1.3 <u>IDENTIFICATION OF AGENTS AND CONTRACTORS</u>

Holtec International is a specialty engineering company with a principal focus on spent fuel storage technologies. Holtec has carried out turnkey wet storage capacity expansions (engineering, licensing, fabrication, removal of existing racks, performance of underwater modifications, volume reduction of the old racks and hardware, installation of new racks, and commissioning of the pool for increased storage capacity) in numerous plants around the world. Over 45 plants in the U.S., Britain, Brazil, Korea, and Taiwan have utilized Holtec's wet storage technology to extend their in-pool storage capacity.

Holtec's corporate engineering consists of experts with advanced degrees (Ph.D.'s) in every discipline germane to the fuel storage technologies, namely structural mechanics, heat transfer, computational fluid dynamics, and nuclear physics. All engineering analyses for Holtec's fuel storage projects (including HI-STORM 100) are carried out in-house.

Holtec International's quality assurance program was originally developed to meet NRC requirements delineated in 10CFR50, Appendix B, and was expanded to include provisions of 10CFR71, Subpart H, and 10CFR72, Subpart G, for structures, systems, and components designated as important to safety. A description of the quality assurance program and its method of satisfying all 18 criteria in 10CFR72, Subpart G, that apply to the design, fabrication, construction, testing, operation, modification, and decommissioning of structures, systems, and components important to safety is provided in Chapter 13.

It is currently planned that the HI-STORM 100 System will be fabricated by U.S. Tool & Die, Inc. (UST&D) of Pittsburgh, Pennsylvania. UST&D is an N-Stamp holder and a highly respected fabricator of nuclear components. UST&D is on Holtec's Approved Vendors List (AVL) and has a quality assurance program meeting 10CFR50 Appendix B criteria. Extensive prototypical fabrication of the MPCs has been carried out at the UST&D shop to resolve fixturing and tolerance issues. If another fabricator is to be used for the fabrication of any part of the HI-STORM 100 System, the proposed fabricator will be evaluated and audited in accordance with Holtec International's quality assurance program described in Chapter 13.

Construction, assembly, and operations on-site may be performed by Holtec or a licensee as the prime contractor. A licensee shall be suitably qualified and experienced to perform selected activities. Typical licensees are technically qualified and experienced in commercial nuclear power plant construction and operation activities under a quality assurance program meeting 10CFR50 Appendix B criteria.

1.4 GENERIC CASK ARRAYS

The HI-STORM 100 System is stored in a vertical configuration. The required center-to-center spacing between the modules (layout pitch) is guided by operational considerations. Tables 1.4.1 and 1.4.2 provide the nominal layout pitch information. Site-specific pitches are determined by practical operation with supporting heat transfer calculations in Chapter 4. The pitch values in Tables 1.4.1 and 1.4.2 are nominal and may be varied to suit the user's specific needs.

Table 1.4.1 provides recommended cask spacing data for array(s) of two by N casks. The pitch between adjacent rows of casks and between each adjacent column of casks are denoted by P_1 and P_2 In Table 1.4.1. There may be an unlimited number of rows. The distance between adjacent arrays of two by N casks (P3) shall be as specified in Table 1.4.1. See Figure 1.4.1 for further clarification. The pattern of required pitches and distances may be repeated for an unlimited number of columns.

For a square array of casks the pitch between adjacent casks may be in accordance with Table 1.4.2. See Figure 1.4.2 for further clarification. The data in Table 1.4.2 provide nominal values for large ISFSIs (i.e., those with hundreds of casks in a uniform layout), where access of feed air to the centrally located casks may become a matter of thermal consideration. From a thermal standpoint, regardless of the size of the ISFSI, the casks should be arrayed in such a manner that the tributary area for each cask (open ISFSI area attributable to a cask) is a minimum of 225 ft². Subsection 4.4.1.1.7 provides the detailed thermal evaluation of the required tributary area. For specific sites, a smaller tributary area can be utilized after appropriate thermal evaluations for the site-specific conditions are performed.

Table 1.4.1

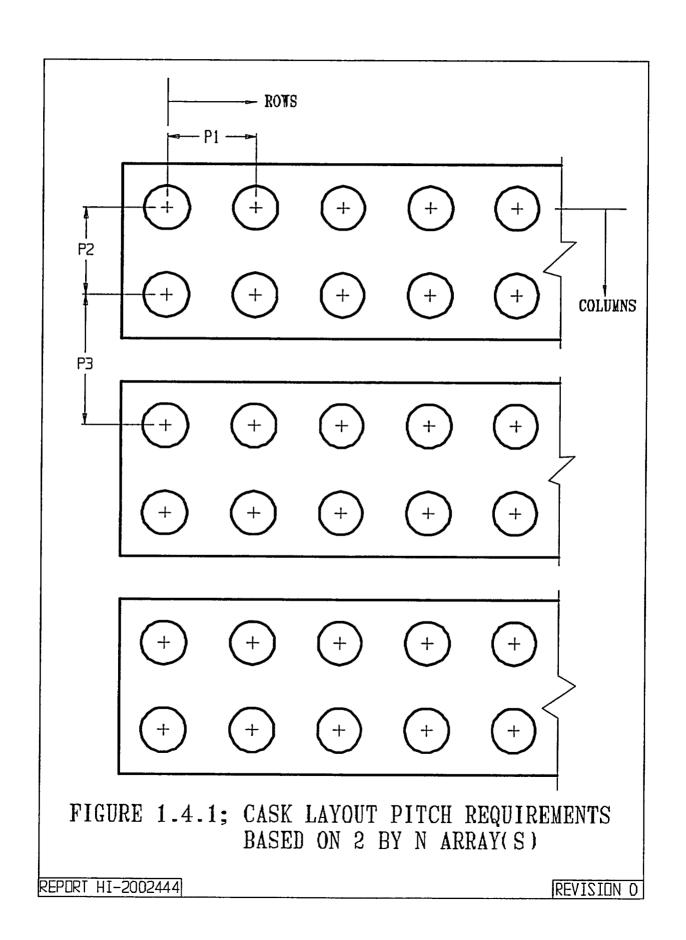
CASK LAYOUT PITCH DATA FOR 2 BY N ARRAYS

Orientation	Nominal Cask Pitch (ft.)
Between adjacent rows, P1, and adjacent columns, P2	13.5
Between adjacent sets of two columns, P3	38

Table 1.4.2

CASK LAYOUT PITCH DATA FOR SQUARE ARRAYS

Orientation	Nominal Cask Pitch (ft.)		
Between adjacent casks	18' - 8"		



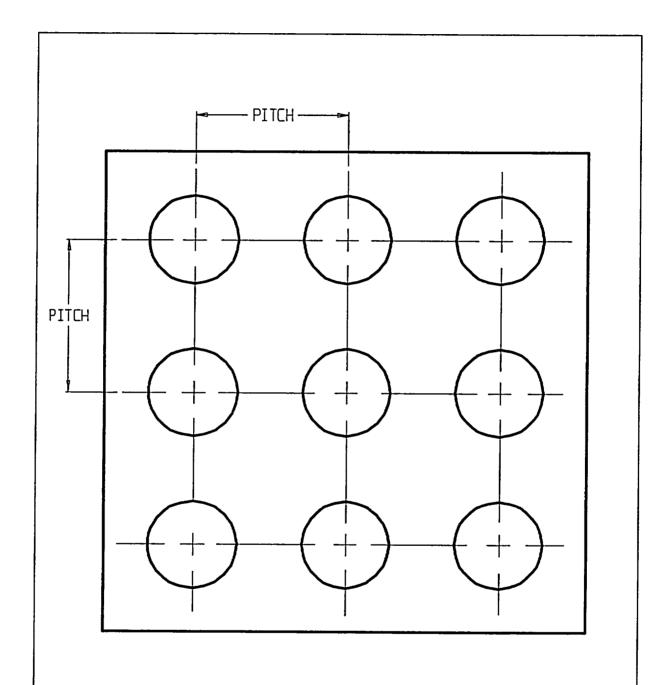


FIGURE 1.4.2; CASK LAYOUT PITCH REQUIREMENTS BASED ON A SQUARE ARRAY

REPORT HI-2002444

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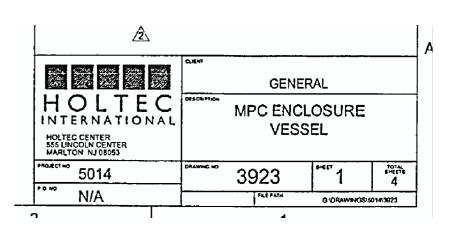
1.5 GENERAL ARRANGEMENT DRAWINGS

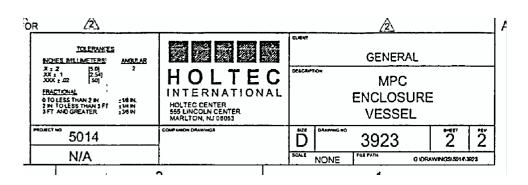
The following HI-STORM 100 System design drawings and bills of materials are provided on subsequent pages in this subsection:

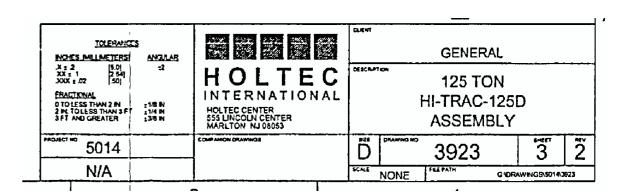
Drawing	Description	Rev.
Number/Sheet	Description	
3923	MPC Enclosure Vessel	2
3925	MPC-24E/EF Fuel Basket Assembly	1
3926	MPC-24 Fuel Basket Assembly	1
3927	MPC-32 Fuel Basket Assembly	2
3928	MPC-68/68F/68FF Basket Assembly	1
1495 Sht 1/6	HI-STORM 100 Assembly	11
1495 Sht 2/6	Cross Section "Z" - "Z" View of HI-STORM	16
1495 Sht 3/6	Section "Y" - "Y" of HI-STORM	12
1495 Sht 4/6	Section "X" -"X" of HI-STORM	12
1495 Sht 5/6	Section "W" -"W" of HI-STORM	14
1561 Sht 1/6	View "A" -"A" of HI-STORM	10
1561 Sht 2/6	Detail "B" of HI-STORM	13
1561 Sht 3/6	Detail of Air Inlet of HI-STORM	11
1561 Sht 4/6	Detail of Air Outlet of HI-STORM	12
3669	HI-STORM 100S Assembly	5
1880 Sht 1/10	125 Ton HI-TRAC Outline with Pool Lid	9
1880 Sht 2/10	125 Ton HI-TRAC Body Sectioned Elevation	10
1880 Sht 3/10	125 Ton HI-TRAC Body Sectioned Elevation "B" - "B"	9
1880 Sht 4/10	125 Ton Transfer Cask Detail of Bottom Flange	10
1880 Sht 5/10	125 Ton Transfer Cask Detail of Pool Lid	10
1880 Sht 6/10	125 Ton Transfer Cask Detail of Top Flange	10
1880 Sht 7/10	125 Ton Transfer Cask Detail of Top Lid	9
1880 Sht 8/10	125 Ton Transfer Cask View "Y" - "Y"	9
1880 Sht 9/10	125 Ton Transfer Cask Lifting Trunnion and Locking Pad	7
1880 Sht 10/10	125 Ton Transfer Cask View "Z" - "Z"	9
1928 Sht 1/2	125 Ton HI-TRAC Transfer Lid Housing Detail	11
1928 Sht 2/2	125 Ton HI-TRAC Transfer Lid Door Detail	10
2145 Sht 1/10	100 Ton HI-TRAC Outline with Pool Lid	8
2145 Sht 2/10	100 Ton HI-TRAC Body Sectioned Elevation	8
2145 Sht 3/10	100 Ton HI-TRAC Body Sectioned Elevation 'B-B'	8
2145 Sht 4/10	100 Ton HI-TRAC Detail of Bottom Flange	7
2145 Sht 5/10	100 Ton HI-TRAC Detail of Pool Lid	6
2145 Sht 6/10	100 Ton HI-TRAC Detail of Top Flange	8
2145 Sht 7/10	100 Ton HI-TRAC Detail of Top Lid	8
2145 Sht 8/10	100 Ton HI-TRAC View Y-Y	8
2145 Sht 9/10	100 Ton HI-TRAC Lifting Trunnions and Locking Pad	5
2145 Sht 10/10	100 Ton HI-TRAC View Z-Z	7
2152 Sht 1/2	100 Ton HI-TRAC Transfer Lid Housing Detail	10
2152 Sht 2/2	100 Ton HI-TRAC Transfer Lid Door Detail	8
3187	Lug and Anchoring Detail for HI-STORM 100A	2

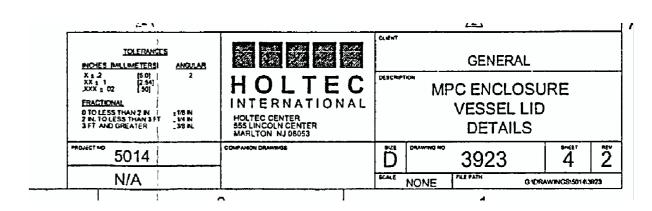
Drawing Number/Sheet	Description	Rev.	
BM-1575, Sht 1/2	Bill-of-Materials HI-STORM 100 Storage Overpack	15	
BM-1575, Sht 2/2	Bill-of-Materials HI-STORM 100 Storage Overpack	17	
BM-1880, Sht 1/2	Bill-of-Material for 125 Ton HI-TRAC	9	
BM-1880, Sht 2/2	Bill-of-Material for 125 Ton HI-TRAC	7	
BM-1928, Sht 1/1	Bill-of-Material for 125 Ton HI-TRAC Transfer Lid	10	
BM-2145 Sht 1/2	Bill-of-Material for 100 Ton HI-TRAC	6	
BM-2145 Sht 2/2	Bill-of-Material for 100 Ton HI-TRAC	5	
BM-2152 Sht 1/1	Bill-of-Material for 100 Ton HI-TRAC Transfer Lid	8	
3768	125 Ton HI-TRAC 125D Assembly	 	



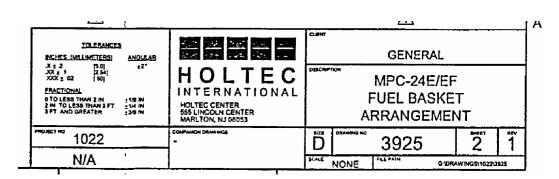


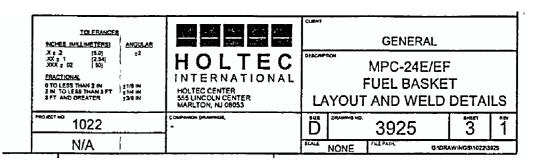


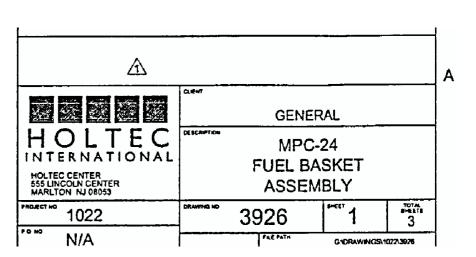


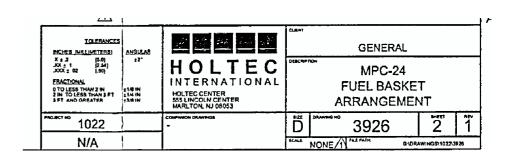


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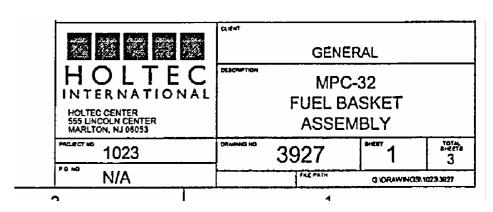


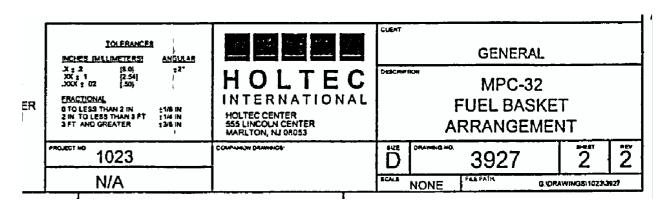


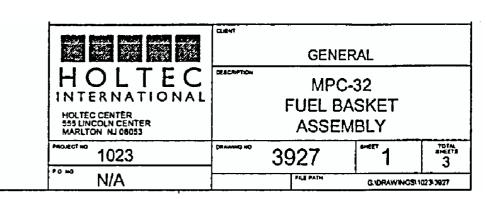


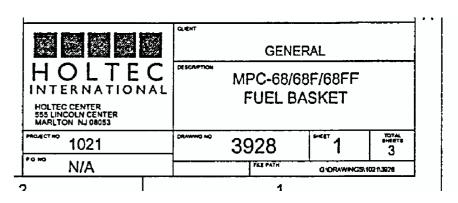


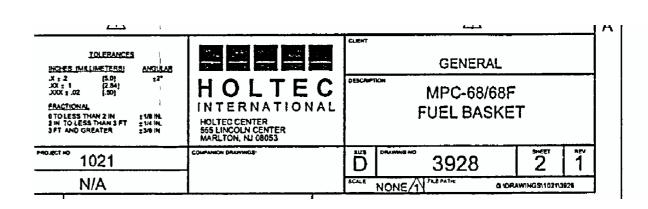
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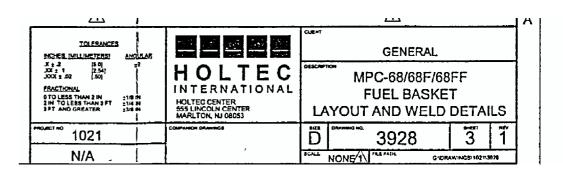


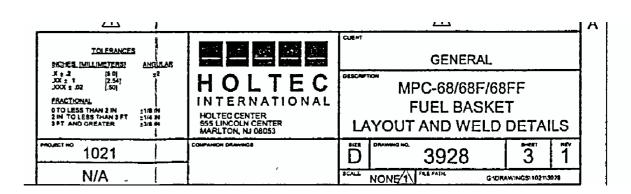


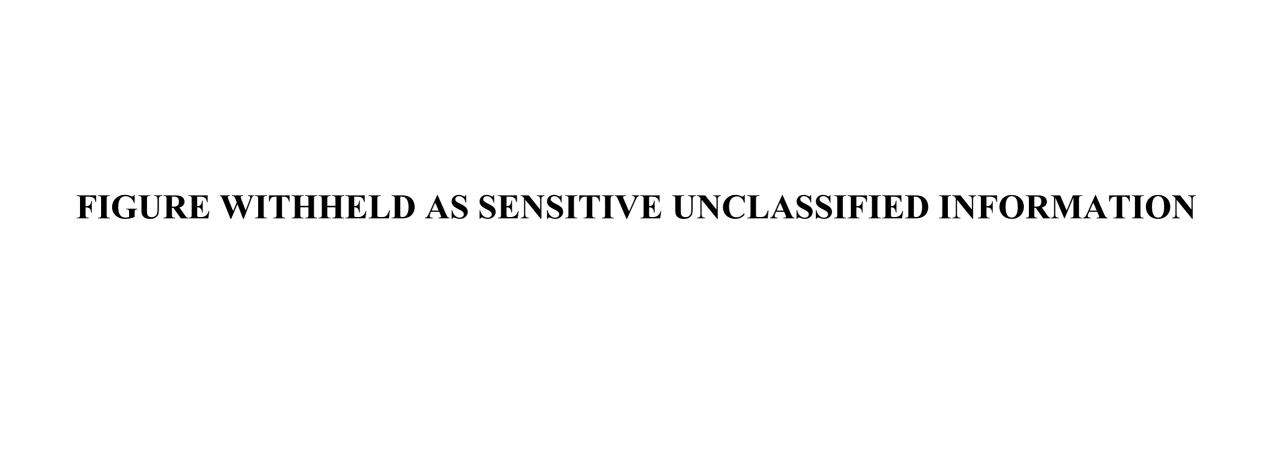


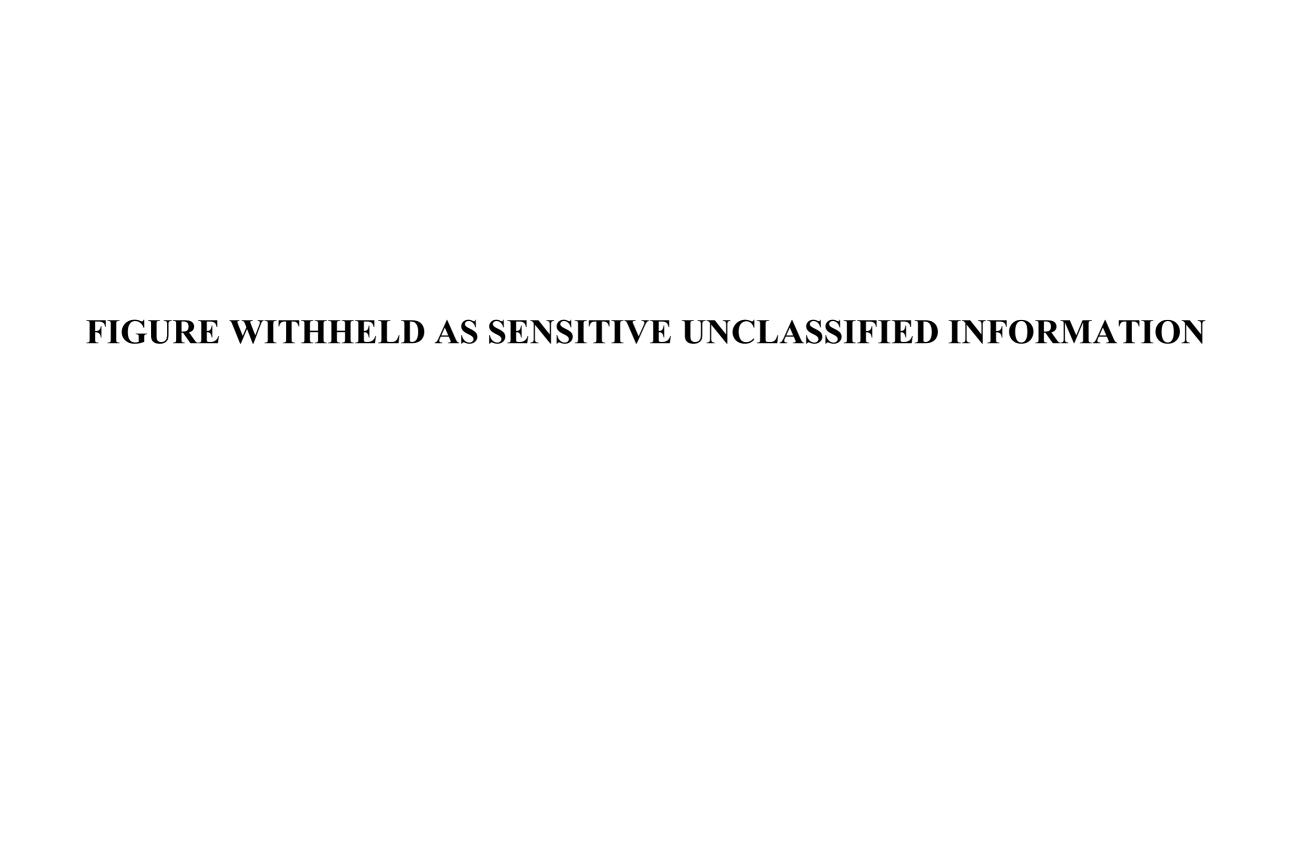


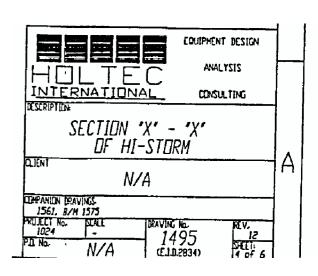


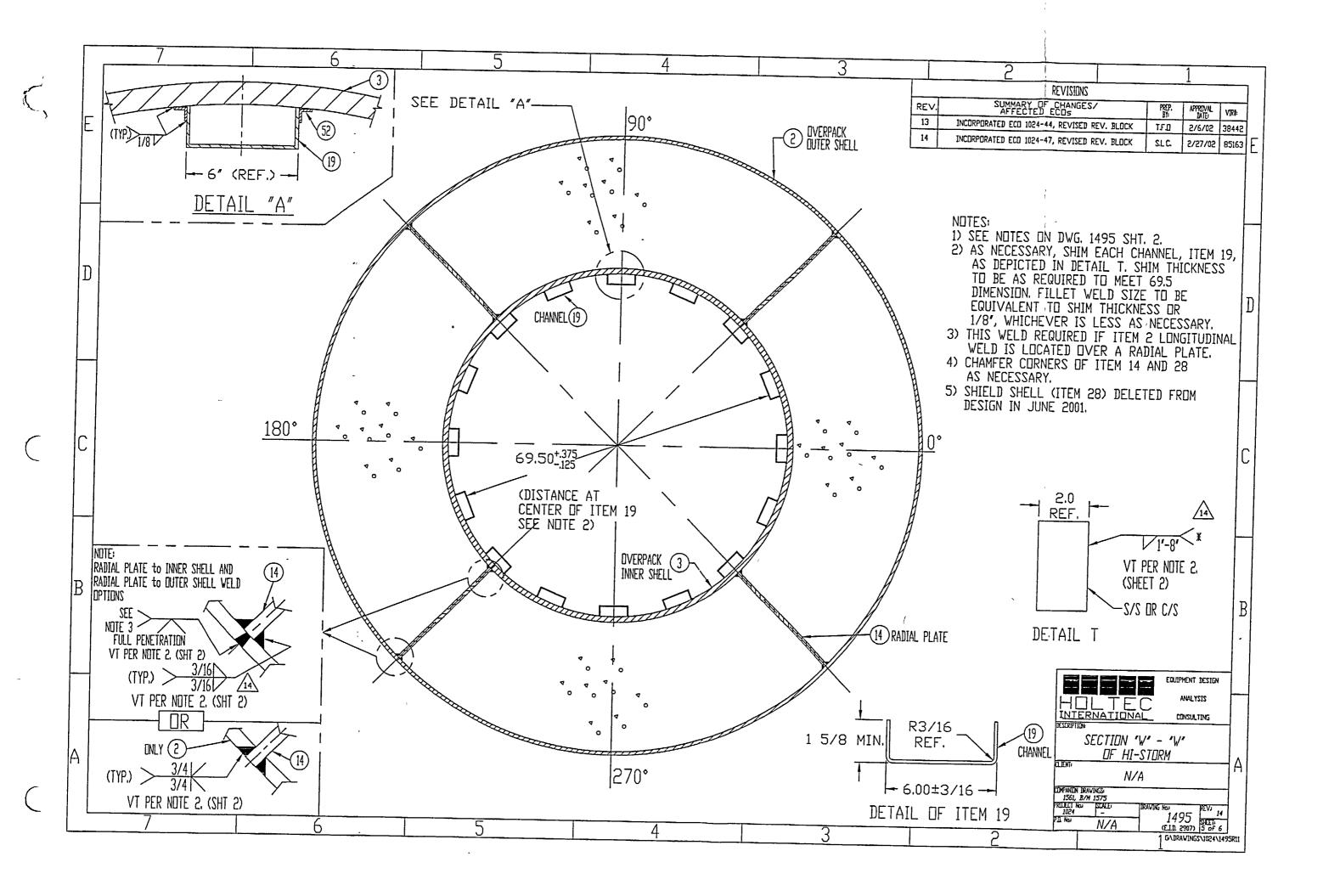


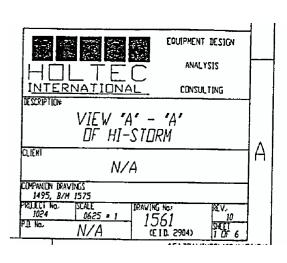


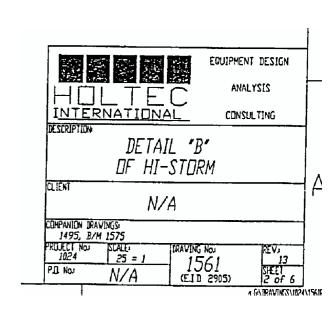


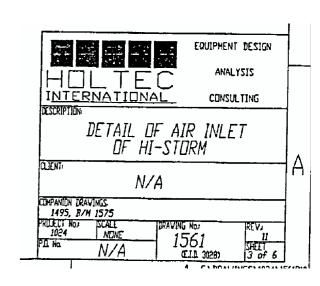


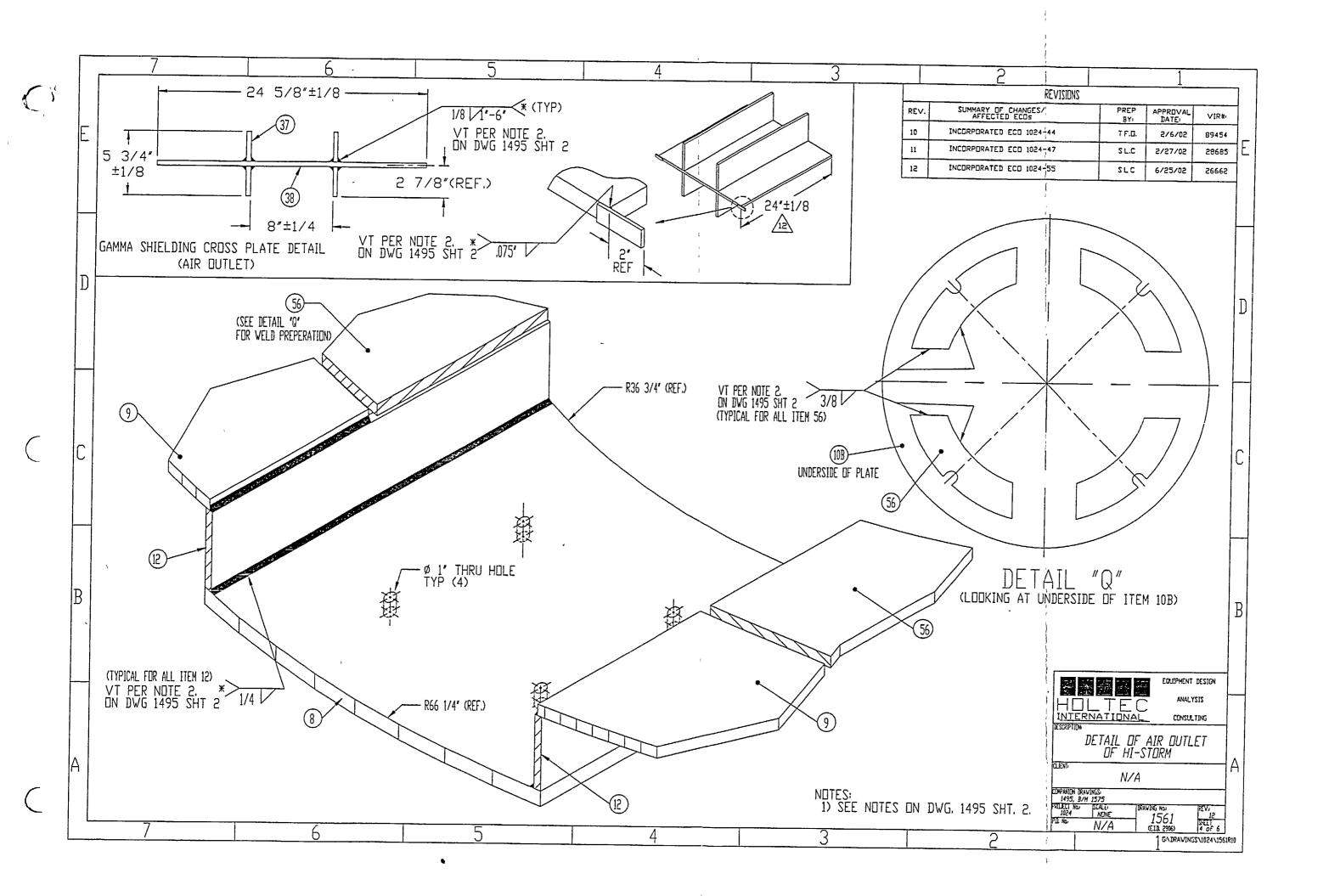




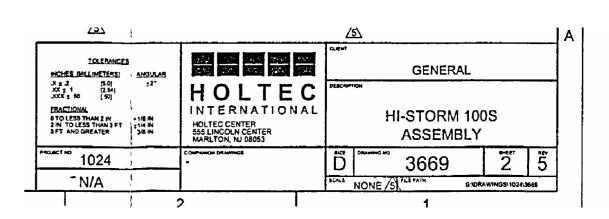




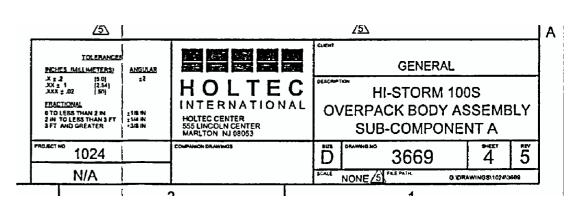


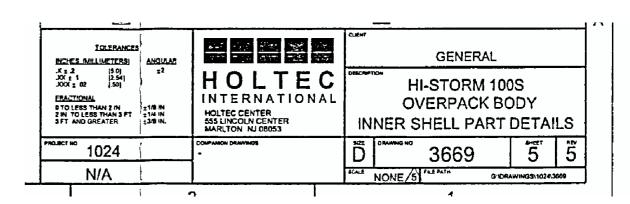


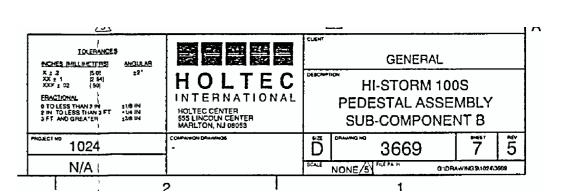
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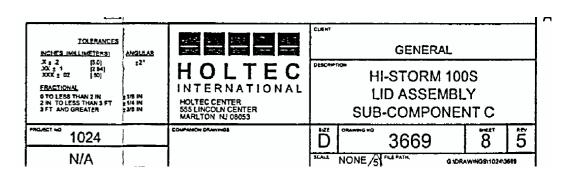


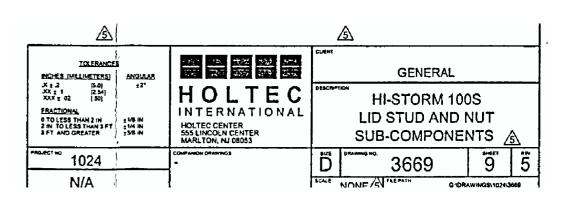
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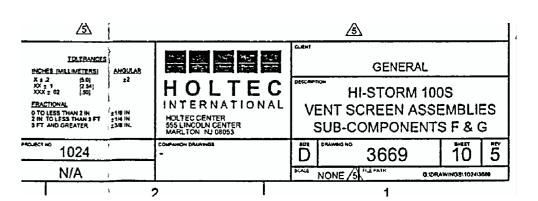


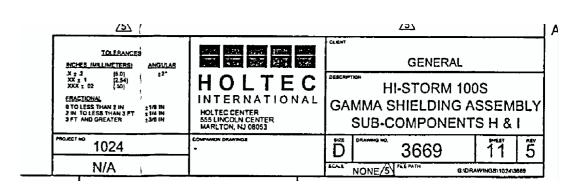


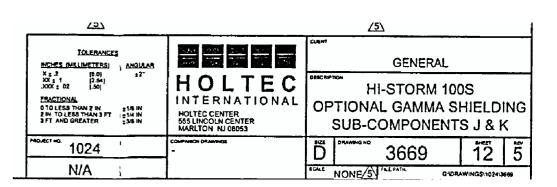


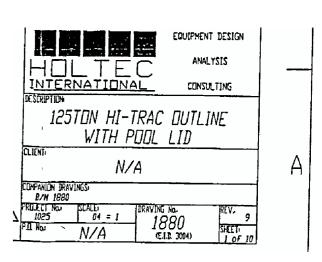


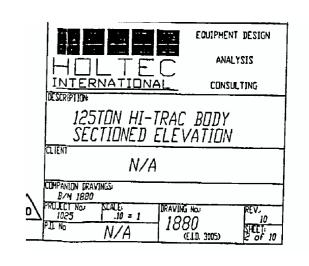


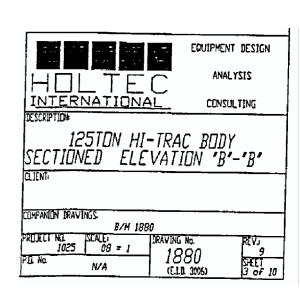


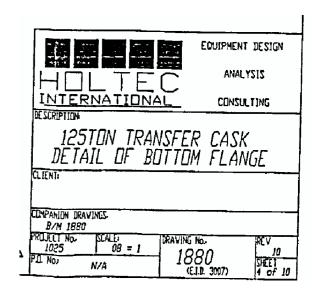


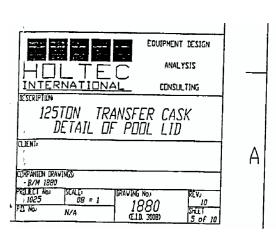


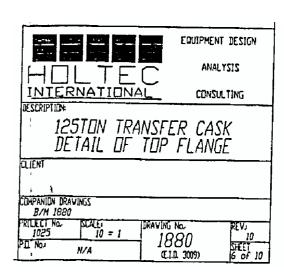


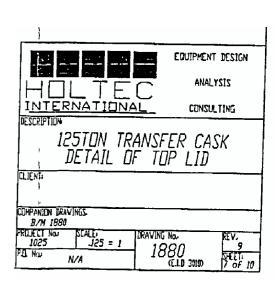












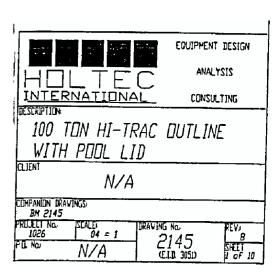
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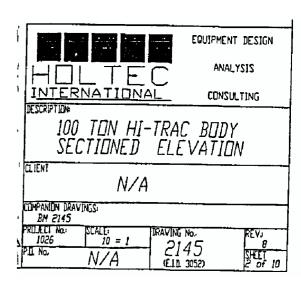
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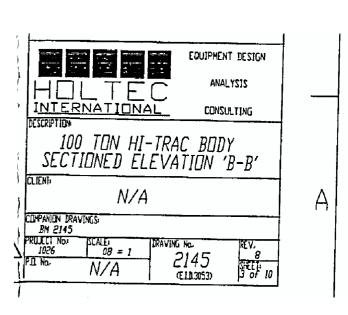
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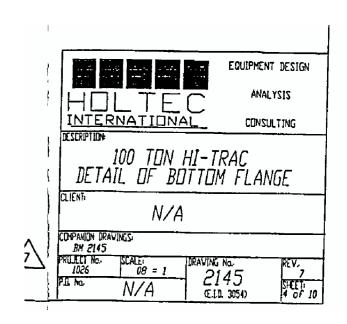
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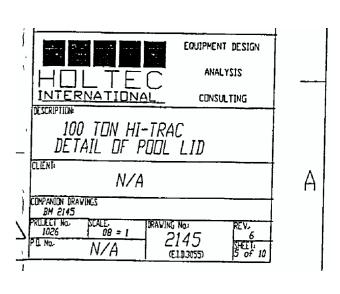


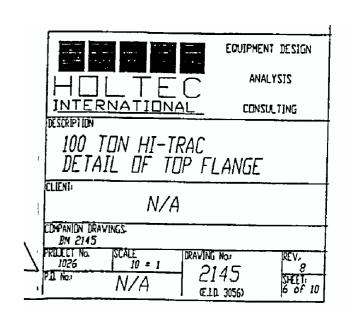


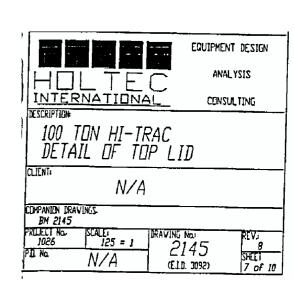


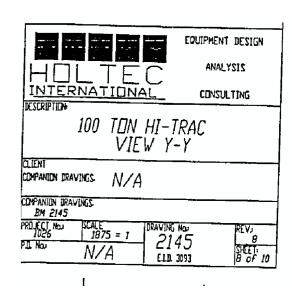


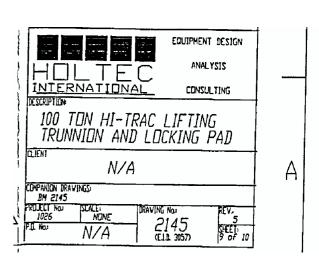


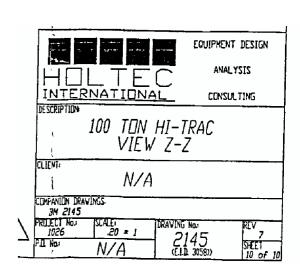




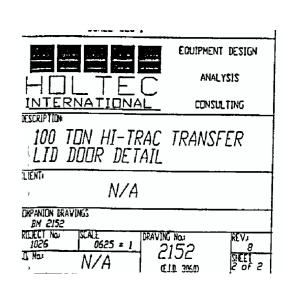








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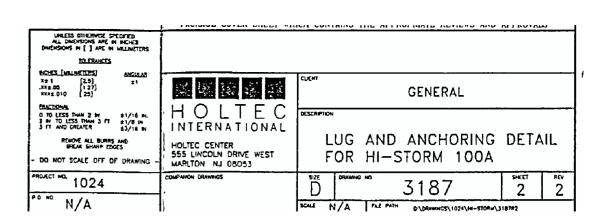
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LUG AND ANCHORING DETAIL
FOR HI-STORM 1000A

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	T		ATERIAL FOR HI-STORM (DWG. 1495, 1561) SHT	1 Ur 2		
REV.		AFF	MARY OF CHANGES/ ECTED E.C.D.s	PREP. BY:	APPROVAL DATE:	VIR#:
13	INCORPO	RATED E.C.O.# 1024-44.,	CHANGED REVISION BLOCK TO NEW FORMAT	T.F.D.	2/6/02	3443
14	INCORPO	RATED E.C.O.# 1024-50		S.L.C	5/7/02	46085
15	1	RATED E.C.O.# 1024-54		S.L.C	6/20/02	32848
1 1 2 1 3 1 4 1 5 1 6 1 7 1 8 4 9 1 10A 1 10B 1 11 4 12 8 13 8 14 4 15 4 16 4	SA 516 GR. 70 SA-516-70 SA-516-70 SA-516-70 SA 516 GR. 70 DR SA 515 GR. 70 DR SA 515 GR. 70 SA 516 GR. 70 SA 194 2H SA-564-630 AGE HARDENED AT 1075°F DR SA193-87	LID TOP PLATE LID TOP PLATE LID TOP PLATE INLET VENT HORIZONTAL PLATE EXIT VENT VERTICAL PLATE INLET VENT VERTICAL PLATE RADIAL PLATE TOP LID NUT LID STUD	DESCRIPTION 2 THK. X 133 7/8ø BASEPLATE 3/4 THK. X 224 1/2 LG. X 132 1/2 D.D. CYLINDER (MAY BE MAY 1 1/4 THK. X 224 1/2 LG. X 76 D.D. CYLINDER 26 3/4 THK. RADIAL SHIELD 1/4 THK. X 68 3/8 D.D. X 21 5/8 LG. CYLINDER 1 1/4 THK. X 70° Ø PLATE. 1 THK. X 10 1/2° WIDE X 69 D.D. 1 1/4 THK. X 26 WIDE X 29 1/2 LG. PLATE (SEE DET. DWG. 1561 S 3/4 THK. X 132 D.D. X 109 I.D RING (CUT IN 4 PIECES) 2 THK. X 124 Ø PLATE (SEE NOTE 4) 2 THK. X 126 Ø PLATE (SEE NOTE 4) 2 THK. X 16 1/2 WIDE X 29 1/2 LG. PLATE (SEE DET. DWG. 1561 S 1/2 THK. X 16 1/2 WIDE X 29 1/2 APPRDX. LG. PLATE 3/4 THK. X 10 WIDE X 29 1/2 APPRDX. LG. PLATE 3/4 THK. X 10 WIDE X 29 1/2 APPRDX. LG. PLATE 3/4 THK. X 27 1/2 WIDE X 224 1/2 LG. PLATE 3 1/4 - 4 UNC HEAVY HEX NUT 3 1/4 - 4 UNC X 16 LG. (SEE DWG. 1561, SHT 2)	ADE IN SECTION	JNS, SEE DWG 1495	
17 4	SA 350 LF3 DR SA 203 E	BOLT ANCHOR BLOCK	5 X 5 X 6 ANCHOR BLOCK W/ 3 1/4 - 4 UNC X 5 LG HOLE IN CE	NTER		
	04 544 50 74 00	DELETED CHANNEL	3/16 THK. X 6 WIDE X 170 7/8 LG. CHANNEL (SEE DETAIL 1495 SH	. 5) (GALVA)	NIZE EUB C/S)	
	SA 516 GR. 70	SHIELD BLOCK RING	1/4 THK. X 63 1/2 I.D. X 85 1/2 D.D. (MAY BE MADE FROM MORE THAN 1 PIECE.)	- Content	1	
21 1	CONCRETE	PEDESTAL SHIELD	17' THK, PLATFORM			
23 1	CA 51/ CD 70	LID SHIELD PEDESTAL PLATE	10 1/2 THK. TOP SHIELD 1/2 THK X 67 7/8 Ø		1	
		PEDESTAL PLATFORM	5 THK. X 67 7/8 Ø PLATE (MAY USE MULTIPLE PLATES OF LESSER - NUMBER OF PLATES AND THICKNESS OF PLATES OPTIONAL)	THICKNESS	·	
25 1	CONCRETE	SHIELD BLOCK	18' THK.		1	
26 1	SA 516 GR. 70 DR SA 515 GR. 70	SHIELD BLOCK SHELL	1/2 THK X 86 D.D. CYLINDER X 8' HIGH (MAY MAKE DUT DF MORE	THAN 1 PIECE) ¹	
2/ 1		SHIELD BLOCK SHELL	1/2 THK X 64 D.D. CYLINDER X 8' HIGH (MAY MAKE DUT OF MORE			
28 - 29 1	240 204	DELETED				
30 4	SA 240 304 C/S DR S/S	STURAGE MARKING NAME PLATE	14 GAGE (0.0751 THK.) X 4 WIDE X 10 LG. SHEET			
<u> </u>	57 5 ER 373	LID (LOUS	1 1/2'-6UNC X 1 1/2' DP BOLT OR 1 1/2'-6UNC X 2' LG SET SCREV	<u>/</u>	1	

<u>*</u>

¹⁾ THE CUNCRETE MATERIAL IS TO MEET THE REQUIREMENTS SPECIFIED IN APPENDIX 1.D OF THE HI-STORM 100 FSAR
DOCKET NUMBER 72-1014 (LATEST REVISION).
2) ALL DIMENSIONS IDENTIFIED ON BM-1575 ARE APPROXIMATE DIMENSIONS EXCEPT THICKNESSES OF STEEL PLATES WHICH IN THE
RAW MATERIAL FORM MUST HAVE TOLERANCES MEETING THE APPLICABLE SPECIFICATION.

³⁾ ITEMS WITH A * CONSIDERED NOT TO BE NF CLASS 3 (NON STRUCTURAL)

⁴⁾ AS AN OPTION, ITEMS 10A & 10B CAN BE COMBINED AS A SINGLE 4° THICK PLATE AT 126° Ø.

-			BM-15	BM-1575 (E.I.D. 2836) BILL OF MATERIAL FOR HI-STORM (DWG. 1495, 1561) SHT 2 OF 2							
-		EV.		SUMMAR	RY DF CHANGES/ ECTED E.C.D.s	PREP. BY:	APPROVAL DATE:	VIR #			
-	1:	3 	-	INCORPORAT	ED E.C.O.#: 1024-47	S.L.C	2/27/02	72710			
	1	4		INCORPORAT	ED E.C.D.#: 1024-50	S.L.C	5/7/02	19678			
	15	5		INCORPORAT	ED E.C.D.#: 1024-54	S.L.C	6/20/02	89834			
	16	6		INCORPORATED E.C.O.#: 1024-56			6/21/02	14060			
	17	7	INCORPORATED E.C.O.#: 1024-55			S.L.C					
Ī	TEM	QTY.	SPECIFICATION	NOMENCLATURE	DESCRIPTION	S.L.C	6/25/02	96106			
$\langle \mid \mid$	31	4	SA 240 304	DELETED EXIT VENT SCREEN SHEET		,					
	33	4	SA 240 304	EXIT VENT SCREEN FRAME	16 GAGE (0.0595 THK.) X 6 1/4 WIDE X 40 LG. SHEET 16 GAGE (0.0595 THK.)	,					
	34	1	COMMERCIAL	SCREEN	16 WIDE X 212 LG. 6 X 6 MESH 0.020 WIRE Ø 0.147 WIDTH OPEN FROM McMASTER-CARR 101 PAGE# 2521 ITEM# 9220T67 CUT AS NECESSARY OR EQUIV	AL FUT					
	35	4	SA 240 304	INLET VENT SCREEN FRAME	16 GAGE (0.0595 THK.)	ALENI					
	36	2	COMMERCIAL	THERMOCOUPLE OR RTD	1/8 Ø SHEATH WITH TEMPERATURE ELEMENT (BY USER).	i					
	37	16	SA240-304	GAMMA SHIELD CROSS PLATE	1/4 THK X 2.75 X 24						
	38 39	4 24	SA240-304	GAMMA SHIELD CROSS PLATE	1/4 THK X 24 X 24 5/8	· · · · · · · · · · · · · · · · · · ·					
	40	Ω 24	SA240-304 SA240-304	CROSS PLATE TABS	.075 THK X 1/4 X 2 1/2						
-	41	16	SA240-304	GAMMA SHIELD CROSS PLATE	1/4 THK X 14 5/8 X 24	``		·			
	42	2	C/S DR S/S	GAMMA SHIELD CROSS PLATE DRAIN PIPE	1/4 THK X 3.09 X 24						
	43	8	SA240-304	GAMMA SHIELD CROSS PLATE	3/4 SCH 160 PIPE X 11 1/2 LG						
	44	2	316 SS	COMPRESSION FITTING	1/4 THK X 5.09 X 17 1/4						
	45	2	CAST_IRON	PROTECTION HEAD	1/8' X 1/4 NPT MALE PASS THRU COMPRESSION FITTING (OPTIONAL)	-				
	46	2	304 SS	BUSHING	1/2 NPT X 1/2 NPT (OPTIONAL)	1					
	47	2	304 SS	COUPLING	1/4 X 1/2 NPT (OPTIONAL)						
	48	2	304 SS	HEX NIPPLE	1/2 NPT COUPLING W/ MOUNTING STUD 1/2 DIA X 3' LG. (OPTIONA	L)					
	49	2	304 SS	CONNECTION	1/2 X 1/2 NPT HEX NIPPLE (OPTIONAL)	3					
	50	28	2\2	SCREW	1/2 NPT CONDUIT CONNECTION (OPTIONAL)	1					
_	51	4	2\2	WASHER	Ø1/4' X LENGTH AS REQUIRED	·					
	52	96	A36	CHANNEL MOUNTS	1/2' MIN. THK. X 3 1/2' I.D X 8' MIN. O.D. 3/16' X 1' X 1' X 24' LONG						
	53	4	C/S	SHIMS	2* THE V 2* LIDEC V 2* LIDEU						
	54	4	\$/\$	BAR INLET SCREEN BASE	2' THK X 3' LDNG X 2' HIGH						
	55	8	2\2	BAR INLET SCREEN BASE	1/2' X 1' X 24 3/32' LG. BAR						
	56	1	SA516 GR. 70	SHEAR RING	1/2' X 1' X 15' LG. BAR.						
	57	2	SA516 GR. 70	GROUNDING BLOCK	3/4' THK. X 73 1/2' I.D. X 108' D.D. PLATE (CUT IN FOUR PIECES) 1/2' THK. X 2' WIDE X 4' LONG	1					
-	SASIS GR. 70 SKITVENT FRAME LEG										
				EXITVENT FRAME TOP							
				INLETVENT FRAME LEG	3/8' THK. X 1' WIDE X 28 1/4' LG. (CUT AS REQUIRED)	١					
(3/8' THK. X 1' WIDE X 12' LG. (CUT AS REQUIRED)	1					
_					3/8' THK. X 1' WIDE X 18 3/4' LG. (CUT AS REQUIRED)						
_					3/8" THK. X 1/2" WIDE X 32 5/16" LG.						
_				ENTI CONCENT DUSE	3/8" THK. X 1/2" WIDE X 10" LG.	1					

	BM-1	880 (L OF MATERIAL FOR 125	TON HI-TRAC (D)	VG. 1880) SHT. 1 OF	2	
	REV.	ND.		RY OF CHANGES/ ECTED ECOs	PREP. BY	-APPROVAL DATE:	VIRIII	
	9		15, 12, 1	RATED ECO 1025-35, B, 6 & 5.	T.F.O.	11/30/01	70889	
	ITEM	QTY.	SPECIFICATION	NDMENCLATURE		DESCRIPTION		
	1	<u> </u>	ASTM B 29	RADIAL LEAD SHIELD	113 CU. FT. COMMON	LEAD APPROX.		
	$\omega_{\mathbb{R}}$	1	SA 516 GR. 70 SA 516 GR. 70	DUTER SHELL	1 THK, X 81,25 D.D.	X 184.75 LG. CYLINDER		
A	_ <u>3</u>		- 2H 316 GK. 70	INNER SHELL DELETED	0.75 THK. X 68.75	.D. X 184.75 LG. CYLIN	DER	
份	4A			DELETED				
私	4B	-	_	DELETED				
A	_5	ı	_	DELETED				
<u>/9\</u>	_5A		-	DELETED		_		
	6A	2	SA 516 GR. 70	WATER JACKET END PLATE	1 THK, X 94.625 D. (MAY BE MADE FRO	D. X 81.25 I.D. X 141° (A 4 MORE THAN 1 PIECE)	APP)	
	6B	1		WATER JACKET END PLATE	I THK. X 94.625 П	D. X 81.25 I.D. RING 4 MORE THAN 1 PIECE)		
	7	_1	SA 350 LF3	TOP FLANGE	4.5 THK. X 81.25 D.	D. X 68.75 I.D. RING		
	8	<u>l</u>	SA 516 GR. 70	LOWER WATER JACKET SHELL	0.5 THK. X 86.25 []	D. X 6 LG. CYLINDER		
	9	1	SA 516 GR. 70 DR SA 350 LF3	BOTTOM FLANGE	2 THK. X 93 D.D. X	68.75 I.D.		
A	10	1	SA 516 GR. 70 DR SA 203-E DR SA 350 LF3	POOL LID OUTER RING	3.5 THK. X 93.75 [I.D. X 75 I.D. RING		
	_11	1	SA 516 GR. 70	POOL LID TOP PLATE	2 THK. X 93 Ø PLA	TE		
۵	12 13	1 —	ASTM B 29	POOL LID LEAD SHIELD	6.39 CU. FT. COMMO	N LEAD APPROX.		
盆	14	$\frac{1}{1}$	SA 516 GR. 70 SA 516 GR. 70	TOP LID OUTER RING TOP LID INNER RING	0.5 THK. X /1.8/5 [I.D. X 3.25 LG. CYLINDE	R	
不	15	i	SA 516 GR. 70	TOP LID TOP PLATE	0.3 THK, X 29 U.U. 0.5 THK Y 71.275 C	X 3.25 LG. CYLINDER I.D. X 28.5 I.D. RING		
	16	1	SA 516 GR. 70	TOP LID BOTTOM PLATE	1.0 THK. X 81.25 D.I	N X 27 I D PING	<u></u> -	
	17	1	HOLTITE	TOP LID SHIELDING	5.41 CU. FT. APPROX	ζ.		
<u>A</u>	18	8	SA 516 GR. 70	FILL PORT PLUGS	3 1/4'LG. X 2 7/8' MULTIPLE, UNATTAC	Ø CYLINDER (MAYBE	MADE OF	
	19	24	SA 193 B7	TOP LID STUD	1-8 UNC X 4 3/8 I	.G. STUDS (4 3/8 FULL NCH FLAT AT DNE END	LENGTH	
Δ	20	24	SA 194 2H	TOP LID NUT	11-8 UNC HEAVY HE	X WITH WASHER		
4	_21_	<u> </u>	ELASTOMER	POOL LID GASKET	0.5 THK, X 87.25 II	D. X 85.75 LD. COMMERI	CIAL	
	55	36	SA 193 B7	POOL LID BOLT	1 - 8 UNC X 3.125 THREAD LENGTH W/	I.G. HEX. ROLLS X 125	MIN	
		N	DTE: 1) ALL SA-3	50-LF3 MATERIAL MAY BE REPL	ACED BY CV-503-E			
ļ			2) ALL DIMEN	NSIUNS ARE FOR REFERENCE ONL	Y,			
			272, 24-503-E	VSIONS ARE FOR REFERENCE ON 18, SA 516 GR.70 MAY BE REPL OR SA-350-LF 3 DR EQUIVALE	NCED WITH NT.		İ	
	CARDAMINES 1035 TRUBES TOURS							

	REV.	ND.		D 3003) BILL OF MATERIAL SUMMARY OF CHANGES/ AFFECTED CCOs		PREP BY:	APPROVAL DATE:	VIR#:	
	7			INCORPORATED ECO 1025-: 20, 13, 8 & 5.	35,	T.F.O.	11/30/01	22562	
1	TEM	QTY,	SPECIFICATION	NDMENCLATURE		DESCRIPTION	II		
7	23	12	SA 516 GR.70	ENCLOSURE SHELL PANEL	0.5 ТНК. X 93.00 П.D.		DEG. SHELL SEGMENTS		
	24	2	SA 350 LF3	LIFTING TRUNNION BLOCK	7.625 (APPROX) X 10	X 10			
-	25 26	2	CD (27 M07710	DELETED					
 	27	5	SB 637 N07718 SA 516 GR, 70	LIFTING TRUNNION LIFTING TRUNNION END CAP	6.25 Ø X 9.25 LG. BA 0.5 THK. X 6.25 Ø PL	AR			
	28	4	SA 193 B7	END CAP BOLTS	0.5 - 13 UNC X 1 LG	. WITH 5/8 LG THE	DEAD		
L	29 2 SA 350 LF3 PDCKET TR			POCKET TRUNNION	12.375 X 13 X 12.5 BLOCK				
_	30	<u>-1</u> 12	SA 106	DRAIN PIPE	1 SHC. 80 X 7 (APPR	OX.) LG. PIPE			
┢	31			NRAIN ROLT	1.25 THK. X 5.361 W	X 168.75 LG.			
	33			DELETED	1 - 8UNC X 1.75 LG.	PUCKET PET PEKE	<u>W</u>		
L	34	2	SA 516 GR, 70	WATER JACKET END PLATE	1 THK, X 94.625 D.D.	X 81.25 I.D. X 39°	(APP)		
-	35 36	1	 CA E1(CD 70	DELETED				*****	
\vdash	36 37	1	SA 516 GR. 70 COMMERCIAL	POOL LID BOTTOM PLATE VENT COUPLING	1 THK, X 77 Ø PLATE				
\vdash	38	1	COMMERCIAL	VENT PLUG	1 1/2-3000 lb. SCREW	L HALF COUPLING	(OR SIMILAR)		
Ţ	39	2	COMMERCIAL	PRESSURE RELIEF COUPLING	1 1/2-3000 lb. SCREWED 2-3000 lb. SCREWED	DALE COURTINE OF	OU (UK SIMILAK)		
\[40	2	COMMERCIAL	PRESSURE RELIEF VALVE	MEDIUM PRESSURE PE	THE CHUPEING (I	K SIMILAR)		
L	41	1	SA 106	JACKET DRAIN PIPE	1 1/2 SCH. 40 X 5 L	G. PIPF	Lniv)		
ľ	42	1	COMMERCIAL	JACKET DRAIN VALVE	1 1/2 NDNRISING STE		CDA IIMIO DI		
	43	4	C/S OR S/S	HOLE PLUGS	N/A	- GITT VHLVL (L	IIV STLITCHLY		
	44	4	SA 516 GR. 70	TOP LID LIFTING BLOCK	1.5 SQ. X 3.25 LG. BI	ULK			
	45			DELETED					
	46			DELETED					
7	47	4	SA 516 GR.70	SHORT RIB	0.5 THK. X 6.688" W	Y / 125 LG			

		****		(
	Di-1	-1928 (E.I.D. 300	1) BILL OF MATERIAL FO	R 125 'UN HI-	TRAC TRANSFER	LID (DWG. 1928	3)	
	REV. NO.	SU	MMARY OF CHANGES/AFFECTED	ECOs	PREP BY:	APPROVAL DATE:	VIR#:	
•	10		INCORPORATED ECO 1025-35, 10, 8, 6, & 4.		T.F.O.	11/30/01	87422	
	ITEM QT	Y. SPECIFICATION	NOMENCLATURE		DESCRI	DTION		
M	1 1	SA 516 GR. 70	LID TOP PLATE	1.5 THK, X 93.5 V	VIDE X 128 LG, PLA	ATE		
	2 1	SA 516 GR. 70	LID BOTTOM PLATE		IDE X 128 LG. PLAT			
<u>₩</u>	3 2		LID INTERMEDIATE PLATE	1.5 THK. X 8.625	WIDE X 132 LG. PL			
A	4 2		LEAD COVER PLATE	1 THK. X 8.625 W				
107	5 8		LEAD COVER SIDE PLATE		E X 8.625 LG. PLA	TE		
۸	6 1 ASTM B 29 SIDE LEAD SHIELD 2.65 (APPROX.) CU. FT.							
₩		2 SA 36 WHEEL TRACK 0.25 THK, X 1 X 1 X 128 LG, ANGLE 2 SA 516 GR, 70 DOOR TOP PLATE 2 1/4 THK, X 47 WIDE X 80 LG, PLATE (CUT AS NECESSAI						
	9 2		DOOR LEAD SHIELD	<u>2 1/4 THK. X 47</u> 2.9 (APPROX.) CU.	WIDE X 80 LG. PL	ATE (CUT AS NECES	SARY)	
	10 2		DOOR MIDDLE PLATE			E (CUT AS NECESSA	(DV)	
	l ii l a		DOOR SHIELDING	3.65 (APPROX.) CI	IDE A OU LUI I LAI	L (CO) HO NECESSE	N(1)	
	12 2		DOOR BOTTOM PLATE			E (CUT AS NECESSA	ARY)	
	13 4		DOOR WHEEL HOUSING 1 7/8 THK. X 6 WIDE X 25 LG. PLATE					
	14 2	14 2 SA 516 GR. 70 DOOR INTERFACE PLATE I THK. X 3 7/8 WIDE X 80 LG. PLATE						
	15 6	SA 516 GR. 70	DOOR SIDE PLATE	1 THK. X 5.75 WI	DE X 65 LG. PLATE			
	15A 4	SA 516 GR, 70	DOOR SIDE PLATE	1 THK, X 5.75 WI	DE X 65 LG. PLATE			
	16 4	SA 516 GR. 70	DOUR SIDE PLATE	1 THK. X 5.75 WI	DE X 32.625 APPRO	JX, LG. PLATE		
	17 a		DOOR HANDLE	3/4-10UNC EYE I	BOLT			
	18 1	2 COMMERCIAL	DOOR WHEEL	6 X 3 V-GROOVE	WHEEL.			
	19 1	2 SA 193-B7	WHEEL SHAFT	1.25-7UNC (1.25'	THREAD LENGTH) X	6.625 LG. BAR WIT TION AT UNTHREADE	H D CMD	
	20 -		DELETED		TO THE INCINCENT	TIBN III ONTINCIAL	.D LIVD.	
⑥	21 6	SA 516 GR. 70	LID HOUSING STIFFENER	1 THK, X 3.5 WIT	DE X 8.625 LG. PLA	TF		
<u>60</u>	55 4	SA 193 B7	DOOR LOCK BOLT			W/ 1.5 LG. THREAD	IF D	
				AT END	TO GO! MEM DEETO	W NO EG. THICHE	n L D	
	23 4		DOOR STOP BLOCK	2 THK. X 2 WIDE	X 8 LG. BLOCK			
	24 8		DOOR STOP BLOCK BOLT	1 - 8 UNC X 3 I	.G. BOLT W/ 2.5 LO	J. THREADED AT ENI]	
	25 2	SA 516 GR. 70	DOOR END PLATE	[1_THK, X 5.75 W]	IDE X 19 LG. PLATĒ			
	26 4		LIFTING LUG		IDE X 3.5 LG. PLAT	Ē		
	27 4	SA 516 GR, 70	LIFTING LUG PAD	0.5 THK. X 5 SQ.	PLATE			
	NDTE:	ALL DIMENSIONS ARE	APPROXIMATE.					

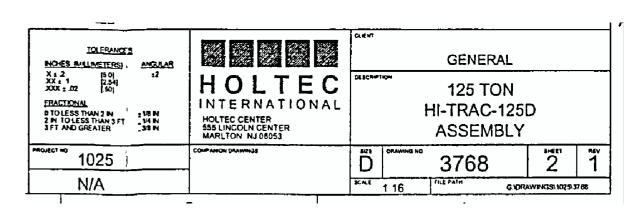
(_								
		BM-2	2145 (E.I.D. 3049	9) BILL OF MATERIAL FOR	100 TON HI-TRAC	(DWG, 2145) SH	IT. 1 OF 2		
	REV.	NO.	MMU2	ARY OF CHANGES/AFFECTED ECO)s	PREP BY:	APPROVAL DATE:	VIR#:	
	6			INCORPORATED ECD-1026-28, 18, 7 & 5	8,	T.F.D.	11/30/01	70563	
	ITEM	QTY.	SPECIFICATION	NDMENCLATURE	DESCRIPTION				
	1	1	ASTM B 29	RADIAL LEAD SHIELD	71.15 CU. FT. COMMON	LEAD APPROX.			
Ì	5	1	SA 516 GR. 70	DUTER SHELL	1 THK, X 78 D.D. X 1	84.75 LG. CYLINDER	5		
.	3	1	SA 516 GR. 70	INNER SHELL	0.75 THK. X 68.75 I.I	D. X 184.75 LG. CYL	INDER		
4	4		<u> </u>	DELETED		-		7	
	4A_		<u> </u>	DELETED ·		-			
Δ	4B			DELETED					
ÝΣ	5		-	DELÉTÉD		_			
Δ	5A	-		DELETED					
	6A	5	SA 516 GR. 70	WATER JACKET END PLATE	(MAY BE MADE FROM MORE THAN 1 PIECE)				
	6B	l I	SA 516 GR. 70	WATER JACKET END PLATE	1 THK. X 91 D.D. X 7	8 I.D. RING	(MAY BE MADE FROM	MORE THAN I PIECE)	
	7	1	SA 350 LF3	TOP FLANGE	4.5 THK, X 78.00 D.D.	. X 68.75 I.D. RING	KINIT DE TRUIT	TIBRE THIN I TIEGE?	
	8	1	SA 516 GR. 70	LOWER WATER JACKET SHELL	1.25 THK, X 83.00 D.1	D. X 6 LG. CYLINDE	R		
	9	1	SA 350 LF3, DR SA 516 GR. 70	BOTTOM FLANGE	2 THK. X 89 D.D. X	68.75 I.D.			
	10	1	SA516 GR 70 DR SA 203-E DR SA350 LF3	POOL LID DUTER RING	2.0 THK X 89-3/4	D.D. X 75 I.D.			
	11	1	SA 516 GR. 70	POOL LID TOP PLATE	2 THK, X 89 Ø				
	12	1	ASTM B 29	POOL LID LEAD SHIELD	3.84 CU FT APPROX.	COMMON LEAD			
	13	T		DELETED					
	14			DELETED			· · · · · · · · · · · · · · · · · · ·		
	15			DELETED					
	16	1	SA 516 GR. 70	TOP LID BOTTOM PLATE	1.0 THK. X 78.00 D.D. X 27 I.D. RING				
	17	1	_SA 516 GR 70	POOL LID BOTTOM PLATE	5 THK X 76.5 Ø				
₽	18	8	SA 516 GR. 70	FILL PORT PLUGS	3 1/4 LG. X Ø2 3/8	PIECE	2)		
£Σ	19	24	SA 193 B7	TOP LID STUD	1-8 UNC X 5 LG. S ONE END)	TUD (FULL LENGT)	THREAD WITH WRE	NCH FLAT AT	
Δ	_20	24	SA 194 2H	TOP LID NUT	1-8 UNC HEAVY HEX	WITH WASHER (3/	16" MAX; OPTIONAL)		
Δ	21	1	ELASTOMER	POOL LID GASKET	0.5° THK, X 83.625 [J.D. X 82.125 I.D. C	DMMERCIAL		
ℯ	55	36	SA 193 B7	POOL LID BOLT	1-8UNC X 3.125 LG. K3/16' MAX; OPTIONA	HEX BOLTS WITH I	.25' MIN THRD LENG	TH W/WASHER	
	53			DELETED					
	24	2	SA 350 LF3	LIFTING TRUNNION BLOCK	7.25 (APP) X 10 X 1	0			
	25	<u> </u>	<u> </u>	DELETED					
	}	NOTE:	S: 1. ALL SA-350-	LF3 MATERIAL MAY BE REPLACE	D BY SA-203-E.				

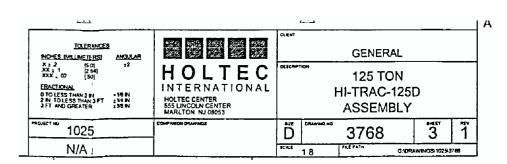
NDTES: 1. ALL SA-350-LF3 MATERIAL MAY BE REPLACED BY SA-203-E. 2. ALL DIMENSIONS ARE FOR REFERENCE ONLY.

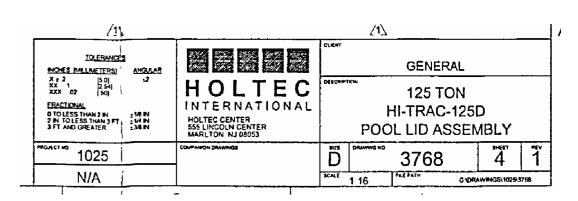
		BM-6	2145 (E.I.D. 305	O) BILL OF MATERIAL FOR	100 TON HI-TRAC	(DWG, 2145) SH	T. 2 OF 2			
	REV.	NO.	SU	MMARY OF CHANGES/AFFECTED E	COs	PREP BY:	APPROVAL DATE:	VIR#:		
	5		I	NCORPORATED ECO-1026-10, 7 &	5.	T.F.O.	11/30/01	66474		
	ITEM	QTY.	SPECIFICATION	NOMENCLATURE	DESCRIPTION					
	26	2	SB 637 N07718	LIFTING TRUNNION	6.25 Ø X 9.25 LG. B		1701			
	27	2		LIFTING TRUNNION END CAP	0.5 THK, X 6.25 Ø P					
	58	4	SA 193 B7	END_CAP_BOLTS	0.5 - 13 UNC X 1 LC	J. WITH 5/8 MIN T	HREAD.			
	29	5	SA 350 LF3	REMOVABLE POCKET TRUNNION	[3.9375 X 13 X 12.37	5 BLOCK				
ŀ	30	6	SA564-630 (HII00)	DOWEL PINS	1 3/8" Ø BAR					
A	_31 _32	1	SA 106 SA 193 B7	DRAIN PIPE	1 SCH 80 X 6 LG AF	PPROX (CUT TO SU	JIT)			
737		33 DELETED			1 - 8UNC X 1.75 LG	ZEI ZCKEW				
Ì	34 2 SA 516 GR. 70 WATER JACKET FND PLATE 1				1 THK. X 91 O.D. X 78 I.D. X 48° APP					
	35	1		DELETED		ווא סף א יעיו ס				
Æ.	36	10	SA 516 GR. 70	ENCLOSURE SHELL PANEL	0.375 THK, X 88.75	D.D. X 168.75 LG.	36 DEG, SHELL SEG	MENT		
	37	1	COMMERCIAL	VENT COUPLING	1	WED HALF COUPLIN	(IR SIMIL AD)			
	38 39	5	COMMERCIAL COMMERCIAL	VENT PLUG	1 1/2-3000 Lb. SCREWED HEXAGON HEAD PLUG (OR SIMILAR)					
S) S)	40	5	COMMERCIAL	PRESSURE RELIEF COUPLING PRESSURE RELIEF VALVE	2"-3000 (b. SCREWE)	-3000 lb. SCREWED HALF COUPLING (OR SIMILAR)				
737	41	1	SA 106	JACKET DRAIN PIPE	MEDIUM PRESSURE POP VALVE (OR SIMILAR)					
A	42	i	COMMERCIAL	JACKET DRAIN VALVE	1 1/2 SCH. 40 X 5 LG. PIPE 1 1/2 NONRISING STEM GATE VALVE (OR SIMILAR)					
	43	4	C/S OR S/S	HOLE PLUGS	1 1/2 NONRISING STEM GATE VALVE (OR SIMILAR)					
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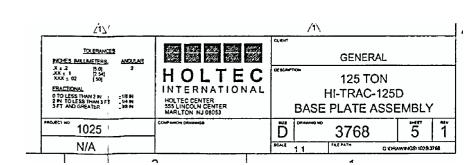
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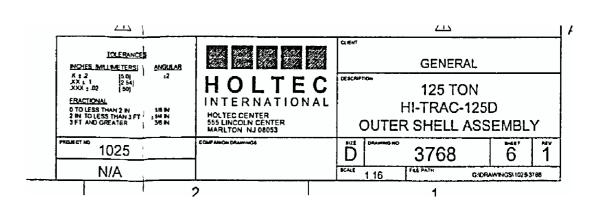
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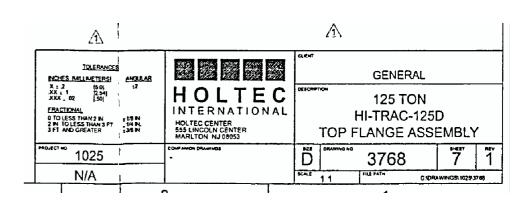


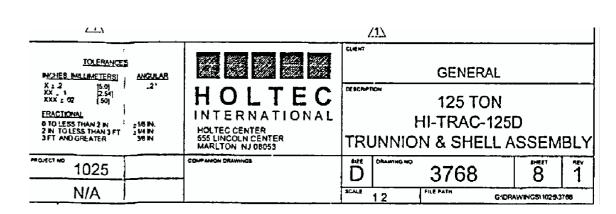


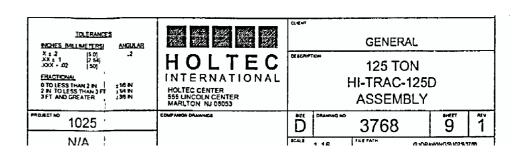


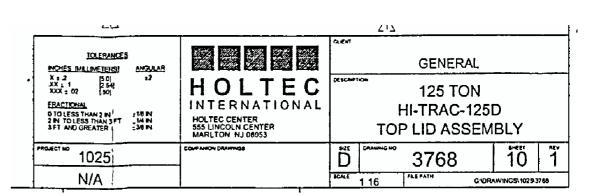


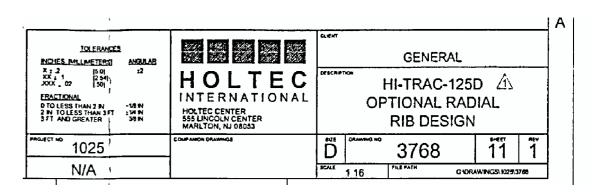












1.6 <u>REFERENCES</u>

- [1.0.1] 10CFR Part 72, "Licensing Requirements for the Storage of Spent Fuel in an Independent Spent Fuel Storage Installation", Title 10 of the Code of Federal Regulations, 1998 Edition, Office of the Federal Register, Washington, D.C.
- [1.0.2] Regulatory Guide 3.61 (Task CE306-4) "Standard Format for a Topical Safety Analysis Report for a Spent Fuel Storage Cask", USNRC, February 1989.
- [1.0.3] NUREG-1536, "Standard Review Plan for Dry Cask Storage Systems", U.S. Nuclear Regulatory Commission, January 1997.
- [1.0.4] American Concrete Institute, "Code Requirements for Nuclear Safety Related Concrete Structures", ACI 349-85, ACI, Detroit, Michigan[†]
- [1.0.5] American Concrete Institute, "Building Code Requirements for Structural Concrete", ACI 318-95, ACI, Detroit, Michigan.
- [1.1.1] ASME Boiler & Pressure Vessel Code, Section III, Subsection NB, American Society of Mechanical Engineers, 1995 with Addenda through 1997.
- [1.1.2] USNRC Docket No. 72-1008, Final Safety Analysis Report for the (Holtec International Storage, Transport, and Repository) HI-STAR System, latest revision.
- [1.1.3] USNRC Docket No. 71-9261, Safety Analysis Report for Packaging for the (Holtec International Storage, Transport, and Repository) HI-STAR System, latest revision.
- [1.1.4] 10CFR Part 50, "Domestic Licensing of Production and Utilization Facilities", Title 10 of the Code of Federal Regulations, 1998 Edition, Office of the Federal Register, Washington, D.C.
- [1.1.5] Deleted.
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- [1.2.2] Directory of Nuclear Reactors, Vol. II, Research, Test & Experimental Reactors, International Atomic Energy Agency, Vienna, 1959.
- [1.2.3] V.L. McKinney and T. Rockwell III, "Boral: A New Thermal-Neutron Shield", USAEC Report AECD-3625, August 29, 1949.

[†] The 1997 edition of ACI-349 is specified for ISFSI pad and embedment design for deployment of the anchored HI-STORM 100A and HI-STORM 100SA

- [1.2.4] Reactor Shielding Design Manual, USAEC Report TID-7004, March 1956.
- [1.2.5] "Safety Analysis Report for the NAC Storable Transport Cask", Revision 8, September 1994, Nuclear Assurance Corporation (USNRC Docket No. 71-9235).
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- [1.2.7] Materials Handbook, 13th Edition, Brady, G.S. and H.R. Clauser, McGraw-Hill, 1991, Page 310.
- [1.2.8] Deleted.
- [1.2.9] ANSI N14.6-1993, "American National Standard for Special Lifting Devices for Shipping Containers Weighing 10,000 Pounds (4500 kg) or More for Nuclear Materials," American National Standards Institute, June, 1993.
- [1.2.10] Deleted.

APPENDIX 1.A: ALLOY X DESCRIPTION

1.A <u>ALLOY X DESCRIPTION</u>

1.A.1 Alloy X Introduction

Alloy X is used within this licensing application to designate a group of stainless steel alloys. Alloy X can be any one of the following alloys:

- Type 316
- Type 316LN
- Type 304
- Type 304LN

Qualification of structures made of Alloy X is accomplished by using the least favorable mechanical and thermal properties of the entire group for all MPC mechanical, structural, neutronic, radiological, and thermal conditions. The Alloy X approach is conservative because no matter which material is ultimately utilized, the Alloy X approach guarantees that the performance of the MPC will meet or exceed the analytical predictions.

This appendix defines the least favorable material properties of Alloy X.

1.A.2 Alloy X Common Material Properties

Several material properties do not vary significantly from one Alloy X constituent to the next. These common material properties are as follows:

- density
- specific heat
- Young's Modulus (Modulus of Elasticity)
- Poisson's Ratio

The values utilized for this licensing application are provided in their appropriate chapters.

1.A.3 Alloy X Least Favorable Material Properties

The following material properties vary between the Alloy X constituents

- Design Stress Intensity (S_m)
- Tensile (Ultimate) Strength (S_u)
- Yield Strength (S_v)
- Coefficient of Thermal Expansion (á)

Coefficient of Thermal Conductivity (k)

Each of these material properties are provided in the ASME Code Section II [1.A.1]. Tables 1.A.1 through 1.A.5 provide the ASME Code values for each constituent of Alloy X along with the least favorable value utilized in this licensing application. The ASME Code only provides values to -20°F. The design temperature of the MPC is -40°F to 725°F as stated in Table 1.2.3. Most of the above-mentioned properties become increasingly favorable as the temperature drops. Conservatively, the values at the lowest design temperature for the HI-STAR 100 System have been assumed to be equal to the lowest value stated in the ASME Code. The lone exception is the thermal conductivity. The thermal conductivity decreases with the decreasing temperature. The thermal conductivity value for -40°F is linearly extrapolated from the 70°F value using the difference from 70°F to 100°F.

The Alloy X material properties are the minimum values of the group for the design stress intensity, tensile strength, yield strength, and coefficient of thermal conductivity. Using minimum values of design stress intensity is conservative because lower design stress intensities lead to lower allowables that are based on design stress intensity. Similarly, using minimum values of tensile strength and yield strength is conservative because lower values of tensile strength and yield strength lead to lower allowables that are based on tensile strength and yield strength. When compared to calculated values, these lower allowables result in factors of safety that are conservative for any of the constituent materials of Alloy X. Further discussion of the justification for using the minimum values of coefficient of thermal conductivity is given in Chapter 3. The maximum and minimum values are used for the coefficient of thermal expansion of Alloy X. The maximum and minimum coefficients of thermal expansion are used as appropriate in this submittal. Figures 1.A.1-1.A.5 provide a graphical representation of the varying material properties with temperature for the Alloy X materials.

1.A.4 References

[1.A.1] ASME Boiler & Pressure Vessel Code Section II, 1995 ed. with Addenda through 1997.

 $\label{eq:table 1.A.1} \mbox{ALLOY X AND CONSTITUENT DESIGN STRESS INTENSITY (S_m) vs. TEMPERATURE}$

Temp. (°F)	Туре 304	Type 304LN	Туре 316	Type 316LN	Alloy X (minimum of constituent values)
-40	20.0	20.0	20.0	20.0	20.0
100	20.0	20.0	20.0	20.0	20.0
200	20.0	20.0	20.0	20.0	20.0
300	20.0	20.0	20.0	20.0	20.0
400	18.7	18.7	19.3	18.9	18.7
500	17.5	17.5	18.0	17.5	17.5
600	16.4	16.4	17.0	16.5	16.4
650	16.2	16.2	16.7	16.0	16.0
700	16.0	16.0	16.3	15.6	15.6
750	15.6	15.6	16.1	15.2	15.2
800	15.2	15.2	15.9	14.9	14.9

- 1. Source: Table 2A on pages 314, 318, 326; and 330 of [1.A.1].
- 2. Units of design stress intensity values are ksi.

 $\label{eq:table 1.A.2} \mbox{ALLOY X AND CONSTITUENT TENSILE STRENGTH (S_u) vs. TEMPERATURE}$

Temp. (°F)	Type 304	Type 304LN	Туре 316	Type 316LN	Alloy X (minimum of constituent values)
-40	75.0	75.0	75.0	75.0	75.0
100	75.0	75.0	75.0	75.0	75.0
200	71.0	71.0	75.0	75.0	71.0
300	66.0	66.0	73.4	70.9	66.0
400	64.4	64.4	71.8	67.1	64.4
500	63.5	63.5	71.8	64.6	63.5
600	63.5	63.5	71.8	63.1	63.1
650	63.5	63.5	71.8	62.8	62.8
700	63.5	63.5	71.8	62.5	62.5
750	63.1	63.1	71.4	62.2	62.2
800	62.7	62.7	70.9	61.7	61.7

- 1. Source: Table U on pages 437, 439, 441, and 443 of [1.A.1].
- 2. Units of tensile strength are ksi.

Temp. (°F)	Type 304	Type 304LN	Type 316	Type 316LN	Alloy X (minimum of constituent values)
-40	30.0	30.0	30.0	30.0	30.0
100	30.0	30.0	30.0	30.0	30.0
200	25.0 ·	- 25.0	⁻ 25.8	25.5	25.0
300	22.5	22.5	23.3	22.9	22.5
400	20.7	20.7	21.4	21.0	20.7
500	19.4	19.4	19.9	19.4	19.4
600	18.2	18.2	18.8	18.3	18.2
650	17.9	17.9	18.5	17.8	17.8
700	17.7	17.7	18.1	17.3	17.3
750	17.3	17.3	17.8	16.9	16.9
800	16.8	16.8	17.6	16.6	16.6

- 1. Source: Table Y-1 on pages 518, 519, 522, 523, 530, 531, 534, and 535 of [1.A.1].
- 2. Units of yield stress are ksi.

Table 1.A.4

ALLOY X AND CONSTITUENT COEFFICIENT OF THERMAL EXPANSION vs. TEMPERATURE

Temp. (°F)	Type 304 and Type 304LN	Type 316 and Type 316LN	Alloy X Maximum	Alloy X Minimum
-40	8.55	8.54	8.55	8.54
100	8.55	8.54	8.55	8.54
150	8.67	8.64	8.67	8.64
200	8.79	8.76	8.79	8.76
250	8.90	8.88	8.90	8.88
300	9.00	8.97	9.00	8.97
350	9.10	9.11	9.11	9.10
400	9.19	9.21	9.21	9.19
450	9.28	9.32	9.32	9.28
500	9.37	9.42	9.42	9.37
550	9.45	9.50	9.50	9.45
600	9.53	9.60	9.60	9.53
650	9.61	9.69	9.69	9.61
700	9.69	9.76	9.76	9.69
750	9.76	9.81	9.81	9.76
800	9.82	9.90	9.90	9.82

- 1. Source: Table TE-1 on pages 590 and 591 of [1.A.1].
- 2. Units of coefficient of thermal expansion are in./in.-°F x 10⁻⁶.

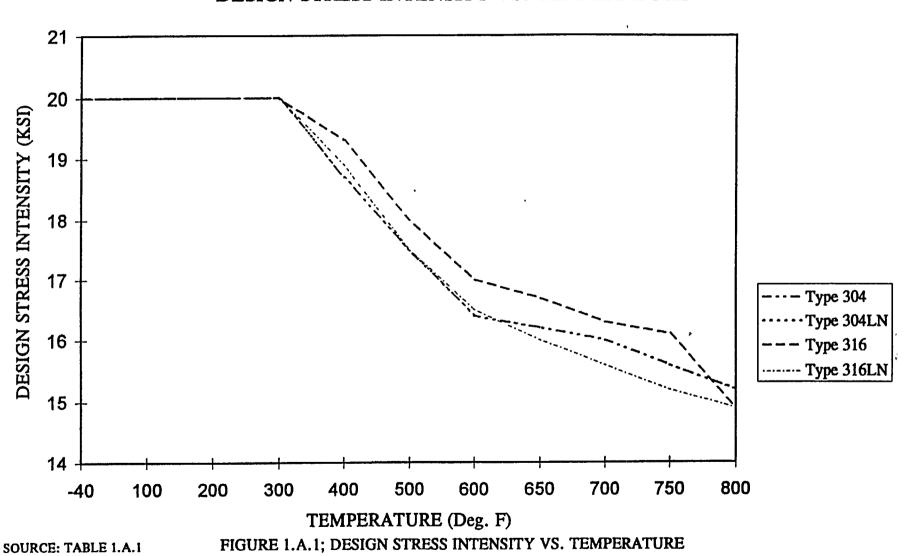
Table 1.A.5

ALLOY X AND CONSTITUENT THERMAL CONDUCTIVITY vs. TEMPERATURE

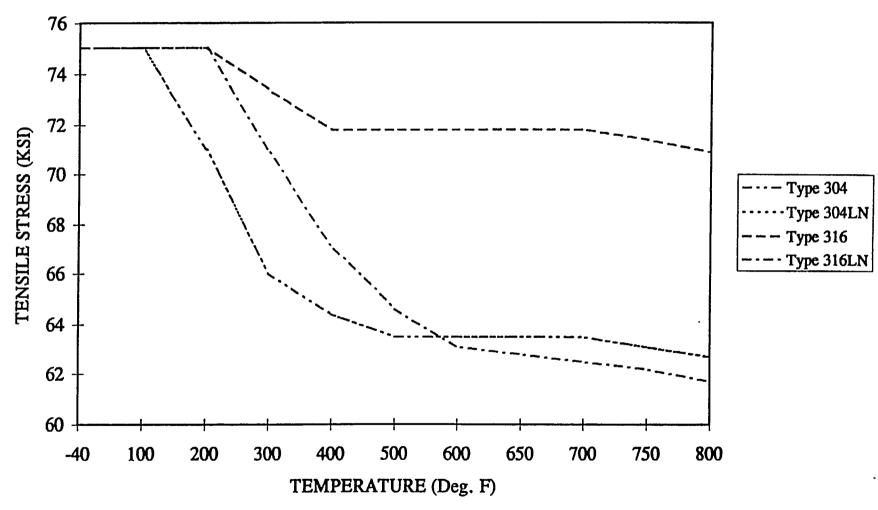
Temp. (°F)	Type 304 and Type 304LN	Type 316 and Type 316LN	Alloy X (minimum of constituent values)
-40	8.23	6.96	6.96
70	8.6	7.7	7.7
100	8.7	7.9	7.9
150	9.0	8.2	8.2
200	9.3	8.4	8.4
250	9.6	8.7	8.7
300	9.8	9.0	9.0
350	10.1	9.2	9.2
400	10.4	9.5	9.5
450	10.6	9.8	9.8
500	10.9	10.0	10.0
550	11.1	10.3	10.3
600	11.3	10.5	10.5
650	11.6	10.7	10.7
700	11.8	11.0	11.0
750	12.0	11.2	11.2
800	12.2	11.5	11.5

- 1. Source: Table TCD on page 606 of [1.A.1].
- 2. Units of thermal conductivity are Btu/hr-ft-°F.

DESIGN STRESS INTENSITY VS. TEMPERATURE



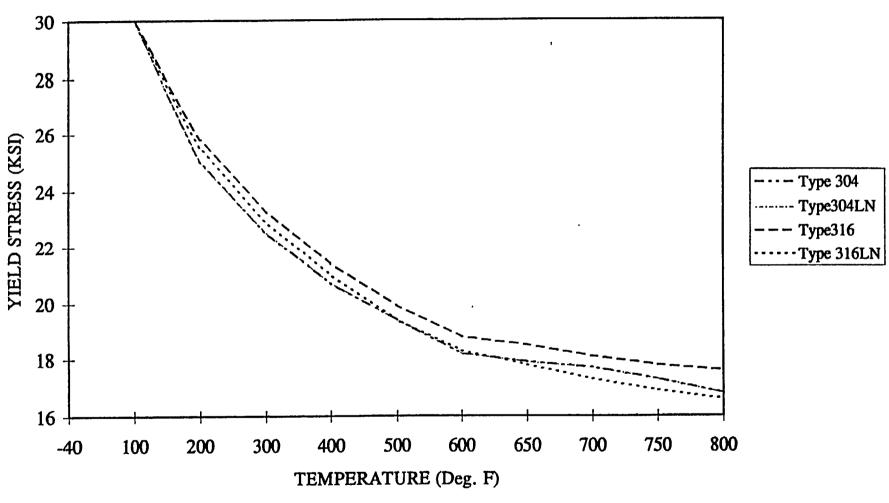
TENSILE STRENGTH VS. TEMPERATURE



SOURCE: TABLE 1.A.2

FIGURE 1.A.2; TENSILE STRENGTH VS. TEMPERATURE

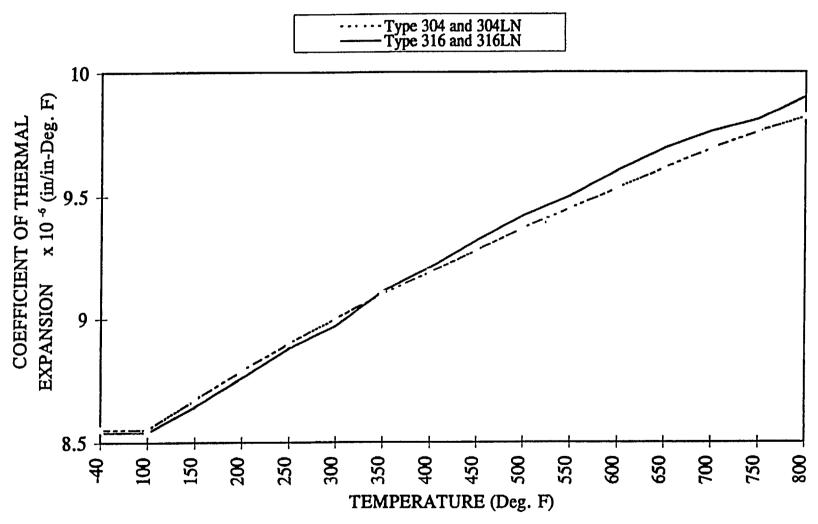
YIELD STRESS VS. TEMPERATURE



SOURCE: TABLE 1.A.3

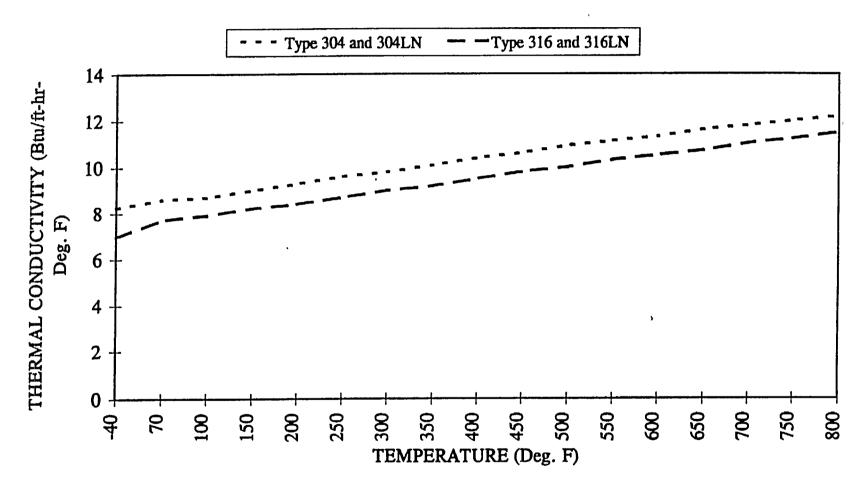
FIGURE 1.A.3; YIELD STRESS VS. TEMPERATURE

COEFFICIENT OF THERMAL EXPANSION VS. TEMPERATURE



SOURCE: TABLE 1.A.4 FIGURE 1.A.4; COEFFICIENT OF THERMAL EXPANSION VS. TEMPERATURE

THERMAL CONDUCTIVITY VS. TEMPERATURE



SOURCE: TABLE 1.A.5

FIGURE 1.A.5; THERMAL CONDUCTIVITY VS. TEMPERATURE

APPENDIX 1.B: HOLTITE TM MATERIAL DATA

The information provided in this appendix describes the neutron absorber material, Holtite-A for the purpose of confirming its suitability for use as a neutron shield material in spent fuel storage casks. Holtite-A is one of the family of Holtite neutron shield materials denoted by the generic name HoltiteTM. It is currently the only neutron shield material approved for installation in the HI-STAR 100 cask. It is chemically identical to NS-4-FR which was originally developed by Bisco Inc. and used for many years as a shield material with B_4C or Pb added.

Holtite-A contains aluminum hydroxide (Al(OH)₃) in an epoxy resin binder. Aluminum hydroxide is also known by the industrial trade name of aluminum tri-hydrate or ATH. ATH is often used commercially as a fire-retardant. Holtite-A contains approximately 62% ATH supported in a typical 2-part epoxy resin as a binder. Holtite-A contains 1% (nominal) by weight B₄C, a chemically inert material added to enhance the neutron absorption property. Pertinent properties of Holtite-A are listed in Table 1.B.1.

The essential properties of Holtite-A are:

- 1. the hydrogen density (needed to thermalize neutrons),
- 2. thermal stability of the hydrogen density, and
- 3. the uniformity in distribution of B₄C needed to absorb the thermalized neutrons.

ATH and the resin binder contain nearly the same hydrogen density so that the hydrogen density of the mixture is not sensitive to the proportion of ATH and resin in the Holtite-A mixture. B₄C is added as a finely divided powder and does not settle out during the resin curing process. Once the resin is cured (polymerized), the ATH and B₄C are physically retained in the hardened resin. Qualification testing for B₄C throughout a column of Holtite-A has confirmed that the B₄C is uniformly distributed with no evidence of settling or non-uniformity. Furthermore, an excess of B₄C is specified in the Holtite-A mixing and pouring procedure as a precaution to assure that the B₄C concentration is always adequate throughout the mixture.

The specific gravity specified in Table 1.B.1 does not include an allowance for weight loss. The specific gravity assumed in the shielding analysis includes a 4% reduction to conservatively account for potential weight loss at the design temperature of 300°F or an inability to reach theoretical density. Tests on the stability of Holtite-A were also performed by Holtec International. The results of the tests are summarized in Holtec Reports HI-2002396, "Holtite-A Development History and Thermal Performance Data" and HI-2002420, "Results of Pre- and Post-Irradiation Test Measurements." The information provided in these reports demonstrates that Holtite-ATM possesses the necessary thermal and radiation stability characteristics to function as a reliable shielding material in the HI-STAR 100 overpack.

The Holtite-A is encapsulated in the HI-STAR 100 overpack and, therefore, should experience a very small weight reduction during the design life of the HI-STAR 100 System. The data and test results confirm that

Holtzte-A remains stable under design thermal and radiation conditions, the material properties meet or exceed that assumed in the shielding analysis, and the B_4C remains uniformly distributed with no evidence of settling or non-uniformity.

Based on the information described above, Holtite-A meets all of the requirements for an acceptable neutron shield material.

Table 1.B.1

REFERENCE PROPERTIES OF HOLTITE-A NEUTRON SHIELD MATERIAL

PHYSICAL PROPERTIES	
% ATH	62 nominal
Specific Gravity	1.68 g/cc nominal
Max. Continuous Operating Temperature	300°F
Hydrogen Density	0.096 g/cc minimum
Radiation Resistance	Excellent
CHEMICAL PROPERTIES (Nominal)	
wt% Aluminum	21.5
wt% Hydrogen	6.0
wt% Carbon	27.7
wt% Oxygen	42.8
wt% Nitrogen	2.0
wt% B ₄ C	up to 6.5 (Holtite-A uses 1% B ₄ C) 1.0

PAGES 1.B-4 THROUGH 1.B-20 INTENTIONALLY DELETED

APPENDIX 1.C: MISCELLANEOUS MATERIAL DATA (Total of 6 Pages Including This Page)

The information provided in this appendix specifies the paint properties and demonstrates their suitability for use in spent nuclear fuel storage casks. The following is a listing of the information provided.

• Thermaline 450, Carboline, Product Data Sheet and Application Instructions

Thermaline 450 or equivalent is specified to coat the overpack to the maximum extent practical and the inner cavity of the HI-TRAC transfer cask. Carboline 890 or equivalent is specified to coat external surfaces of the HI-TRAC transfer cask. As can be seen from the product data sheets, the paints are suitable for the design temperatures (see Table 2.2.3) and the environment.

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product data sheet

THERMALINE 450

VOC#

SELECTION DATA

GENERIC TYPE: A glass flake filled, phenolic modified, amine cured epoxy novalac.

GENERAL PROPERTIES: A dense cross-linked polymer which exhibits outstanding barrier protection against a variety of chemical exposures. Excellent resistance to wet/dry cycling conditions at elevated temperatures. Designed to coat the exterior of insulated piping. It is also suitable for coating non-insulated piping and equipment exposed to chemical attack. The glass flakes help provide excellent abrasion resistance, permeation resistance and internal reinforcement.

- Temperature resistance to 450°F
- Excellent abrasion resistance
- Excellent overall chemical resistance
- Excellent thermal shock resistance

RECOMMENDED USES: Typically used as a one coat system to coat pipes and tanks that will be insulated. May also be used to coat non-insulated pipe, structural steel, equipment or concrete that may be subjected to severe chemical attack, abrasion or other abuse typical of a chemical plant environment.

TYPICAL CHEMICAL RESISTANCE:

Exposure	Spiesh & Spillage	Eumes
Acids	Excellent	Excellent
Alkalies	Excellent	Excellent
Solvents	Excellent	Excellent
Salt 🗦 🛴	Excellent	Excellent
Water	Excellent	Excellent

TEMPERATURE RESISTANCE (Under insulation):

Continuous: 425°F (218°C) Excursions to: 450°F (232°C)

At 200°F (93°C) coating discoloration may be observed without loss of film integrity.

SUBSTRATES: Apply over properly prepared steel.

COMPATIBLE COATINGS: Normally applied directly to substrate. May be applied over epoxies and phenolics as recommended. May be topcoated with epoxies, polyurethanes or other finish coats as recommended.

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SPECIFICATION DATA

THEORETICAL SOLIDS CONTENT OF MIXED MATERIAL:

THERMALINE 450 "

8v Volume 70 ± 2%

VOLATRE ORGANIC CONTENT (VOC):
The following are nominal values:
As supplied: 2.13 lbs./gal. (255 gm./liter).

RECOMMENDED DRY FILM THICKNESS: 8-10 mils (200-250 microns) to be achieved in 1 or 2 coats.

THEORETICAL COVERAGE PER MIXED GALLON:

1,117 mil sq. ft. (27.9 sq.m/l at 25 microns)

139 sq. ft at 8 mils (3.5 sq. m/l at 200 microns)

111 sq. ft at 10 mils (2.8 sq.m/l at 250 microns)

*Mixing and application losses will vary and must be taken into consideration when estimating job require ments.

STORAGE CONDITIONS: Store indoors
Temperature: 40-110°F (4-43°C) Humidity: 0.90%

SHELF LIFE: 24 months when stored indoors at 75°F (24°C)

COLOR: Red (0500) and Gray (5742)

GLOSS: Low (Epoxies lose gloss, discolor and eventually chalk in sunlight exposure.)

ORDERING INFORMATION

Prices may be obtained from your Carboline Sales Representative or Carboline Customer Service Department.

APPROXIMATE SHIPPING WEIGHT:

THERMALINE 450 12 lbs. (5.5 kg) 58 lbs. (26.3 kg)

Thinner 213 8.4 lbs. (3.8 kg) 41 lbs. (18.6 kg)

FLASH POINT: (Setaflash)
THERMALINE 450 Part A:
THERMALINE 450 Part B:
Thinner 213

53°F (12°C)
>200°F (>93°C)

To the best of our branchings the technical data certained herein are true and accurate at the date of issuance and are subject to change without prior notice. User must certain Carbains Campany to verify corrections before specifying or ordering. No guarantee of accuracy is given at implied. We quarantee our products to conform to Carbains our results from the carbains or injuries resulting from time. Liability, if any, is limited to replacement of products in conform to Carbains oue to have, an accuracy of the conformation of the conforma

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APPLICATION INSTRUCTIONS

THERMALINE 450

These restructures are not intended to show product recommendations for specific service. They are issued as an aid in determining serricit surface properation, making sustrations and aspectators produce. It is assumed that the proper product recommendations have been made. These sustrations should be followed electly to obtain the maximum service from the materials.

SURFACE PREPARATION: Remove all oil or grease from surface to be coated with Thinner 2 or Surface Cleaner 3 (refer to Surface Cleaner 3 instructions) in accordance with SSPC-SP 1.

STEEL:

Not insulated: Abrasive blast to a Commercial Finish in accordance with SSPC-SP 6 and obtain a 2-3 mil (50-75 micron) blast profile.

Under Insulation: Abrasive blast to a Near White Finish in accordance with SSPC-SP 10 and obtain a 2-3 (50-75 micron) blast profile.

MIXING: Power mix each component separately, then combine and power mix in the following proportions.

Allow 30 minutes induction time at 75°F (24°C) prior to use.

THERMALINE 450 Part A: 0.8 gals. 4.0 gals. THERMALINE 450 Part B: 0.2 gals. 1.0 gals.

THINNING: May be thinned up to 13 oz/gal with Thinner 213.

Use of thinners other than those supplied or approved by Carboline may adversely affect product performance and void product warranty, whether express or implied.

POT LIFE: Three hours at 75°F (24°C) and less at higher temperatures. Pot life ends when coating loses body and begins to sag.

APPLICATION CONDITIONS:

	<u>Material</u>	Surfaces	<u>Ambient</u>	Humidity
Normal	65-85°F	65-85°F	65-85°F	30-60%
	(18-29°C)	(18-29°C)	(18-29°C)	
Minimum	55°F (13°C)	50°F (10°C)	50°F (10°C)	0%
Maximum	90°F (32°C)	110°F (43°C)	100°F (38°C)	R5%

Do not apply when the surface temperature is less than 5°F or 3°C above the dew point.

Special thinning and application techniques may be required above or below normal conditions.

SPRAY: The following spray equipment has been found suitable and is available from manufacturers such as Binks, DeVilbiss and Graco.

Conventional: Pressure pot equipped with dual regulators, 1/2" I.D. minimum material hose, .110" I.D. fluid tip and appropriate air cap.

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Airless:

 Pump Ratio:
 30:1 (min)*

 GPM Output:
 3.0 (min)

 Material Hose:
 1/2* I.D. (min)

 Tip Size:
 .035*-.041*

 Output psl:
 2200-2500

*Teflon packings are recommended and are available from the pump manufacturer.

BRUSH: For striping of welds, touch-up of small areas only. Use a natural bristle brush, applying full strokes Avoid rebrushing.

ROLLER: Not recommended.

DRYING TIMES: These times are based on a dry film thickness of 10 mils (250 microns). Higher film thickness, insufficient ventilation or cooler temperatures will require longer cure times and could result in solvent entrapment and premature failure.

Surface Temperature	Dry To Hendle	Dry to Topcost	Final Cure
50°F (10°C)	18 hours	48 hours	21 days
60°F (16°C)	12 hours	32 hours	14 days
75°F (24°C)	6 hours	15 hours	7 days
90°F (32°C)	3 hours	8 hours	4 days

If the final cure time has been exceeded, the surface must be abraded by sweep blasting prior to the application of any additional coats.

EXCESSIVE HUMIDITY OR CONDENSATION ON THE SURFACE DURING CURING MAY RESULT IN A SURFACE HAZE OR BLUSH; ANY HAZE OR BLUSH MUST BE REMOVED BY WATER WASHING BEFORE RECOATING.

VENTILATION & SAFETY: WARNING: VAPORS MAY CAUSE EXPLOSION. When used in enclosed areas, thorough air circulation must be used during and after application until the coating is cured. The ventilation system should be capable of preventing the solvent vapor concentration from reaching the lower explosion limit for the solvents used. In addition to insuring proper ventilation, fresh air respirators or fresh air hoods must be used by all application personnel Where flammable solvents exist, explosion-proof lighting must be used. Hypersensitive persons should wear clean, protective clothing, gloves and/or protective cream on face, hands and all exposed areas

CLEANUP: Use Thinner 2.

CAUTION: READ AND FOLLOW ALL CAUTION STATE-MENTS ON THIS PRODUCT DATA SHEET AND ON THE MATERIAL SAFETY DATA SHEET FOR THIS PRODUCT.

CAUTION CONTAINS FLAMMABLE SOLVENTS. KEEP AWAY FROM SPARKS AND OPEN FLAMES. WORKMEN IN CONFINED AREAS MUST WEAR FRESH AIRLINE RESPIRATORS HYPERSENSITIVE PERSONS SHOULD WEAR GLOVES OR USE PROTECTIVE CREAM. ALL ELECTRICAL EQUIPMENT AND RESTALLATIONS SHOULD SE MADE IN ACCORDANCE WITH THE MONSPARCING SHOES. IN AREAS WHERE EXPLOSION HAZARDS EXIST, WORKMEN SHOULD SE REQUIRED TO USE NONFERROUS TOOLS AND TO WEAR CONDUCTIVE AND



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APPENDIX 1.D: Requirements on HI-STORM 100 Shielding Concrete

1.D.1 Introduction

The HI-STORM 100 overpack utilizes plain concrete for neutron and gamma shielding. While most of the shielding concrete used in the HI-STORM 100 overpack is installed in the annulus between the concentric structural shells, smaller quantities of concrete are also present in the pedestal shield and the overpack lid. Because plain concrete has little ability to withstand tensile stresses, but is competent in withstanding compressive and bearing loads, the design of the HI-STORM 100 overpack places no reliance on the tension-competence of the shielding concrete. ACI 318-95 provides formulas for permissible compressive and bearing stresses in plain concrete which incorporate a penalty over the corresponding permissible values in reinforced concrete. The formulas for permissible compressive and bearing stresses set forth in ACI 318-95 are used in calculations supporting this TSAR in load cases involving compression or bearing loads on the overpack concrete. However, since ACI 318-95 is intended for commercial applications and the overpack concrete is designated as an ITS Category B material, it is necessary to invoke provisions of ACI 349 (85) (which is sanctioned by NUREG-1536) for all requirements except for the allowable stress formulas (which do not exist in ACI 349) and load combinations. This appendix provides a complete set of criteria applicable to the plain concrete in the HI-STORM 100 overpack.

1.D.2 <u>Design Requirements</u>

The primary function of the plain concrete is to provide neutron and gamma shielding. As plain concrete is a competent structural member in compression, the plain concrete's effect on the performance of the HI-STORM overpack is included. The formulas for permissible compressive and bearing stresses set forth in ACI 318-95 are used. However, as plain concrete has very limited capabilities in tension, no tensile strength is allotted to the concrete.

The steel structure of the HI-STORM overpack provides the strength to meet all load combinations specified in Chapters 2 and 3. Credit for the structural strength of the plain concrete is limited to the compressive load carrying capability of the concrete in calculations appropriate to handling and transfer operations, and to demonstrate that the HI-STORM 100 System continues to provide functional performance in a post-accident environment. Therefore, the load combinations provided in ACI 349 and NUREG-1536, Table 3-1 are not applied to the plain concrete.

The shielding performance of the plain concrete is maintained by ensuring that the allowable concrete temperature limits are not exceeded. The thermal analyses for normal and off-normal conditions demonstrate that the plain concrete does not exceed the allowable long term temperature limit provided in Table 1.D.1. Under accident conditions, the bulk of the plain concrete in the HI-STORM overpack does not exceed the allowable short term temperature limit provided in Table 1.D.1. Any portion of the plain concrete which exceeds the short term temperature limit under accident conditions is neglected in the post-accident shielding analysis and in any post-accident structural analysis.

1.D.3 Material Requirements

Table 1.D.1 provides the material limitations and requirements applicable to the overpack plain concrete. These requirements are drawn from ACI 349 (85) supplemented by the provisions of NUREG 1536 (page 3-21) and standard good practice. Two different minimum concrete densities are specified for the overpack concrete, based on the presence or absence of the steel shield shell.

1.D.4 Construction Requirements

The HI-STORM 100 overpack is composed of a steel structure that houses plain concrete. The steel structure acts as the framework for the pouring of the concrete. The steel structure defines the dimensions of the concrete which ensures that the required thickness of concrete is provided. The fabrication sequence for the HI-STORM 100 overpack as it pertains to the concrete is provided below. All item numbers are taken from the design drawings in Section 1.5. All nomenclature is taken from bills-of-material in Section 1.5.

The steel structure of the HI-STORM 100 overpack body is assembled at a qualified steel fabrication facility. However, access remains to the annulus formed by the overpack inner and outer shells (Items 3 and 2, respectively); likewise, the pedestal shell (Item 5) is welded to the baseplate (Item 1) and the pedestal platform (Item 24) to form the pedestal cavity, but penetrations exist in the baseplate to allow placement of concrete. The steel structure of the overpack body is transported to the reactor site or a nearby concrete facility.

Once the steel structure of the body is received, the body will be inspected to ensure the steel structure meets the requirements of Sections 5.1 and 6.1 of ACI 349. The concrete shall be mixed, conveyed, and deposited in accordance with Sections 5.2 through 5.4 of ACI 349. Sufficient rigidity in the steel structure overpack body is provided such that all the concrete may be placed in a single pour into each of the four segments formed by the inner shell (Item 3), outer shell (Item 2), and radial plates (Item 14). If more than one pour is performed, the requirements of Section 6.4 of ACI 349 must be met for construction joints. The pedestal shell may require bracing and support in accordance with Section 6.1 of ACI 349 to maintain the proper position and shape.

Mixing and placing of the concrete shall follow the guidance of Sections 5.6 and 5.7 for cold and hot weather conditions, respectively. Consolidation of the plan concrete shall be performed in accordance with ACI 309-87. As no reinforcement is placed in the concrete, the possibility of voids is greatly diminished. Curing of the concrete shall be in accordance with Section 5.5 of ACI 349. Water curing or accelerated curing using sealing materials methods may be used as described in ACI 308-92, Standard Practice for Curing Concrete. This would include the use of either a plastic film or a curing compound.

Non-shrink grout shall be applied as necessary to account for any deviation of the concrete elevation To fabricate the overpack lid an identical process is followed.

Table 1.D.1 provides the construction limitations and requirements applicable to the overpack plain concrete. These requirements are drawn from ACI 349 (85).

1.D.5 <u>Testing Requirements</u>

Table 1.D.2 provides the testing requirements applicable to the overpack plain concrete. These requirements are drawn from ACI 349 (85).

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Table 1.D.1: Requirements for Plain Concrete

ITEM	APPLICABLE LIMIT OR REFERENCE
Density in overpack body (Minimum)	146 lb/ft3 (HI-STORM 100 up to Serial Number (S/N) 7),
	155 lb/ft3 (HI-STORM 100 S/N 8 and higher, and HI-
	STORM 100S)
Density in lid and pedestal (Minimum)	146 lb/ft³
Specified Compressive Strength	3,300 psi (min.)
Compressive and Bearing Stress Limit	Per ACI 318-95
Cement Type and Mill Test Report	Type II; Section 3.2 (ASTM C 150 or ASTM C595)
Aggregate Type	Section 3 3 (including ASTM C33(Note 2))
Nominal Maximum Aggregate Size	1 (inch)
Water Quality	Per Section 3.4
Material Testing	Per Section 3 1
Admixtures	Per Section 3 6
Maximum Water to Cement Ratio	0.5 (Table 4.5 2)
Maximum Water Soluble Chloride Ion Cl in Concrete	1 00 percent by weight of cement (Table 4 5.4)
Concrete Quality	Per Chapter 4 of ACI 349
Mixing and Placing	Per Chapter 5 of ACI 349
Consolidation	Per ACI 309-87
Quality Assurance	Per Holtec Quality Assurance Manual, 10 CFR Part 72, Appendix G commitments
Maximum Local Temperature Limit Under Long Term Conditions	200°F (See Note 3)
Maximum Section Average Temperature Limit Under Short Term Conditions	350°F (Appendix A, Subsection A 4 2)
Aggregate Maximum Value ² of Coefficient of Thermal	6E-06 inch/inch/°F
Expansion (tangent in the range of 70°F to 100°F)	(NUREG-1536, 3 V 2 b i (2)(c)2 b)

1

- 1. All section and table references are to ACI 349 (85)
- 2. The coarse aggregate shall meet the requirements of ASTM C33 for class designation 1S from Table 3. However, if the requirements of ASTM C33 cannot be met, concrete that has been shown by special tests or actual service to produce concrete of adequate strength and durability meeting the requirements of Tables 1.D 1 and 1.D.2 is acceptable in accordance with ACI 349 Section 3.3.2.
- 3. The 200 °F long term temperature limit is specified in accordance with Paragraph A 4.3 of ACI 349 for normal conditions. The 200 °F long term temperature limit is based on (1) the use of Type II cement, specified aggregate criteria, and the specified compressive stress in Table 1 D 1, (2) the relatively small increase in long term temperature limit over the 150°F specified in Paragraph A 4.1, and (3) the very low maximum stresses calculated for normal and off-normal conditions in Section 3.4 of this FSAR.

The following aggregate types are a priori acceptable limestone, dolomite, marble, basalt, granite, gabbro, or rhyolite. The thermal expansion coefficient limit does not apply when these aggregates are used. Careful consideration shall be given to the potential of long-term degradation of concrete due to chemical reactions between the aggregate and cement selected for HI-STORM 100 overpack concrete

Table 1.D.2: Testing Requirements for Plain Concrete

TEST	SPECIFICATION
Compression Test	ASTM C31, ASTM C39, ASTM C192
Unit Weight (Density)	ASTM C138
Maximum Water Soluble Chloride Ion Concentration	Federal Highway Administration Report FHWA-RD-77-85, "Sampling and Testing for Chloride Ion in Concrete"