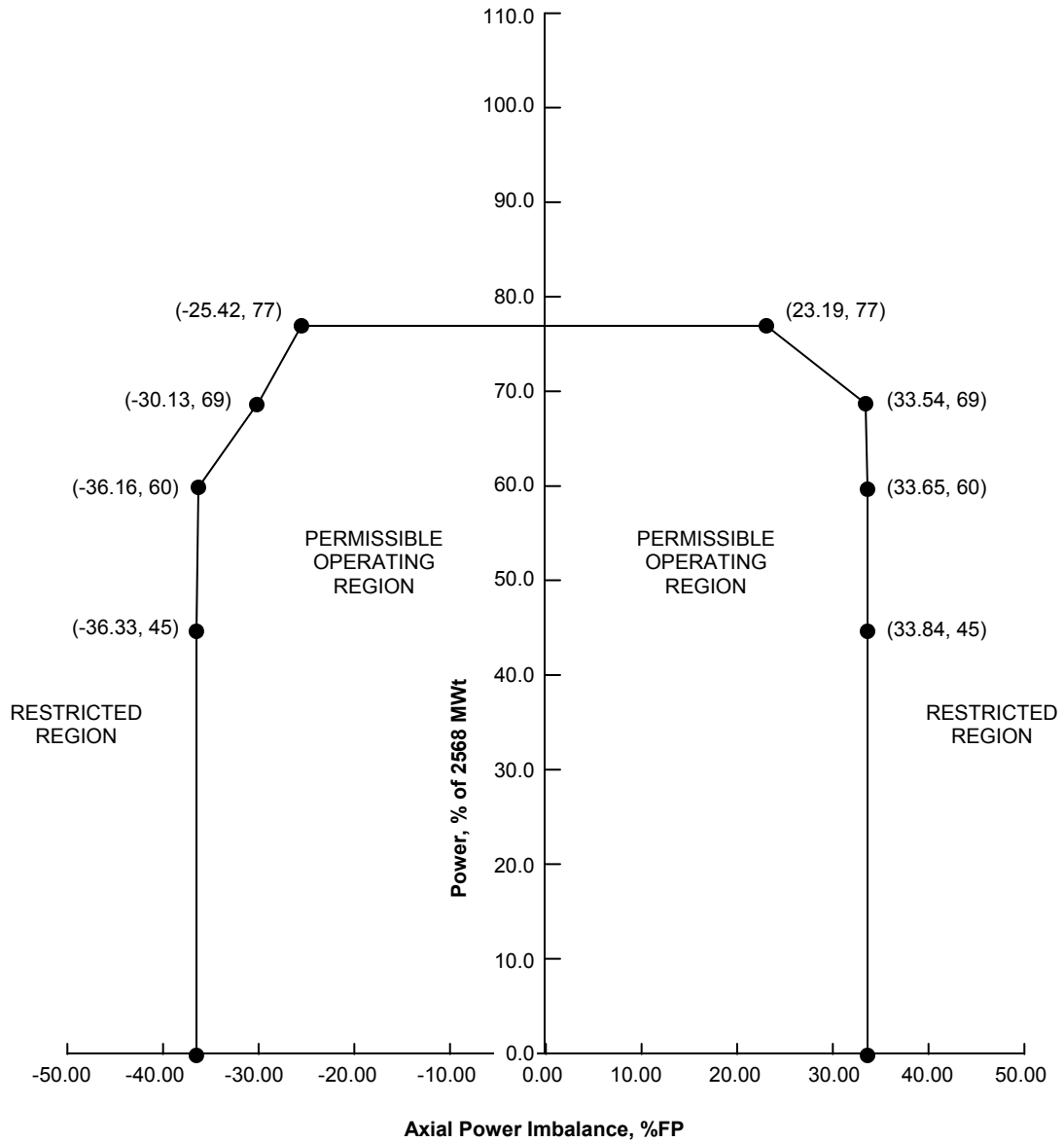
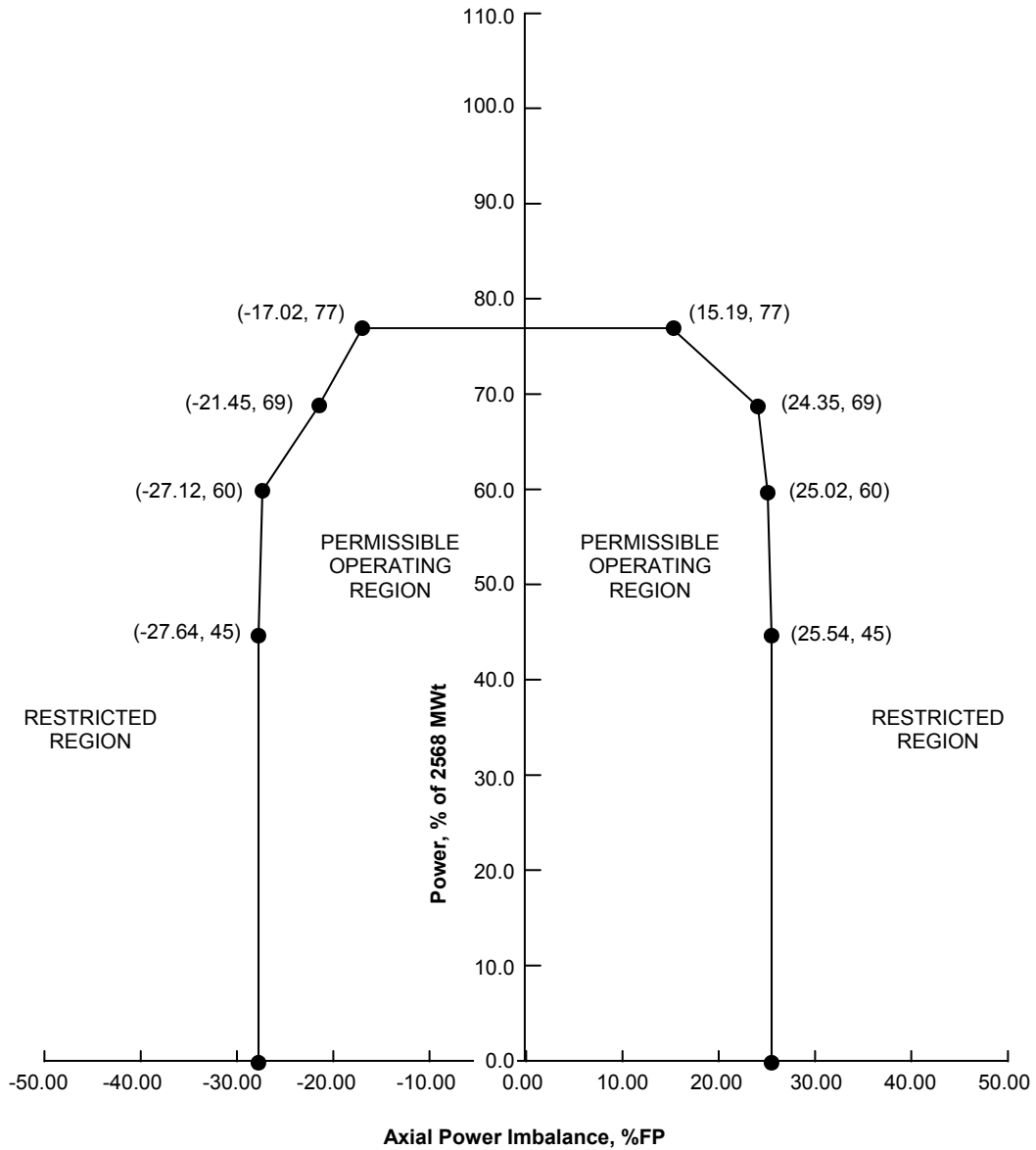


Figure 7-B

AXIAL POWER IMBALANCE Setpoints for Minimum In-Core Conditions* for Three-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)



* Assumes that no individual long emitter detector affecting the minimum incore imbalance calculation exceeds 73% sensitivity depletion. The imbalance setpoints for the minimum incore system must be reduced to 2.8% FP at the earliest time-in-life this assumption is no longer valid.

Figure 7-C

AXIAL POWER IMBALANCE Setpoints for Ex-Core Conditions for Three-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)

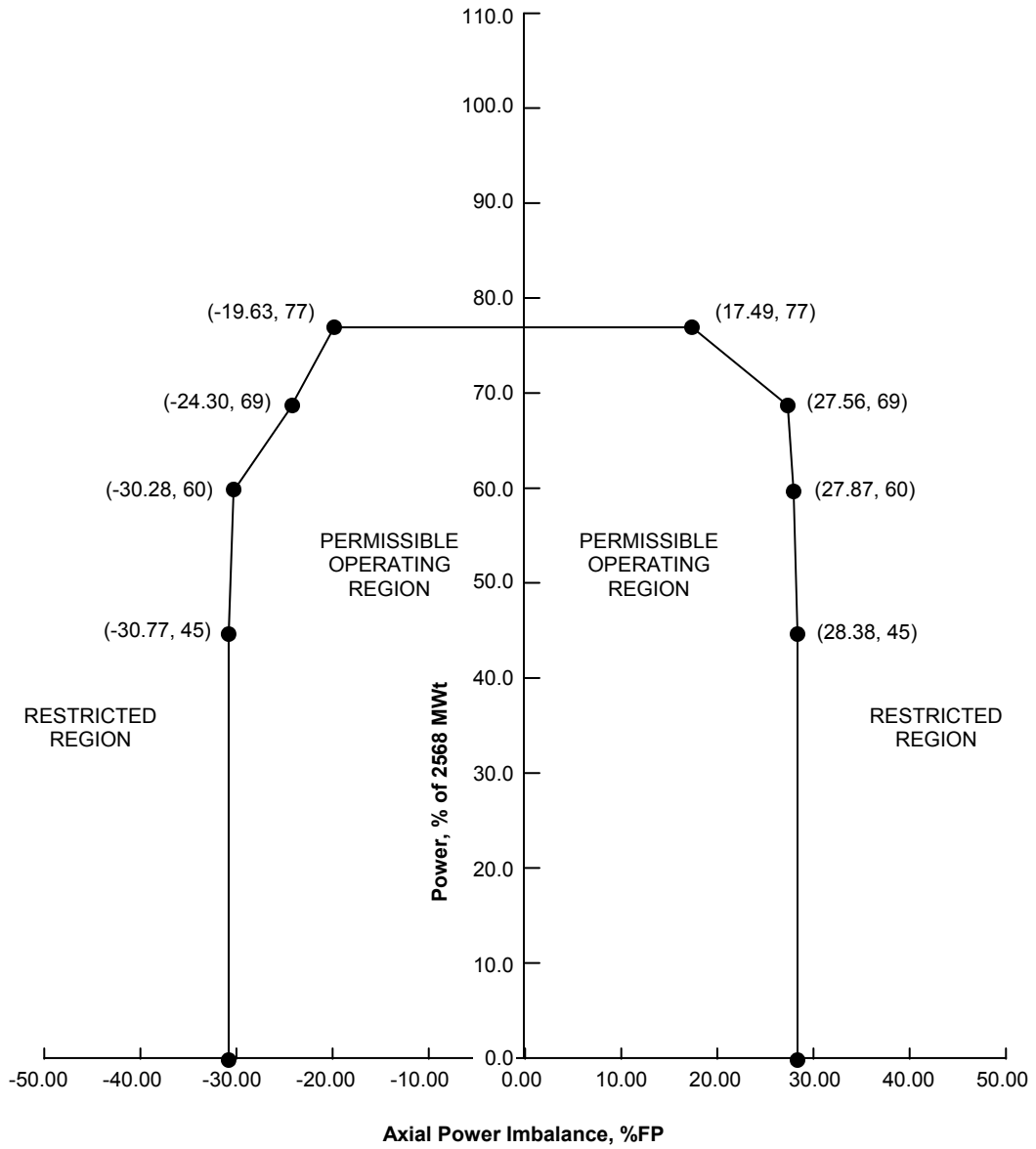


Figure 8-A

AXIAL POWER IMBALANCE Setpoints for Full In-Core Conditions for Two-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)

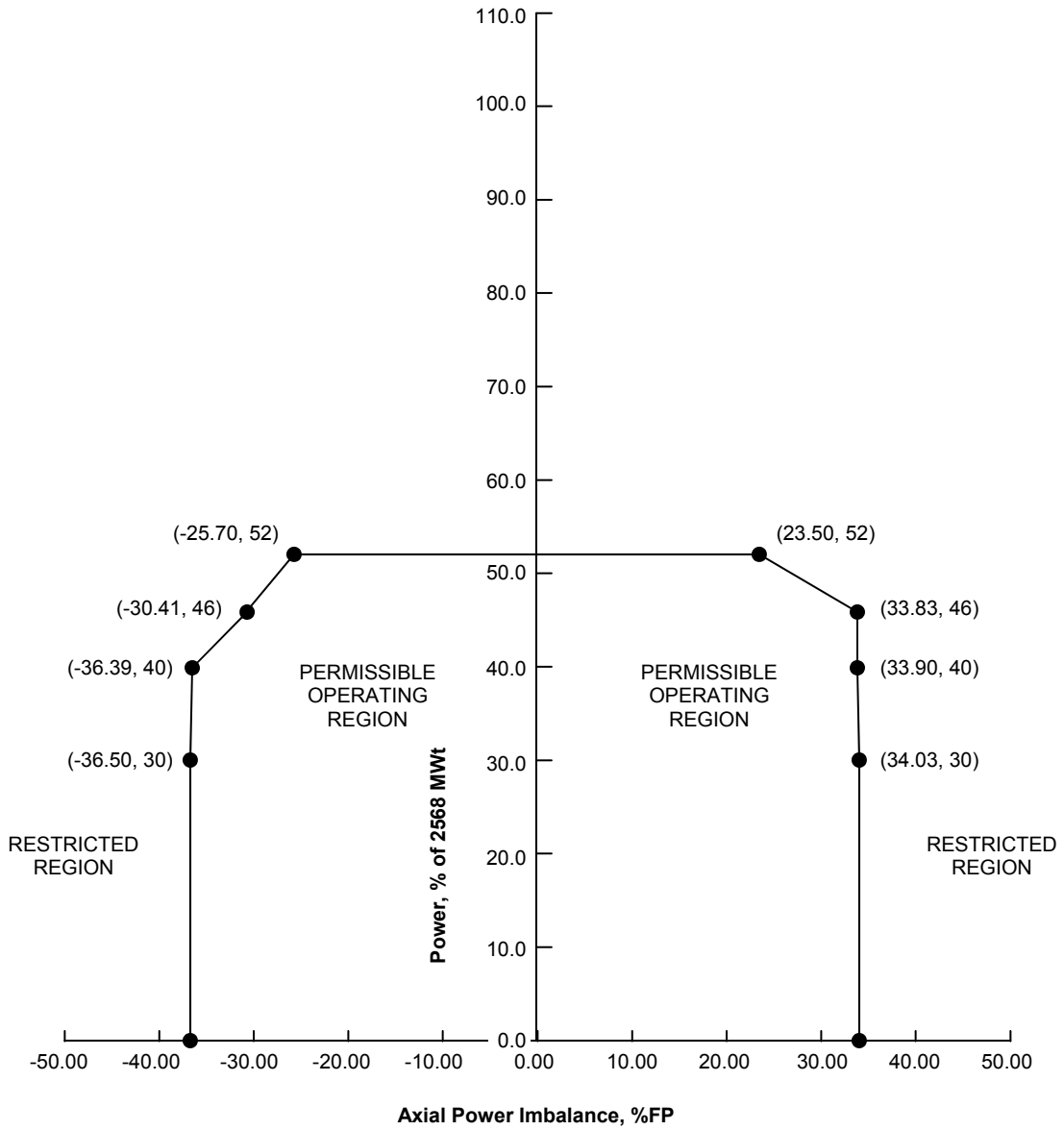
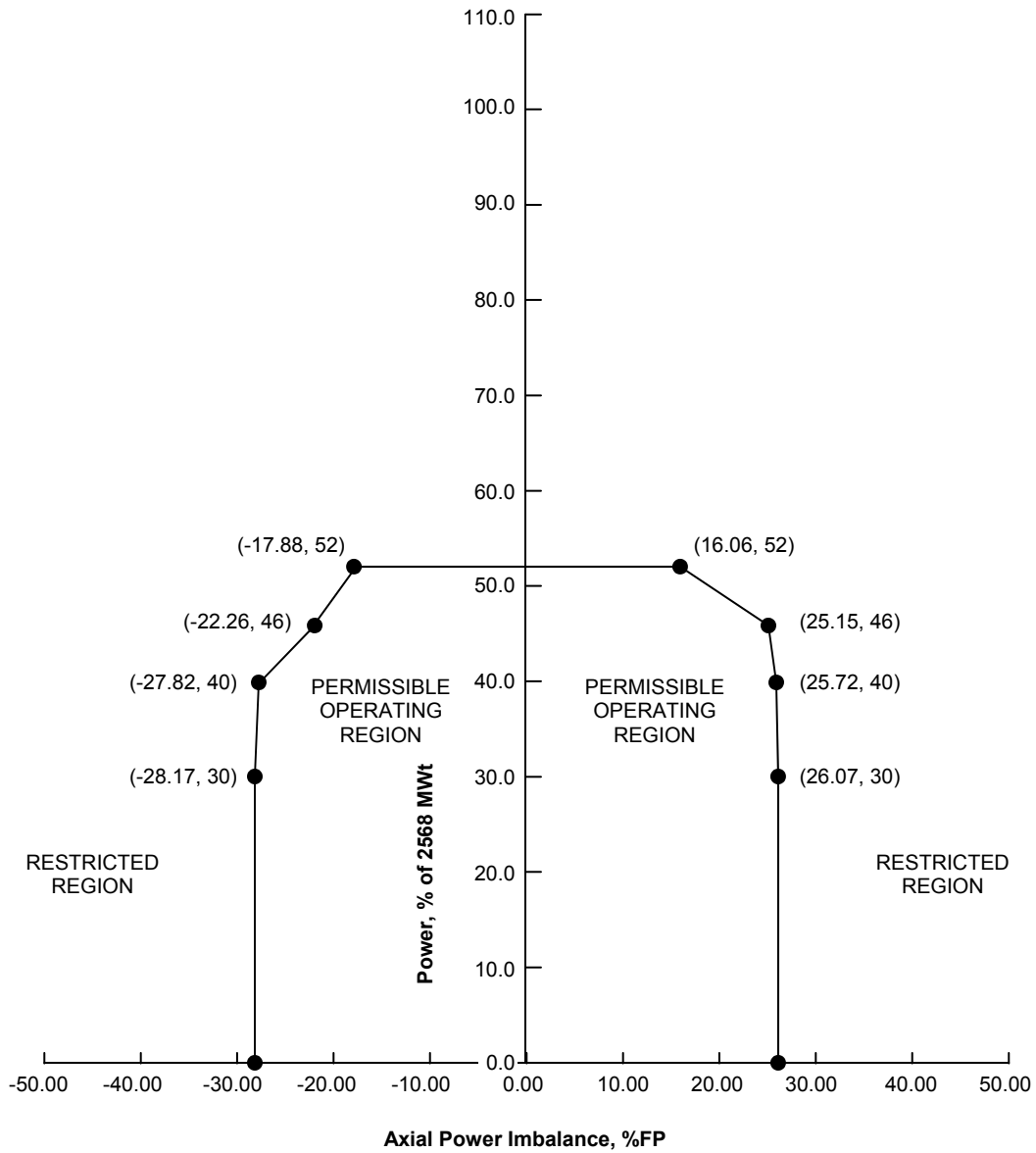


Figure 8-B

AXIAL POWER IMBALANCE Setpoints for Minimum In-Core Conditions* for Two-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)

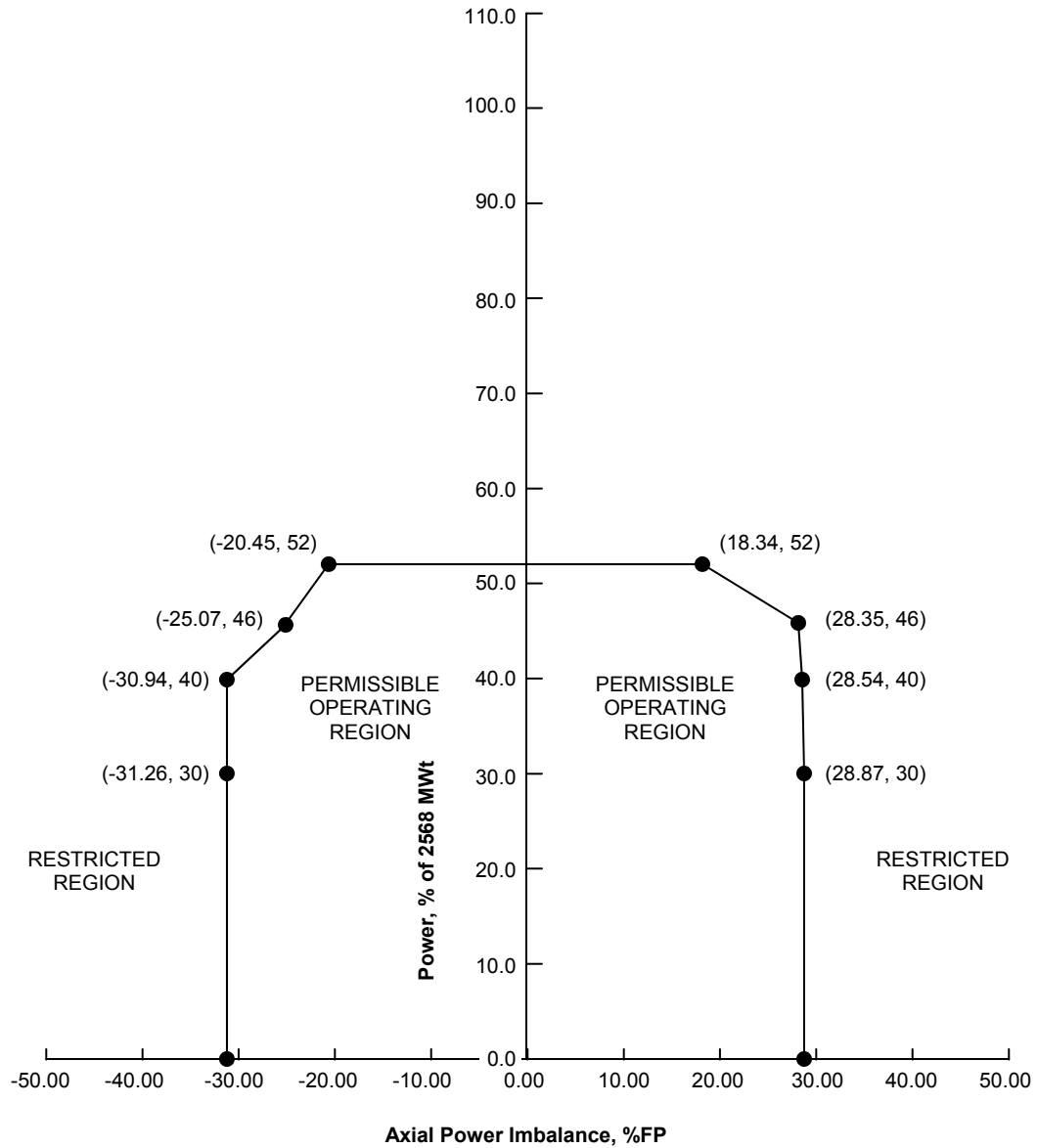


* Assumes that no individual long emitter detector affecting the minimum incore imbalance calculation exceeds 73% sensitivity depletion. The imbalance setpoints for the minimum incore system must be reduced to 2.8% FP at the earliest time-in-life this assumption is no longer valid.

Figure 8-C

AXIAL POWER IMBALANCE Setpoints for Ex-Core Conditions for Two-Pump Operation from 0 to EOC

(Figure is referred to by Technical Specification 3.2.3)



Quadrant Power Tilt Limits And Setpoints

(Limits are referred to by Technical Specification 3.2.4)

From 0 EFPD to EOC

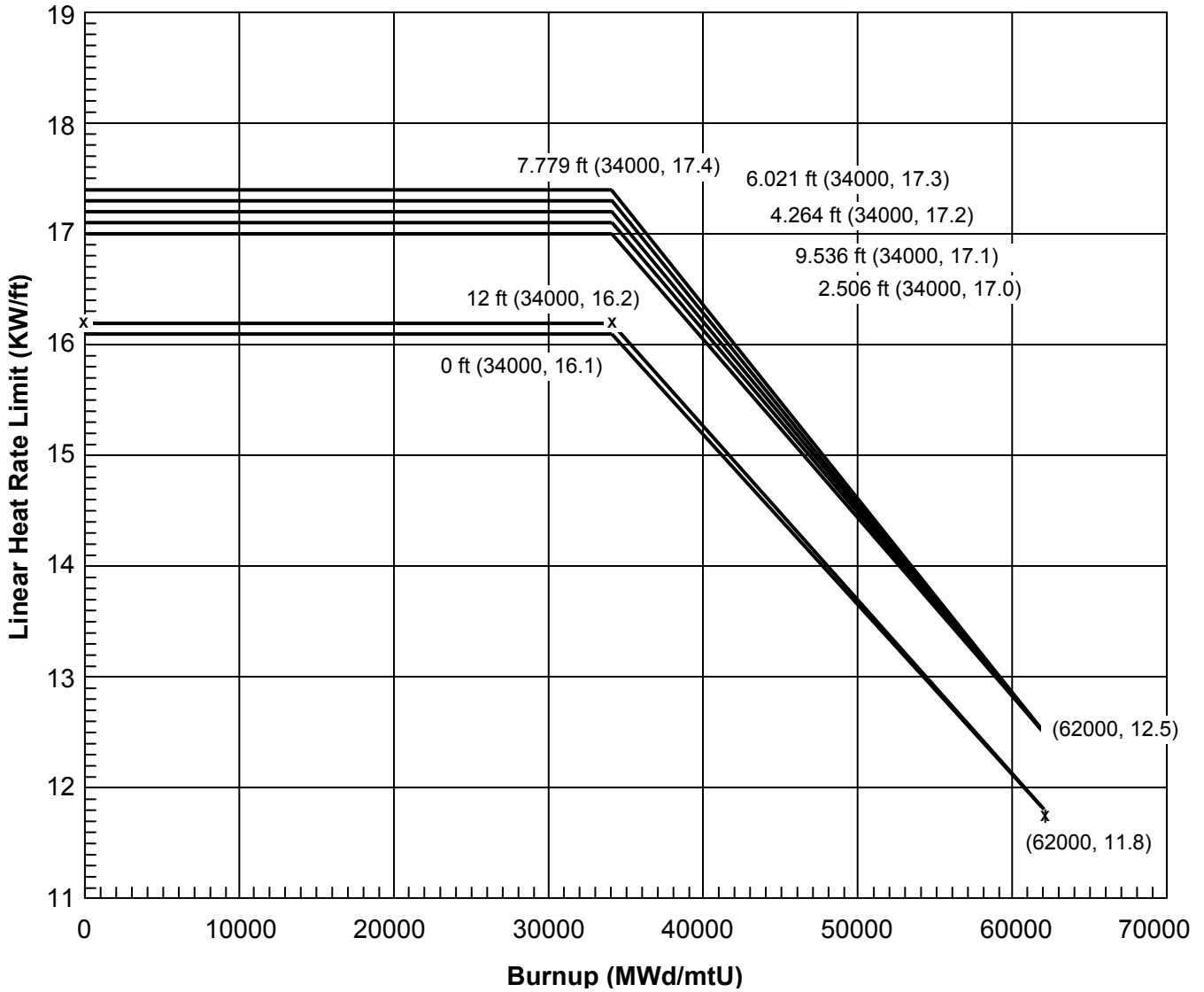
<u>Measurement System</u>	<u>Steady State Value (%)</u>		<u>Maximum Value (%)</u>
	<u>≤ 60 % FP</u>	<u>> 60 % FP</u>	
Full In-core Detector System Setpoint	6.83	5.71	25.00
Minimum In-core Detector System Setpoint	2.78*	1.90*	25.00
Ex-core Power Range NI Channel Setpoint	4.05	1.96	25.00
Measurement System Independent Limit	7.50	4.92	25.00

* Assumes that no individual long emitter detector affecting the minimum in-core tilt calculation exceeds 73% sensitivity depletion. The setpoint must be reduced to 1.50% (power levels > 60% FP) and to 2.19% (power levels ≤ 60% FP) at the earliest time-in-life that this assumption is no longer valid.

Figure 9A

LOCA Linear Heat Rate Limits for Mark-B-HTP Fuel

(Figure is referred to by Technical Specification 3.1.8 and 3.2.5)



DNB Power Peaking Factors

(Limits are referred to by Technical Specification 3.1.8 and 3.2.5)

The following total power peaking factors define the Maximum Allowable Peaking (MAP) limits to protect the initial conditions assumed in the DNB Loss of Flow transient analysis. The total power peaking factors for the Mark-B-HTP fuel are provided. The total power peaking factors for IC-DNB 4-pump and 3-pump are identical; hence one set of IC-DNB values are provided for both 4-pump and 3-pump operation.

IC-DNB Total Power Peaking Factors

Mark-B-HTP								
Axial Peak	x/L	IC MAP Limits	Axial Peak	x/L	IC MAP Limits	Axial Peak	x/L	IC MAP Limits
1.1	0.01	2.08970	1.4	0.01	2.68281	1.7	0.01	2.74462
	0.14	2.09061		0.14	2.58266		0.14	2.58449
	0.20	2.09081		0.20	2.64487		0.20	2.65108
	0.30	2.09080		0.30	2.74565		0.30	2.75329
	0.40	2.09048		0.40	2.78466		0.40	2.82309
	0.50	2.09030		0.50	2.69263		0.50	2.86702
	0.60	2.08995		0.60	2.58415		0.60	2.79623
	0.70	2.08979		0.70	2.49099		0.70	2.70161
	0.80	2.08866		0.80	2.37534		0.80	2.58298
	0.89	2.04041		0.89	2.30086		0.89	2.50578
0.99	1.94602	0.99	2.21159	0.99	2.41376			
1.2	0.01	2.38393	1.5	0.01	2.70611	1.8	0.01	2.76248
	0.14	2.38637		0.14	2.58407		0.14	2.58536
	0.20	2.38711		0.20	2.64723		0.20	2.65100
	0.30	2.38666		0.30	2.74950		0.30	2.75344
	0.40	2.38616		0.40	2.81333		0.40	2.82636
	0.50	2.38612		0.50	2.77586		0.50	2.87190
	0.60	2.38553		0.60	2.66315		0.60	2.85278
	0.70	2.30194		0.70	2.56832		0.70	2.75823
	0.80	2.20190		0.80	2.44935		0.80	2.64208
	0.89	2.13510		0.89	2.37414		0.89	2.56412
0.99	2.04448	0.99	2.28275	0.99	2.47374			
1.3	0.01	2.66050	1.6	0.01	2.72554	1.9	0.01	2.78038
	0.14	2.58201		0.14	2.58400		0.14	2.58548
	0.20	2.64238		0.20	2.64915		0.20	2.65223
	0.30	2.70551		0.30	2.75237		0.30	2.75356
	0.40	2.68966		0.40	2.81854		0.40	2.82802
	0.50	2.59373		0.50	2.84445		0.50	2.87614
	0.60	2.49505		0.60	2.73470		0.60	2.89110
	0.70	2.40470		0.70	2.63922		0.70	2.80738
	0.80	2.29341		0.80	2.51853		0.80	2.69523
	0.89	2.22210		0.89	2.44208		0.89	2.61744
0.99	2.13400	0.99	2.34902	0.99	2.52919			

Notes

1. The values above are not error corrected.
2. The values above were generated using SCD methods which incorporate a 3.8% radial peak uncertainty in the DNBR design limit. Therefore, the above IC MAP limits can be compared to predicted peaks without the addition of up to 3.8% in radial peak calculation uncertainty. These limits, however, do not incorporate any grid bias uncertainty.
3. The present T-H methodology allows for an increase in the design radial-local peak for power levels below 100% full power. The equations defining the multipliers are as follows:

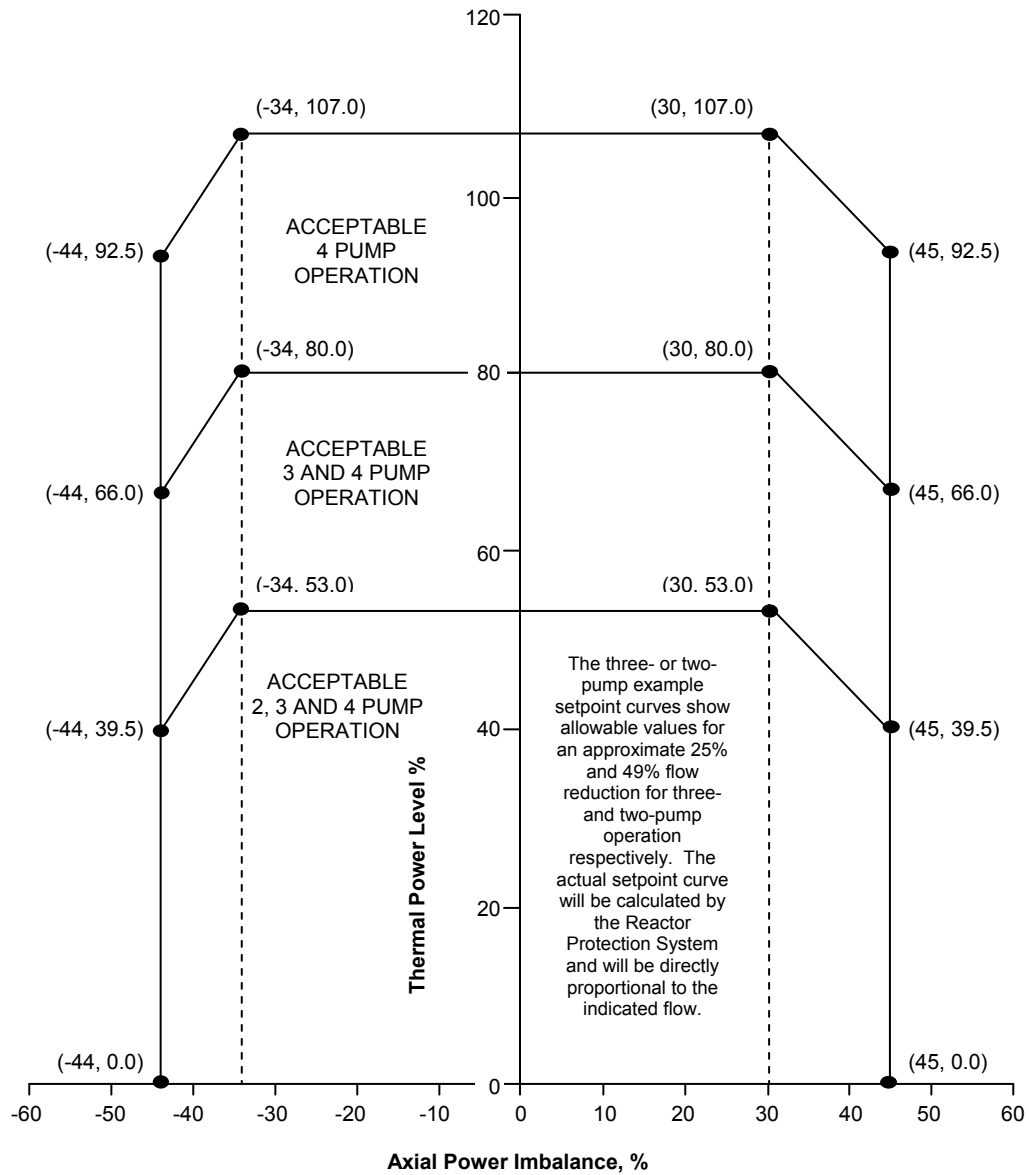
	$P/P_m = 1.00$	$P/P_m < 1.00$
MAP Multiplier	1.0	$1 + 0.3(1 - P/P_m)$

Where P = core power fraction, and
 P_m = 1.00 for 4-pump operation, or
 = 0.75 for 3-pump operation

Figure 10

Reactor Protection System Maximum Allowable Setpoints for Axial Power Imbalance

(Figure is referred to by Technical Specification 2.1.1.1, 2.1.1.2, and 3.3.1)

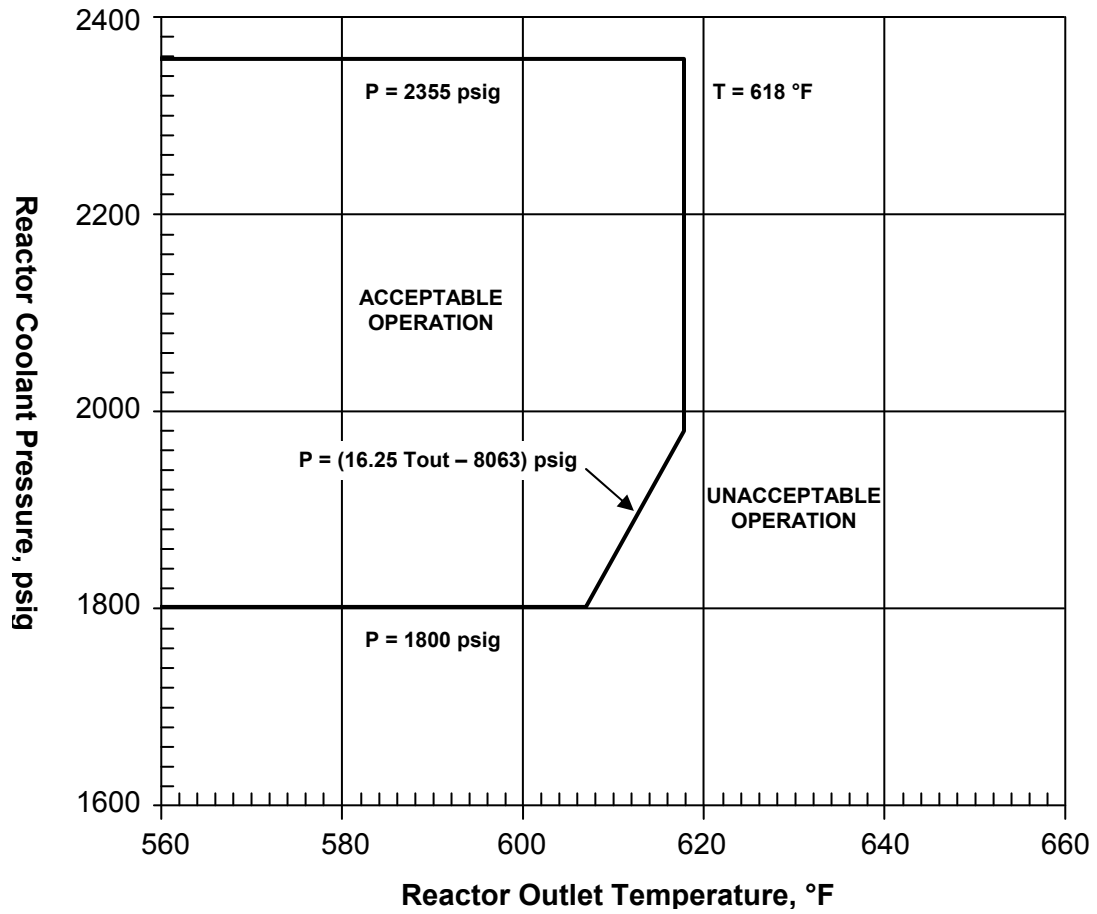


	Flux / Flow Setpoint (% Power / % Flow)
Four Pump Operation	1.07
Three Pump Operation	1.07
Two Pump Operation	1.07

Figure 11

Reactor Protection System Variable Low Pressure Temperature Envelope Setpoints

(Figure is referred to by Technical Specification 3.3.1)



**RCS Pressure, Temperature, and Flow
DNB Surveillance Limits**

(Limit is referred to by Technical Specification 3.4.1)

	Four-Pump Operation	Three-Pump Operation	Two-Pump Operation
Minimum RCS Hot Leg Pressure (psig) ^{Note 1}	2082.2	2081.2 ^{Note 4} 2120.4 ^{Note 5}	2118.1
Maximum RCS Hot Leg Temperature (°F) ^{Note 2}	602.6	602.9	603.15
Minimum RCS Total Flow (Mlb _m /hr) ^{Note 3}	143.36 ^{Note 6}	106.46 ^{Note 7}	70.64 ^{Note 8}
	138.01 ^{Note 9}	102.45 ^{Note 9}	67.96 ^{Note 9}

Note 1 -- Using individual indications P1021, P1023, P1038 and P1039 (or equivalent) from the plant computer.

Note 2 -- Using individual indications T1011NR, T1014NR, T1039NR, T1042NR, T1012, T1013, T1040 and T1041 or averages TOUTA, XTOUTA, TOUTB, XTOUTB, TOUT, XTOUT from the plant computer.

Note 3 -- Using indication WRCFT (or equivalent) from the plant computer, and can be linearly interpolated between these values provided the T_{ave} versus Power level curve is followed.

Note 4 -- Applies to the RCS loop with two RCPs operating.

Note 5 -- Applies to the RCS loop with one RCP operating.

Note 6 -- For $T_{cold} = 556.57$ °F.

Note 7 -- For $T_{cold} = 556.3$ °F.

Note 8 -- For $T_{cold} = 556.1$ °F.

Note 9 -- For $T_{cold} = 580$ °F.

RCS Loops – Mode 1 and Mode 2

(Limit is referred to by Technical Specification 3.4.4)

	Nominal Operating Power Level (% Power)
Four Pump Operation	100
Three Pump Operation	75
Two Pump Operation*	49

* Technical Specification 3.4.4 does not allow indefinite operation in Modes 1 and 2 with only two pumps operating.

Refueling Boron Concentration

(Limit is referred to by Technical Specification 3.9.1)

The minimum required boron concentration (which includes uncertainties) for use during refueling as a function of EFPD is 2386 ppm.