

WOLF CREEK

NUCLEAR OPERATING CORPORATION

Stephen E. Hedges
Site Vice President

December 28, 2011
WO 11-0093

U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555

- Reference: 1) Letter WO 11-0024, dated May 18, 2011, from S. E. Hedges, WCNOC, to USNRC
- 2) Letter WO 11-0078, dated September 29, 2011, from S. E. Hedges, WCNOC, to USNRC
- Subject: Docket No. 50-482: Licensee Event Report 2011-004-02, "Automatic Safety Injection Actuation Due to Operating Crew Failure to Follow Procedure"

Gentlemen:

Reference 1 submitted Licensee Event Report (LER) 2011-004-00, "Automatic Safety Injection Actuation Due to Operating Crew Failure to Follow Procedure," which described an event involving a safety injection actuation and steam line isolation on March 19, 2011, when a main steam isolation valve was opened. Reference 2 provided supplemental LER 2011-004-01 to indicate that this event is not reportable in accordance with 10 CFR 50.73(a)(2)(v)(D). This supplement reinstates reporting this event in accordance with 10 CFR 50.73(a)(2)(v) and includes reporting in accordance with 10 CFR 50.73(a)(2)(i)(B) for entry into Limiting Condition for Operation (LCO) 3.0.3 for greater than one hour.

This letter contains no commitments. If you have any questions concerning this matter, please contact me at (620) 364-4190, or Mr. Gautam Sen at (620) 364-4175.

Sincerely,


Stephen E. Hedges

SEH/rlt

Enclosure

cc: E. E. Collins (NRC), w/e
J. R. Hall (NRC), w/e
N. F. O'Keefe (NRC), w/e
Senior Resident Inspector (NRC), w/e



1. FACILITY NAME: WOLF CREEK GENERATING STATION

2. DOCKET NUMBER: 05000 482

3. PAGE: 1 OF 6

4. TITLE: Automatic Safety Injection Actuation Due to Operating Crew Failure to Follow Procedures

5. EVENT DATE			6. LER NUMBER			7. REPORT DATE			8. OTHER FACILITIES INVOLVED	
MONTH	DAY	YEAR	YEAR	SEQUENTIAL NUMBER	REV NO.	MONTH	DAY	YEAR	FACILITY NAME	DOCKET NUMBER
3	19	2011	2011	004	02	12	28	2011	FACILITY NAME	05000
									FACILITY NAME	DOCKET NUMBER
										05000

9. OPERATING MODE: 3	11. THIS REPORT IS SUBMITTED PURSUANT TO THE REQUIREMENTS OF 10 CFR§: (Check all that apply)									
10. POWER LEVEL: 0	<input type="checkbox"/>	20.2201(b)	<input type="checkbox"/>	20.2203(a)(3)(i)	<input type="checkbox"/>	50.73(a)(2)(i)(C)	<input checked="" type="checkbox"/>	50.73(a)(2)(vii)	<input type="checkbox"/>	50.73(a)(2)(viii)(A)
	<input type="checkbox"/>	20.2201(d)	<input type="checkbox"/>	20.2203(a)(3)(ii)	<input type="checkbox"/>	50.73(a)(2)(ii)(A)	<input type="checkbox"/>	50.73(a)(2)(viii)(B)	<input type="checkbox"/>	50.73(a)(2)(ix)(A)
	<input type="checkbox"/>	20.2203(a)(1)	<input type="checkbox"/>	20.2203(a)(4)	<input type="checkbox"/>	50.73(a)(2)(ii)(B)	<input type="checkbox"/>	50.73(a)(2)(ix)(B)	<input type="checkbox"/>	50.73(a)(2)(x)
	<input type="checkbox"/>	20.2203(a)(2)(i)	<input type="checkbox"/>	50.36(c)(1)(i)(A)	<input type="checkbox"/>	50.73(a)(2)(iii)	<input type="checkbox"/>	50.73(a)(2)(x)	<input type="checkbox"/>	73.71(a)(4)
	<input type="checkbox"/>	20.2203(a)(2)(ii)	<input type="checkbox"/>	50.36(c)(1)(ii)(A)	<input checked="" type="checkbox"/>	50.73(a)(2)(iv)(A)	<input type="checkbox"/>	73.71(a)(5)	<input type="checkbox"/>	OTHER
	<input type="checkbox"/>	20.2203(a)(2)(iii)	<input type="checkbox"/>	50.36(c)(2)	<input checked="" type="checkbox"/>	50.73(a)(2)(v)(A)	<input type="checkbox"/>	Specify in Abstract below or in NRC Form 366A		
	<input type="checkbox"/>	20.2203(a)(2)(iv)	<input type="checkbox"/>	50.46(a)(3)(ii)	<input checked="" type="checkbox"/>	50.73(a)(2)(v)(B)				
	<input type="checkbox"/>	20.2203(a)(2)(v)	<input type="checkbox"/>	50.73(a)(2)(i)(A)	<input checked="" type="checkbox"/>	50.73(a)(2)(v)(C)				
	<input type="checkbox"/>	20.2203(a)(2)(vi)	<input checked="" type="checkbox"/>	50.73(a)(2)(i)(B)	<input checked="" type="checkbox"/>	50.73(a)(2)(v)(D)				

12. LICENSEE CONTACT FOR THIS LER

FACILITY NAME: Gautam Sen, Manager Regulatory Affairs

TELEPHONE NUMBER (Include Area Code): (620) 364-4175

13. COMPLETE ONE LINE FOR EACH COMPONENT FAILURE DESCRIBED IN THIS REPORT

CAUSE	SYSTEM	COMPONENT	MANUFACTURER	REPORTABLE TO EPIX	CAUSE	SYSTEM	COMPONENT	MANUFACTURER	REPORTABLE TO EPIX

14. SUPPLEMENTAL REPORT EXPECTED: YES (If yes, complete 15. EXPECTED SUBMISSION DATE) NO

15. EXPECTED SUBMISSION DATE: MONTH: DAY: YEAR:

ABSTRACT (Limit to 1400 spaces, i.e., approximately 15 single-spaced typewritten lines)

On March 19, 2011 at 0000 Central Daylight Time (CDT), the unit was taken offline for the start of a refueling outage. At 0404 CDT with the plant in Mode 3, while opening the "C" main steam isolation valve (MSIV), a safety injection (SI) actuation and steam line isolation occurred. A momentary large steam flow and pressure drop were observed in the affected steam generator. The pressure drop was rapid enough to actuate all three rate-sensitive low steam generator pressure bistables based on rate alone, with the lowest steam pressure still well above the setpoint. The low steam generator pressure bistables cleared prior to MSIV closure.

Control room operators utilized procedure EMG E-0, "Reactor Trip or Safety Injection," at the initiation of the event and EMG ES-03, "SI Termination," to terminate the SI. The SI and steam line isolation resulted in actuation of both trains of Emergency Core Cooling Systems. The steam line isolation signal closed the only open MSIV. Both diesel generators started and operated in standby mode without tying to the engineered safety features busses. All control rods were previously inserted as part of the controlled shutdown; however, the SI actuation resulted in opening of the reactor trip breakers. Operator action terminated the SI into the Reactor Coolant System (RCS) prior to pressurizer overfill at 0411 CDT.

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PLANT CONDITIONS PRIOR TO EVENT

Mode 3

On March 19, 2011 at 0000 CDT, the unit was taken offline for the start of a refueling outage. At 0054 CDT the unit entered Mode 3. No inoperable systems, structures, or components (SSCs) contributed to this event on March 19, 2011.

EVENT DESCRIPTION

On March 19, 2011, with reactor power less than 25 percent, after transitioning from procedure GEN 00-004, "Power Operation," to GEN 00-005, "Minimum Load to Hot Standby," control room operators implemented procedure SYS AE-200, "Feedwater Preheating During Plant Startup and Shutdown," for establishing the feedwater preheating system [EIIS codes: SB] for plant cooldown. At 0100 CDT, following Mode 3 entry, the main steam isolation valves (MSIVs) [EIIS codes: SB, ISV] were closed to terminate a cooldown of the reactor coolant system (RCS) [EIIS codes: AB].

Closing the MSIVs to stop the cooldown isolated main steam to secondary systems. The "A" main feedwater pump (MFP) [EIIS codes: SB, P] had not been tripped when the MSIVs were closed. The MFP was subsequently tripped during warmup of the main steam lines for opening the MSIVs. This condition contributed to the inadequate warming of the steam lines.

Procedure SYS AB-120, "Main Steam and Steam Dump Startup and Operation," was implemented for opening the MSIVs when it was determined to continue with the plant cooldown on the steam dump valves to establish the preferred cooldown configuration. All four MSIV bypass valves were opened to warm and pressurize the main steam header. The procedure specifies to ensure the differential pressure across the MSIVs is less than 20 psid using temporary gauges. The procedure indicates that temporary gauges with a range of 0 – 300 psig be installed. This procedure step was marked as "not applicable" since steam generator pressure was approximately 1100 psig and the range of the temporary gauges was much less than current plant conditions. The differential pressure across the MSIVs was determined to be less than 20 psid across the valves using control room installed instrumentation (AB PI-507 and steam generator pressures).

At 0404 CDT, while opening the "C" MSIV, a safety injection (SI) actuation and steam line isolation occurred. A momentary large steam flow and pressure drop were observed in the affected steam generator. The pressure drop was rapid enough to actuate all three rate-sensitive low steam generator pressure bistables based on rate alone, with the lowest steam pressure still well above the setpoint. The low steam generator pressure bistables cleared prior to MSIV closure.

Control room operators utilized procedure EMG E-0, "Reactor Trip or Safety Injection," at the initiation of the event and EMG ES-03, "SI Termination," to terminate the SI. The SI and steam line isolation resulted in actuation of both trains of Emergency Core Cooling Systems (ECCS) [EIIS codes: BQ/BP] and injection into the reactor vessel [EIIS codes: AB, RPV]. The steam line isolation signal closed the only open MSIV. Both diesel generators [EIIS codes: EK] started and operated in standby mode without tying to the engineered safety features busses [EIIS codes: EB, BU]. All control rods were previously inserted as part of the controlled shutdown; however, the SI actuation resulted in opening of the reactor trip breakers. Operator action terminated the SI into the RCS prior to pressurizer overfill at 0411 CDT.

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Subsequent review determined that when the "C" MSIV was opened, temperature points from the plant computer for the main steam line were indicating an average temperature of 533.9 degrees F. The steam table pressure conversion for this temperature is approximately 900 psig. When the MSIV was opened existing steam generator pressures were approximately 1100 psig, which equates to a differential pressure of approximately 200 psig across the MSIVs.

BASIS FOR REPORTABILITY

This event is reportable pursuant to 10 CFR 50.73(a)(2)(iv)(A) as an event or condition that resulted in a valid automatic actuation of systems listed in paragraph (a)(2)(iv)(B) of this section of 10 CFR 50.73. The actuation was not part of a pre-planned sequence during testing or reactor operation.

Control room operators utilized procedure EMG E-0, "Reactor Trip or Safety Injection," at the initiation of the event and EMG ES-03, "SI Termination," to terminate the SI. The actions of these procedures result in the operators performing a manual reset of SI. The manual reset of SI following a 60 second time delay, in conjunction with Reactor Trip, P-4 interlock, generates an automatic block of SI. Manual reset of SI is necessary to restore the actuated equipment to standby as appropriate. TS 3.3.2, Function 1.b, Safety Injection – Automatic Actuation Logic and Actuation Relays, requires 2 channels operable in Modes 1, 2, and 3. Once SI is blocked, automatic actuation of SI cannot occur until the reactor trip breakers have been manually closed. The reactor trip breakers were closed 2 hours and 39 minutes after the initiation of the event. The manual reset of SI to terminate the safety injection is necessary to prevent overfilling the pressurizer when a steam line break was not present. However, this results in blocking both channels of SI automatic actuation logic. LER 2011-004-00 reported this event under 10 CFR 50.73(a)(2)(v)(D) as an event or condition that could have prevented the fulfillment of the safety function of structures or systems that are needed to mitigate the consequences of an accident. LER 2011-004-01 provided a supplement that retracted reporting this event under 10 CFR 50.73(a)(2)(v)(D). In subsequent discussions with NRC personnel, it was determined that this event does meet the criterion for reporting under 10 CFR 50.73(a)(2)(v) since the blocking of both automatic SI actuation trains resulted in the inoperability of the actuation trains and therefore would not have been capable of performing its intended safety function as defined in the Updated Safety Analysis Report.

This event is also reportable under 10 CFR 50.73(a)(2)(i)(B) as an operation or condition prohibited by TSs for entry into LCO 3.0.3 for greater than 1 hour.

This event is also reportable under 10 CFR 50.73(a)(2)(vii) as an event where a single cause resulted in two independent trains or channels to become inoperable in a single system designed to mitigate the consequences of an accident. The manual reset of SI is a single action taken that results in the automatic block of both channels of the SI actuation logic.

An initial 50.72 notification (EN 46685) was made under 10 CFR 50.72(b)(2)(iv)(A) for an event that resulted in an ECCS discharge into the RCS as a result of a valid signal. A followup notification was made to indicate that the event was reportable under 10 CFR 50.72(b)(3)(iv)(A) as an event that results in a valid actuation of the Reactor Protection System, ECCS, and emergency ac power systems, and 10 CFR 50.72(b)(3)(v) as an event that could have prevented the fulfillment of the safety function of SSCs that are needed to mitigate the consequences of an accident.

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ROOT CAUSE

The root cause of this event was the failure of the operating crew to follow procedure SYS AB-120. The operating crew did not follow the guidance in procedure AP 15C-002, "Procedure Use and Adherence," when a SYS AB-120 step that was tied to a precaution and limitation step was marked "not applicable." Because the SYS AB-120 procedural guidance was not followed, a SI occurred when the "C" MSIV was opened. Differential pressure across the valves was not equalized and was greater than 20 psid.

The gauges available in the control room did not provide the required resolution to ensure 20 psid had been reached. Assumptions were made without utilizing the steam tables to validate whether the 20 psid had been reached. Instead of following procedural guidance the crew was influenced by the previous performance (October 15, 2010) of SYS AB-120, which opened the MSIVs at approximately 30 psid even though the plant conditions were different.

A contributing cause was procedure SYS AB-120 did not provide the operating crew with the necessary guidance (e.g. time, temperature, and condensate removal) for ensuring main steam lines were adequately warmed prior to opening the MSIVs. SYS AB-120 provides instructions for warmup of the main steam system, opening the MSIVs, aligning the steam dump system for operation, and the use of auxiliary medium on the MSIVs. The procedure step for installing the gauge prior to opening the "C" MSIV did not meet the operating criteria established because it was not written for the plant conditions that existed (1100 psig).

A second contributing cause was the operations management oversight individual did not challenge the crew when problems were encountered; instead he allowed them to proceed without involving additional plant personnel. The principal function of the oversight manager is to challenge the evolution if problems are encountered. The operations management oversight was present for the plant cooldown; however, the oversight manager stepped out of the primary role to facilitate moving forward instead of stopping when problems were encountered.

A third contributing cause for this event was the guidance in procedure SYS AE-200 did not clearly state that the main steam flow to feedwater heaters was to be adjusted using the controller setpoint which contributed to the cooldown requiring MSIV closure. The procedure directs the controller be placed in automatic control and indicates that adjustment of the setpoint is allowed if the feedwater heater temperature limit is approached. Adjustment of the setpoint is performed with the controller in automatic by using the setpoint control thumbwheel.

CORRECTIVE ACTIONS

Transient event walkdowns of RCS equipment in containment and secondary plant equipment were performed. Actions were taken to resolve discrepancies identified from these walkdowns.

Essential reading was issued on March 25, 2011 to operations personnel for procedure AP 15C-002, "Procedure Use and Adherence," and the acceptable use of identifying steps as "not applicable" during procedure usage.

Procedure AP 15C-002, "Procedure Use and Adherence," was benchmarked against current industry guidance on procedure adherence including the use of "not applicable." The benchmarking results indicated that the WCNOG practices were consistent with industry practices. Accountability on procedure use and adherence was reinforced through evaluation of operating crews on the simulator and during normal plant operations. These actions were completed on November 22, 2011.

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Revision 28 (May 23, 2011) and On-the-Spot Change (OTSC) 11-0146 (May 24, 2011) to procedure SYS AB-120, "Main Steam and Steam Dump Startup and Operation," provide guidance for the appropriate thermal conditions (i.e., temperature, pressure, differential pressure) that must be met before opening an MSIV. These changes also identify the appropriate instrumentation to be used based on plant conditions.

Procedure SYS AE-200, "Feedwater Preheating During Plant Startup and Shutdown," was revised on April 12, 2011 to clarify the notes and step to ensure the controller is maintained in automatic when adjustments are required to prevent exceeding feedwater heater differential temperatures.

SAFETY SIGNIFICANCE

The SI produced a transient to the RCS. All major equipment functioned within its design capability. The SI transient is bounded by accident analyses discussed in Updated Safety Analysis Report (USAR) Section 15.5.1, "Inadvertent Operation Of the Emergency Core Cooling System During Power Operation." The primary concern that results from an inadvertent actuation of the ECCS at power is that associated with pressurizer overfill. The pressurizer water volume increases as a result of the SI flow. This may eventually lead to filling of the pressurizer and subsequent water relief through the safety or relief valves. The passing of liquid through the pressurizer safety or relief valves could result in rupture of the pressurizer relief tank rupture disks, spilling radioactive coolant into the containment building, thereby escalating a Condition II event to a Condition III or IV event. To prevent the pressurizer from becoming water-solid operator action is ultimately required to terminate SI or mitigate the consequences of this event. In this specific event, the SI occurred with the reactor in shutdown conditions, all rods inserted, and shutdown boration completed. Turbine trip signals and reactor trip signals were generated, but both the turbine and reactor were shutdown. The pressurizer power operated relief valves (PORVs) operated to mitigate the pressurizer insurge pressure transient. Operator action terminated the SI into the RCS prior to pressurizer overfill. Pressurizer level reached 87.5 percent during the SI event. As such, this transient was bounded by the analysis described in USAR Section 15.5.1.

When the "C" MSIV was opened, a rapid decrease in main steam line pressure occurred. The transient is bounded by the analyzed condition of a steam line break (SLB) while the plant is at hot zero power (HZP). The postulated SLB at HZP accident analysis most closely represents the plant conditions that existed during this event. Opening the MSIV gave a rapid change in steam header pressure, as would a SLB and the plant was at HZP conditions. The postulated SLB at HZP accident analysis results in a rapid loss of pressure and an excessive cooldown of the RCS. The postulated SLB at HZP as analyzed in USAR Section 15.1 represents a greater than 100 degree/hour cooldown, and it also assumes that the most reactive control rod is stuck out. The SLB at HZP bounds the transient for this event since the reactor was shut down with all control rods inserted and boron had been added during the shutdown. There was no actual failure of the main steam line piping. An actual SLB event from HZP would produce a cooldown in excess of 150 degrees/hour. For this event the cooldown was only four degrees on the affected loop and there was no prolonged steam flow. Steam generator pressure was restored when the MSIV reclosed as a result of the steam line isolation signal.

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OPERATING EXPERIENCE/PREVIOUS EVENTS

LER 2010-012-00: On October 17, 2010 at 0952 CDT, Wolf Creek Generating Station was at approximately 15 percent power during a startup when a turbine trip and feedwater isolation signal occurred due to high-high steam generator level. The MSIVs were closed due to cooldown after the plant trip and were subsequently reopened. Difficulty was experienced in getting the MSIVs to immediately reopen when the handswitches were first depressed. It was noted at the time that procedure SYS AB-120 did not include guidance for opening a MSIV at normal operating temperature and pressure.

On March 5, 2010, while in Mode 4, a feedwater isolation signal occurred due to a high water level on "A" steam generator. The high water level occurred due to swell caused by opening the "A" MSIV. As a result of this event, changes were made to procedure SYS AB-120 to use temporary gauges with higher accuracy to ensure differential pressure limits were actually met and to lower steam generator levels prior to opening the MSIV. At the time the MSIV was opened, the RCS was in heatup. If the RCS temperature is not held constant for some period of time, equalization of pressure cannot be assured.

LER 85-021-00: On April 28, 1985, an engineered safety features actuation occurred resulting in a safety injection actuation and main steam line isolation. The initiating signal was low steam line pressure on the "D" steam generator. The cause of the low steam line pressure signal was determined to be an anticipatory trip generated by the rate sensitive steam generator pressure circuitry due to a decrease in steam line pressure when a MSIV was opened before pressure was equalized through the MSIV bypass valves. At the time of the event, the plant was in Mode 3 prior to initial criticality.

Prior corrective actions for the above events did not adequately assess the necessary procedural guidance and instrumentation necessary to prevent an increased potential for a safety injection to occur. The corrective actions from the March 5, 2010 event primarily focused on steam generator water level and preventing a reoccurrence of a feedwater isolation when opening a MSIV.