3.2 Run1ga - Side

The run1ga is a 30-foot impact followed by a crush impact, with the crush plate centered above the CV flange. The run1g 30-foot impact restart file was used and the crush plate was moved during the restart phase so that its centerline was approximately above the CV flange. The 30-foot impact was from time 0.0 to 0.0085 sec. The crush plate translation to center it above the CV flange was from time 0.0085 sec to 0.0086 sec. The run1ga crush occurred from 0.0086 sec to 0.027 sec. Therefore, the 30-foot impact results for this run would be the Section 3.1, 30-foot results for run1g, and the crush results for run 1ga (offset crush) are presented in this section.

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Figure 3.2.1 shows the configuration of the model after the crush plate was moved above the CV flange (time = 0.0086 sec). Figure 3.2.2 shows the model configuration after the run1ga crush impact. Figure 3.2.3 through Figure 3.2.6 show enlarged views in the lid and bottom regions of the package assembly.

Figure 3.2.7 shows that the maximum strain in the CV body for the run1ga crush impact is 0.0348 in/in. The effective plastic strain in the CV lid is 0.0002 in/in and is shown in Figure 3.2.8. The CV nut ring remains elastic for the crush impact of run1ga.

The maximum effective plastic strain in the drum angle is shown in Figure 3.2.9 to be 0.1058 in/in. The maximum effective plastic strain in the drum is 0.3818 in/in and occurs in the top drum roll near the crush plate (Figure 3.2.10).

Figure 3.2.11 gives the maximum effective plastic strain in the lid to be 1.1345 in/in. This is a relatively high strain level and the maximum occurs near the stud hole at the 90° position (initially along Y axis). Another high region of strain is near the upper stud nearest the crush plate. The solid elements (used for contact bearing on the studs) around the stud holes show effective plastic strain maximum of 0.8745 in/in. The membrane effective plastic strain in the shell elements is a maximum of 0.8057 in/in and is highly localized near the stud hole at the 90° position. Some tearing of the lid could occur in the lid hole at the 90° position and at the lid hole nearest the crush plate (180°).

Figure 3.2.12 shows the effective plastic strain levels in the drum studs. The maximum is shown to be 0.5207 in/in and occurs in the stud at the 90° position. From Figure 3.2.12 it is seen that the elevated strain occurs near the outer extreme of the stud, and that the through thickness strain levels between 0.3170 and 0.3802 in/in exist.

A study of the timing of the elevated effective plastic strain levels in the lid and the drum studs shows that the lid reaches failure magnitudes before the studs. At the stud hole in the drum lid nearest the crush plate (180°), the bending strain crosses the 0.57 in/in

strain at about 0.0122 seconds in the crush impact. The membrane strain in the lid elements at 180° reaches a maximum of .5295 in/in. The stud at 180° does not experience elevated strain levels (final maximum in this stud is 0.17 in/in). So at the 180° position, only the lid experiences relatively high levels of effective plastic strain.

At the 90° position in the lid, the membrane effective plastic strain exceeds the 0.57 in/in level near 0.0164 seconds in the crush impact. The surface maximum effective plastic strain exceeds 0.57 in/in at about 0.0161 seconds, slightly ahead of the membrane. At time 0.0164 seconds, the effective plastic strain levels in the stud at 90° is about 0.35 in/in maximum, with the through thickness levels between 0.104 in/in to 0.136 in/in. Therefore, at the 90° position, the lid reaches the failure level of 0.57 in/in before the stud.

From this timing data, it is shown that the lid would reach failure levels in bending and membrane before the stud effective plastic strain levels become relatively high. Therefore, it would be expected that the lid would locally tear before the bolting reached elevated effective plastic strain levels, thus possibly reducing the loadings on the studs. Due to the extent of the relatively high levels of effective plastic strain in the drum lid, it would be expected that any lid tearing would be localized and that the large washers would restrain the drum lid.

The effective plastic strain contour patterns for the other components are not shown in figures. The maximum effective plastic strain in the drum bottom is 0.2444 in/in; in the liner it is 0.2853 in/in; in the lid stiffener it is 0.1116 in/in; in the drum stud nuts it is 0.0103 in/in; in the drum stud washers it is 0.1685 in/in and in the plug liner it is 0.2181 in/in.

The kinetic energy time history for the crush plate impact is shown in Figure 3.2.13. The X velocity time history is shown in Figure 3.2.14.

The lid separation time history is shown in Figure 3.2.15 (nodes defined in Figure 3.1.30). From Figure 3.2.15 it is seen that the spike separation of just under 0.004 inches can occur with a final nominal separation of less than 0.002 inches expected.

The kaolite thickness time histories for the nodes defined in Figure 3.1.32 are given in Figure 3.2.16 for run1ga. The drum diameter time histories are given in Figures 3.2.17 and 3.2.18. The nodes defining this response are shown in Figure 3.1.34. As shown in Figure 3.2.17, the bottom head and the bottom drum roll remain at, or near 30-foot impact diameters for the crush impact. This response is expected as qualitatively shown in Figure 3.2.2. The response in the Y-direction is shown in Figure 3.2.18.

Figure 3.2.19 shows the diameter time history for various locations along the liner length. Figure 3.1.37 and Table 3.1.3 define the locations at which the diameters are obtained.

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Figure 3.2.1 - Run1ga, Crush Impact, Initial Configuration for the Crush Impact



3100 RUN1GA SIDE NOV 2003 KQH Time = 0.027



Figure 3.2.2 - Run1ga, Crush Impact, Configuration of the ES-3100 After the Crush Impact





Figure 3.2.3 - Run1ga, Crush Impact, Configuration of the Lid Region Near the Rigid Plane





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Figure 3.2.6 - Run1ga, Crush Impact, Configuration of the Bottom Near the Crush Plate



Figure 3.2.7 - Run1ga, Crush Impact, Effective Plastic Strain in the CV Body

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3100 RUN1GA SIDE NOV 2003 KQH Time = 0.027 Contours of Effective Plastic Strain max ipt. value min=0, at elem# 51809 max=0.000174097, at elem# 565471

Z



Fringe Levels
1.741 e-004
1.557e-004
1.393e-004
1.219e-004
1.045e-004
8.705e-005
6.364e-005
5.223e-005
1.741e-005
0.000e+000

Figure 3.2.8 - Run1ga, Crush Impact, Effective Plastic Strain in the CV Lid







3100 RUN1GA SIDE NOV 2003 KQH Time = 0.027 Contours of Effective Plastic Strain max ipt. value min=0, at elem# 5297 max=0.381755, at elem# 27171

×-z

Figure 3.2.10 - Run1ga, Crush Impact, Effective Plastic Strain in the Drum



Fringe Levels 5.068e-001 6.419e-002

Part A - Initial Design with Borobond Cylinder

3100 RUN1GA SIDE NOV 2003 KQH Time = 0.027 Contours of Effective Plastic Strain max ipt. value min=0.000971315, at elem# 39669 max=1.13448, at elem# 423891

x^Yz

Figure 3.2.11 - Run1ga, Crush Impact, Effective Plastic Strain in the Lid

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Figure 3.2.12 - Run1ga, Crush Impact, Effective Plastic Strain in the Drum Studs

3100 RUN1GA SIDE NOV 2003 KQH Time = 0.027 Contours of Effective Plastic Strain max ipt. value min=0, at elem# 71878 max=0.520685, at elem# 726501





ringe Levels	
5.207e-001 _	
4.686 c- 001 _	
4.165 c- 001 _	
3.645 c -001 _	
3.124 c -001 _	
2.603 c- 001 _	
2.083e-001 _	
1.562 c- 001 _	
1.041e-001 _	
5.207e-002 _	
.000e+000 _	

Part A - Initial Design with Borobond Cylinder



Figure 3.2.13 - Run1ga, Crush Impact, Kinetic Energy Time History



Figure 3.2.14 - Run1ga, Crush Impact, X Velocity Time History



Figure 3.2.15 - Run1ga, Lid Separation Time History





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Figure 3.2.18 - Run1ga, Drum Dimension Time History in the Y-Direction





Figure 3.2.19 - Run1ga, Liner Diameter Time History

3.3 Run1hl - Side

Run1hl is the lower bounding kaolite run (100°F). It is basically the run1g model, but with kaolite properties of section 2.3.5.2. It is a run with a 4-foot impact (time = 0 to 0.01 seconds), followed by a 30-foot impact (0.01 to 0.02 seconds), followed by a 30-foot crush impact (0.02 to 0.04 seconds), finally followed by a 40-inch punch impact (0.04 to 0.055 seconds). The initial configuration of run1hl is similar to Figure 3.1.1. The configuration after the 4-foot impact is shown in Figure 3.3.1. Figure 3.3.2 and 3.3.3 show the configuration at the extremes of the package.

The CV body undergoes plastic deformation in the 4-foot impact. The effective plastic strain in the CV body is shown in Figure 3.3.4 to have a maximum of 0.0263 in/in. The elevated plastic strain levels are near the CV bottom head. The CV lid and nut ring remain elastic during the 4-foot impact. The plastic strain in other components for the 4-foot impact are given in Table 3.3.1.

Table 3.3.1 - Run1hl, 4-Foot Impact, Effective Plastic Strain Levels in Some Components		
Component Effective Plastic Strain,		
Angle	0.0054	
Drum	0.1561	
Drum Bottom Head	0.0991	
Liner	0.0537	
Lid	0.1320	
Lid Stiffener	0.0001	
Lid Studs	0.0000	
Lid Stud Nuts	0.0000	
Lid Stud Washers	0.0011	
Plug Liner	0.0022	

Figure 3.3.5 shows the final configuration for the run1hl 30-foot impact. Figures 3.3.6 and 3.3.7 show the configurations for the package extremes.

The maximum effective plastic strain due to the 30-foot impact in the CV body is 0.0287 in/in as shown in Figure 3.3.8. The maximum effective plastic strain in the drum lid

is shown to be 0.5180 in/in in Figure 3.3.9. The maximum lid strain is a surface strain at the stud hole nearest the rigid surface (0°). The membrane effective plastic strain component is 0.4026 in/in in the localized region near the stud hole. Effective plastic strain levels in other components for the 30-foot impact are given in Table 3.3.2.

Table 3.3.2 - Run1hl, 30-Foot Impact, Effective Plastic Strain Levels in Some Components		
Component Effective Plastic Strain,		
CV Lid	0.0001	
CV Nut Ring	0.0000	
Angle	0.0777	
Drum	0.2250	
Drum Bottom Head	0.2125	
Liner	0.1800	
Lid Stiffener	0.0118	
Lid Studs	0,1098	
Lid Stud Nuts	0.0000	
Lid Stud Washers	0.0225	
Plug Liner	0.0956	

The final configuration for the crush impact is shown in Figure 3.3.10. The configuration at the package extremes are shown in Figure 3.3.11. The maximum effective plastic strain in the CV body is 0.0287 in/in as shown in Figure 3.3.12. The maximum effective plastic strain in the drum for the crush impact is 0.5309 in/in (surface strain). The maximum in the drum occurs near the angle on the crush plate side of the drum as shown in Figure 3.3.13. The maximum membrane effective plastic strain at this location is 0.3616 in/in.

The maximum effective plastic strain in the lid is 1.2969 in/in (surface strain) and occurs just below the upper stud hole (hole nearest the crush plate, 180°) as shown in Figure 3.3.14. The maximum membrane effective plastic strain in this region of the lid is 0.8995 in/in. A time line investigation during the crush impact shows that the lid exceeds 0.57 in/in strain in bending at about 0.0228 seconds at the 180° stud hole. The crush impact started at about 0.0200 seconds, so the lid reaches failure level near the start of the crush impact. The membrane levels in the lid reach 0.57 in/in at about 0.0236 seconds.

The elevated effective plastic strain levels in the lid are localized in the region just inboard of the upper stud.

The effective plastic strain in the drum studs is 0.4159 in/in and occurs in the upper stud at the bearing of the lid onto the stud (180°). The elevated strains in the stud are localized on the inner surface. Effective plastic strain levels throughout the thickness of the stud are generally 0.25 in/in or less.

Considering the strain levels in the lid and the studs, some tearing in the lid at the 180° stud hole would be expected. But the tearing would be localized to the stud hole due to the extent of the strain patterns. Failure of the stud to restrain the lid due to this tearing is not expected. The lid stiffener would limit any tearing from the stud at 180° and the large washer would be expected to restrain the lid.

The effective plastic strain in other components due to the crush impact are listed in Table 3.3.3.

Table 3.3.3 - Run1hl, Crush Impact, Effective Plastic Strain Levels in Some Components		
Component Effective Plastic Strain,		
CV Lid	0.0003	
CV Nut Ring	0.0000	
Angle	0.1178	
Drum Bottom Head	0.3342	
Liner	0.2637	
Lid Stiffener	0.0530	
Lid Stud Nuts	0.0007	
Lid Stud Washers	0.0832	
Plug Liner	0,1255	

The final configuration after the punch impact is shown in Figure 3.3.16. The effective plastic strain level in the CV body is shown in Figure 3.3.6. The maximum strain is 0.0299 in/in and is located near the bottom head. The effective plastic strain level in the drum after the punch impact remains at 0.5309 in/in as shown in Figure 3.3.18. The maximum effective plastic strain in the other package components for the punch impact are listed in Table 3.3.4.

Table 3.3.4 - Run1hl, Punch Impact, Effective Plastic Strain Levels in Some Components		
Component Effective Plastic Strain, in		
CV Lid	0.0006	
CV Nut Ring	0.0000	
Angle	0.1178	
Drum Bottom Head	0.3345	
Liner	0.2637	
Lid	1.2971	
Lid Stiffener	0.0530	
Lid Studs	0.4221	
Lid Stud Nuts	0.0007	
Lid Stud Washers	0.0844	
Plug Liner	0.1255	

Figure 3.3.19 shows the lid separation time history for all the impacts. The CV lid separation shows a maximum spike separation of about 0.006 inches occurs during the punch. The spike is a response to the rebounding impact of the CV/weights. An average value of .003 in or less is demonstrated in the response when the solution is stopped.

Figure 3.3.20 shows the time history for the kaolite thicknesses. The nodal locations for nodes shown in Figure 3.3.20 are shown in Figure 3.1.32.

Figure 3.3.21 shows the diameter changes in the drum in the model X direction. Figure 3.3.22 shows the radial changes in the Y direction (normal to the impact directions). The nodes are defined in Figure 3.1.34.

Figure 3.3.23 shows the liner diameter time history. The node pair locations are shown in Figure 3.1.37 and Table 3.1.3.



3100 RUN1HL LOWER BOUND SIDE MAY 2004 K Time = 0.01

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Figure 3.3.1 - Run1hl, 4-Foot Impact, Final Configuration



Figure 3.3.3 - Run1hl, 4-Foot Impact, Configuration in the Bottom

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Figure 3.3.4 - Run1hl, 4-Foot Impact, Effective Plastic Strain in the CV Body

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Figure 3.3.5 - Run1hl, 30-Foot Impact, Final Configuration

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Part A - Initial Design with Borobond Cylinder











Figure 3.3.9 - Run1hl, 30-Foot Impact, Effective Plastic Strain in the Lid

Part A - Initial Design with Borobond Cylinder



Figure 3.3.10 - Run1hl, Crush Impact, Final Configuration

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Figure 3.3.14 - Run1hl, Crush Impact, Effective Plastic Strain in the Lid

3100 RUN1HL LOWER BOUND SIDE MAY 2004 K Time = 0.04 Contours of Effective Plastic Strain max ipt, value min=0, at elem# 71077 max=0.415936, at elem# 730211



Figure 3.3.15 - Run1hl, Crush Impact, Effective Plastic Strain in the Studs





3100 RUN1HL LOWER BOUND SIDE MAY 2004 K Time = 0.055083

Figure 3.3.16 - Run1hl, Punch Impact, Final Configuration









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Figure 3.3.18 - Run1hl, Punch Impact, Effective Plastic Strain in the Drum



Part A - Initial Design with Borobond Cylinder



Figure 3.3.19 - Run1hl, CV Lid Separation Time History

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Time

Figure 3.3.20- Run1hl, Kaolite Thickness Time History













Figure 3.3.23 - Run1hl, Liner Diameter Time History



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3.4 Run1hh - Side

Run1hh is the upper bounding kaolite run(-40°). It is basically the run1g model, but with the upper bound kaolite properties of section 2.3.5.3. It is a run with a 4-foot impact (time = 0 to 0.01 seconds), followed by a 30-foot impact (0.01 to 0.0188 seconds), followed by a 30-foot crush impact (0.0188 to 0.04 seconds), finally followed by a 40-inch punch impact (0.04 to 0.052 seconds).

The final configuration for the 4-foot impact is shown in Figure 3.4.1. Figures 3.4.2 and 3.4.3 show the configuration at the corners of the shipping package. The effective plastic strain in the CV body for the 4-foot impact is shown in Figure 3.4.4. The maximum effective plastic strain is shown to be 0.0298 in/in near the bottom head. The effective plastic strain in other package components for the 4-foot impact are listed in Table 3.4.1.

Table 3.4.1 - Run1hh, 4-Foot Impact, Effective Plastic Strain Levels in Some Components		
Component	Effective Plastic Strain, in/in	
CV Lid	0.0000	
CV Nut Ring	0.0000	
Angle	0.0059	
Drum	0.1170	
Drum Bottom Head	0.1215	
Liner	0.0598	
Lid	0.0860	
Lid Stiffener	0.0000	
Lid Studs	0.0000	
Lid Stud Nuts	0.0000	
Lid Stud Washers	0.0310	
Plug Liner	0.0046	

The final configuration for the 30-foot impact is shown in Figure 3.4.5. Figures 3.4.6 and 3.4.7 show the configuration at the corners of the package. The maximum effective plastic strain for the 30-foot impact in the CV Body is 0.0386 in/in near the bottom head. The maximum effective plastic strain in the drum lid is 0.4073 in/in near the rigid plane.

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Table 3.4.2 - Run1hh, 30-Foot Impact, Effective Plastic Strain Levels in Some Components		
Component	Effective Plastic Strain, in/in	
CV Lid	0.0000	
CV Nut Ring	0.0000	
Angle	0.0622	
Drum	0.2259	
Drum Bottom Head	0.2528	
Liner	0.0970	
Lid Stiffener	0.0069	
Lid Studs	0.1226	
Lid Stud Nuts	0.0000	
Lid Stud Washers	0.0951	
Plug Liner	0.0995	

The effective plastic strain in other components for the 30-foot impact are given in Table 3.4.2.

The final configuration for the crush impact is shown in Figure 3.4.10. The configuration at the extremes of the package are shown in Figure 3.4.11. The maximum effective plastic strain for the crush impact in the CV body is 0.0462 in/in, on the crush plate side near the lid end of the top inner weight as shown in Figure 3.4.12. The maximum effective plastic strain in the drum is 0.2623 in/in near the angle and the rigid plane (Figure 3.4.13). The maximum effective plastic strain in the drum lid is 0.6411 in/in (surface strain), Figure 3.4.14. The maximum occurs at the lid hole for the stud closest to the crush plate(180°). The membrane effective plastic strain is 0.4922 in/in at this location. The effective plastic strain in the studs is 0.1753 in/in as shown in Figure 3.4.3 for the crush impact.

Part A -	Initial	Design	with	Borob	ond C	ylind	er
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Table 3.4.3 - Run1hh, Crush Impact, Effective Plastic Strain Levels in Some Components		
Component	Effective Plastic Strain, in/in	
CV Lid	0.0004	
CV Nut Ring	0.0000	
Angle	0.0816	
Drum Bottom Head	0.2807	
Liner	0.2005	
Lid Stiffener	0.0217	
Lid Stud Nuts	0.0000	
Lid Stud Washers	0.1034	
Plug Liner	0.1258	

The final configuration for the punch impact is shown in Figure 3.4.16. The maximum effective plastic strain in the CV body after the punch impact is shown to be 0.0599 in/in in Figure 3.4.17. The maximum effective plastic strain in the drum is 0.2623 in/in (surface strain) and is located near the angle at the rigid surface. The maximum effective plastic strain in elements local to the punch impact is 0.1382 in/in (surface strain) as shown in the insert in Figure 3.4.18. The maximum effective plastic strain for the lid and other package components at the end of the punch impact are listed in Table 3.4.4.

Table 3.4.4 - Run1hh, Punch Impact, Effective Plastic Strain Levels in Some Components		
Component	Effective Plastic Strain, in/in	
	0.0004	
	0.0004	
CV Nut Ring	0.0000	
Angle	0.0816	
Drum Bottom Head	0.2807	
Liner	0.2027	
Lid	0.6411	
Lid Stiffener	0.0217	
Lid Studs	0.1761	
Lid Stud Nuts	0.0000	
Lid Stud Washers	0.1034	
· Plug Liner	0.1258	

Figure 3.4.19 shows the CV lid separation for all the impacts. A maximum spike for the lid separation of less than 0.008 inches is found. At the end of the impacts, the maximum separation is on the order of 0.006 in, with the response being oscillatory in nature. Average separation of 0.003 inches or less is shown to be expected after the successive impacts.

Figure 3.4.20 shows the drum diameter time history response to the impacts in the X direction (direction of the impacts). Figure 3.4.21 shows the Y direction radial response (normal to the impact direction). The drum nodes are defined in Figure 3.1.34.

The Figure 3.4.22 shows the kaolite thickness time history for the four impacts. Figure 3.1.32 shows the nodal locations.

Figure 3.4.23 shows the liner diameter time history along its length. The nodal pairs are defined in Figure 3.1.37 and Table 3.1.3.



3100 RUN1HH UPPER BOUND SIDE MAY 2004 K Time = 0.01

Figure 3.4.1 - Run1hh, 4-Foot Impact, Final Configuration

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Part A - Initial Design with Borobond Cylinder

Figure 3.4.4 - Run1hh, 4-Foot Impact, Effective Plastic Strain in the CV Body



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Part A - Initial Design with Borobond Cylinder



Figure 3.4.5 - Run1hh, 30-Foot Impact, Final Configuration





Figure 3.4.7 - Run1hh, 30-Foot Impact, Configuration in the Bottom

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Figure 3.4.8 - Run1hh, 30-Foot Impact, Effective Plastic Strain in the CV Body







Figure 3.4.10 - Run1hh, Crush Impact, Final Configuration

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3100 RUN1HH UPPER BOUND SIDE MAY 2004 K Time = 0.04 Contours of Effective Plastic Strain max ipt. value min=0, at elem# 71878 max=0.175321, at elem# 719921





Figure 3.4.15 - Run1hh, Crush Impact, Effective Plastic Strain in the Studs



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Figure 3.4.16 - Run1hh, Punch Impact, Final Configuration

x^Yz

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Figure 3.4.17 - Run1hh, Punch Impact, Effective Plastic Strain in the CV Body





Figure 3.4.18 - Run1hh, Punch Impact, Effective Plastic Strain in the Drum



Figure 3.4.19 - Run1hh, CV Lid Separation Time History











3100 RUN1HH UPPER BOUND SIDE MAY 2004 K



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Figure 3.4.23 - Run1hh, Liner Diameter Time Histories

