

UNITED STATES NUCLEAR REGULATORY COMMISSION

WASHINGTON, D.C. 20555-0001

March 21, 2000

LICENSEE: Baltimore Gas and Electric Company

FACILITY: Calvert Cliffs Nuclear Power Plant, Unit Nos. 1 and 2

SUBJECT: SUMMARY OF THE DECEMBER 14, 1999, MEETING REGARDING CORROSION BEHAVIOR OF FUEL CLADDING AT CALVERT CLIFFS NUCLEAR POWER PLANT, UNIT NOS. 1 AND 2 (TAC NOS. MA6875 AND MA6876)

On December 14, 1999, the Nuclear Regulatory Commission (NRC) staff held a meeting at the NRC offices in Rockville, Maryland with representatives from Baltimore Gas and Electric Company (BGE) the licensee for Calvert Cliffs Nuclear Power Plant, Unit Nos. 1 and 2 and their consultants ABB - Combustion Engineering Nuclear Power, Inc. (ABB - CENP) to discuss corrosion behavior of fuel cladding at Calvert Cliffs Nuclear Power Plant, Unit Nos. 1 and 2. Enclosure 1 is a list of attendees. Enclosure 2 is a copy of the nonproprietary viewgraphs distributed at the meeting.

The licensee stated that an inspection was performed on fuel that had been discharged from Unit 2 at the end of Cycle 12 and on a lead assembly. As part of the inspection, visual examinations were performed on several high duty fuel assemblies, assemblies that had seen a high rate of burnup in the two cycles in which they were in the core. The visual examinations resulted in the observation that some fuel rods exhibited blistering of the oxide layer, and some fuel rods showed evidence of early stages of spalling.

Based on these observations, several assemblies were taken apart for more detailed inspection of individual fuel rods. The fuel rods were visibly examined and the oxide layer thickness were measured on some of the rods. Some fuel rods, particularly peripheral fuel rods, had measured oxide thicknesses that were higher than predicted by the vendor's corrosion model.

The licensee then described the immediate actions taken which included a voluntary Licensee Event Report (LER), initiating a root cause evaluation and performing an operability evaluation to support current cycles operation. The root cause evaluation concluded that the factors affecting fuel duty are the primary contributors to the unexpected behavior. These factors include: improved operating history, reduced reactor coolant system flow due to plugged steam generator tubes, rod location within the assembly, rod power and adjacent rod power, subcooled boiling and thermal hydraulics effects due to geometry. The operability evaluation determined that there was no concern for normal operation. In addition, it addressed accidents and transients. A preliminary fuel duty model was developed by ABB CENP which uses an improved corrosion model. A fuel duty index was evaluated which is a function of time and temperature. Fuel duty comparisons were made between CC2N and past and current batches which showed fuel duties for current cycles and CC2N are similar. Based on these comparisons, the licensee concluded that the current cores are operable. Finally, the licensee indicated that near term cores (up to and including Unit 2 Cycle 14 (U2C14)) will be evaluated

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by the same approach under 10 CFR 50.59. Beyond U2C14 fuel behavior is expected to be different due to replacement of steam generators (greater flow), use of the TURBO assembly design and use of an advanced cladding alloy. In addition, the licensee stated its intention to continue to examine the fuel and to keep the NRC informed of its findings.

/RA/

Alexander W. Dromerick, Sr. Project Manager, Section 1 Project Directorate I Division of Licensing Project Management Office of Nuclear Reactor Regulation

Docket Nos. 50-317 and 50-318

Enclosures: 1. List of Attendees 2. Licensee's Handout

cc w/encls: See next page

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Calvert Cliffs Nuclear Power Plant Unit Nos. 1 and 2

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LIST OF ATTENDEES

BALTIMORE GAS AND ELECTRIC COMPANY

DECEMBER 14, 1999

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i.

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Corrosion Behavior of OPTIN Cladding at Calvert Cliffs

Presented by Penney File BGE December 14, 1999

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Purpose

- Describe Inspections and Observations
- Summarize Evaluation Supporting Operability of Current Cores
- Describe Approach for U1C15

Outline

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- Describe Inspections and Observations
- Describe Immediate Actions
- Describe Longer Term Actions
- Summarize

Calvert Cliffs Background

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- 24 Month Cycles
- 650 EFPD
- Tcold 546.5
- Thot 592
- Average LHGR 6.25 Kw/Ft
- Tech Spec Fr 1.65
- High Duty 2 24 Month Cycles
- Low Duty 3 24 Month Cycles

Calvert Cliffs Fuel Assembly Schematic

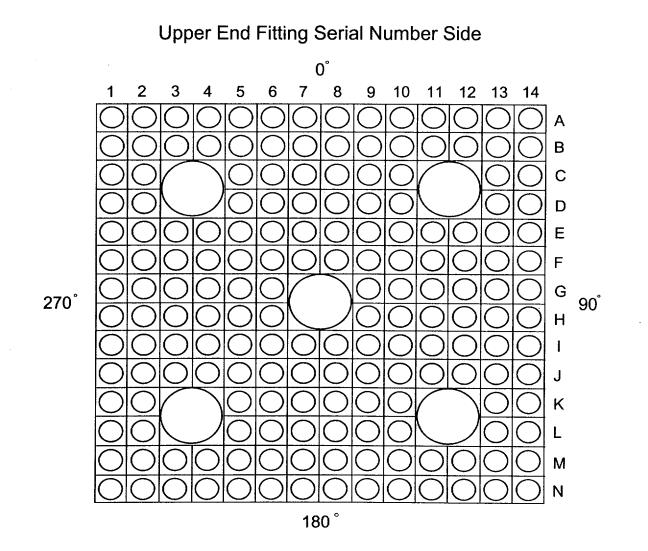


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Outline

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- Describe Inspections and Observations
- Describe Immediate Actions
- Describe Longer Term Actions
- Summarize

July 1999 Initial Inspection Scope

- C2NT Test Assemblies Discharged in Spring 1999
 - 4 Assemblies Visually Examined
 - 1 Assembly Reconstituted to Allow ECT and Oxide Thickness Measurement []
- Visual Examination of Discharged Assemblies to Characterize the Effects of Duty
 - C1 Batch N and P (4 total, Assembly Average Burnups [] GWD/MTU)
 - C2 Batch M and N (4 total, Assembly Average Burnups [] GWD/MTU)

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High Duty Fuel Observations

- Oxide [
- No Evidence of [
- More Detailed Examination Required

Expanded Examination Scope

- 2 High Duty and 1 Low Duty Assembly Reconstituted to Allow Single Rod Exams
 - [] Measured to Characterize Oxide Thickness
 - [] Visually Examined to Characterize Appearance
- Visual Examination of [] High Duty Assemblies to Quantify Population of

Cladding Oxide Thickness Determination

- ECT Technique Used to Measure Liftoff From Base Metal
- Measurements Performed on Individual Rods After Removal From Assembly
 - Four Full Length Axial Traces Performed at 90° Azimuthal Orientations
 - Thickness Data for Each Trace Stored Digitally as a Function of Elevation (0.050 Inch Intervals)
- Data Reduction
 - Axial Traces Combined to Generate Composite
 - Maximum Circumferentially Averaged Oxide Thickness Calculated From Digital Composite as Running Average Over 1 Inch Interval (80 Measurements)

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Low Duty Observations

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- Three Cycle Assembly
- [
- Measured Oxide [
- No Blistering/Spalling

High Duty Observations

- Two Cycle Assemblies
- •
- Accuracy of Oxide Predictions Dependent on []
- Blistering/Slight Spalling Observed,

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Blistering/Spalling

Spalling Is a Process That Begins []
[] Progresses To Blistering
Blistering Progresses To "Spallation"

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High Duty Corrosion Results

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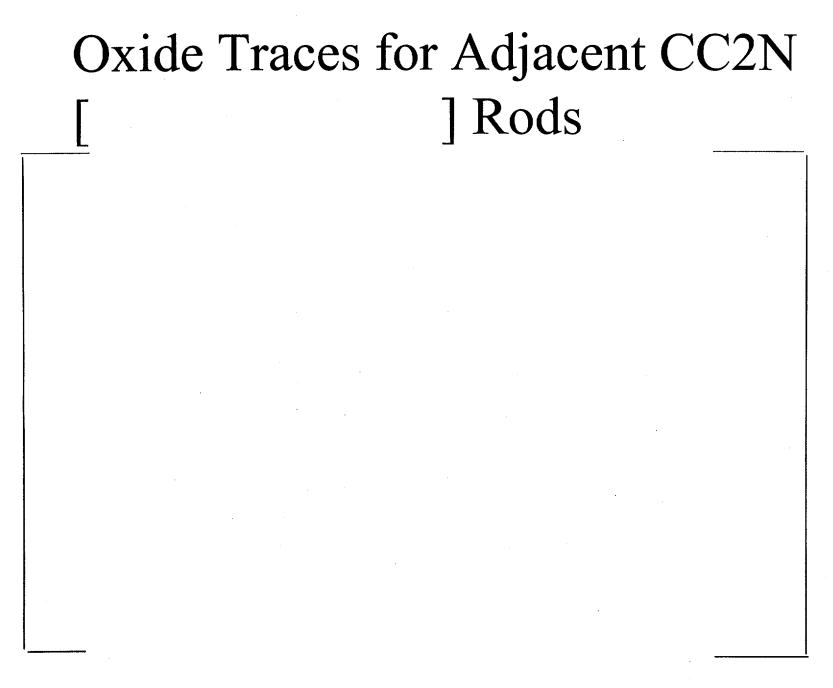


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Calvert Cliffs Fuel Assembly Schematic

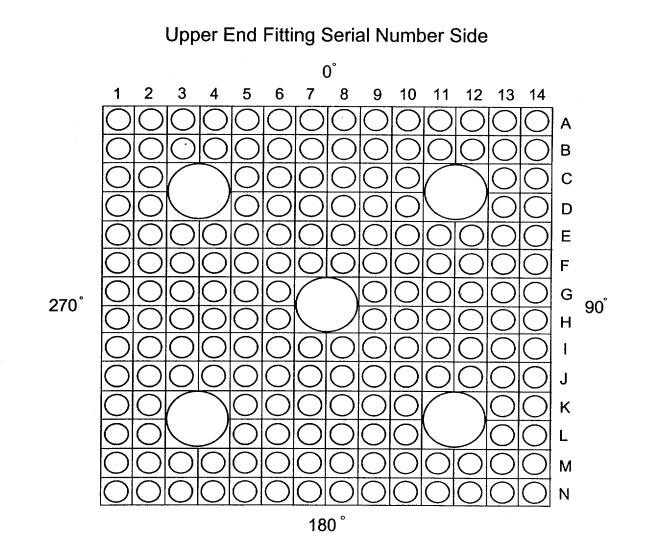
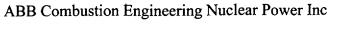


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OPTIN Corrosion Performance in Calvert Cliffs-1 & 2



High Duty Blistering/Spalling

- Blistering/Spalling [
- Behavior Observed on Rods With 57 Microns of Oxide at 51 GWD/MTU

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Calvert Cliffs Fuel Assembly Schematic

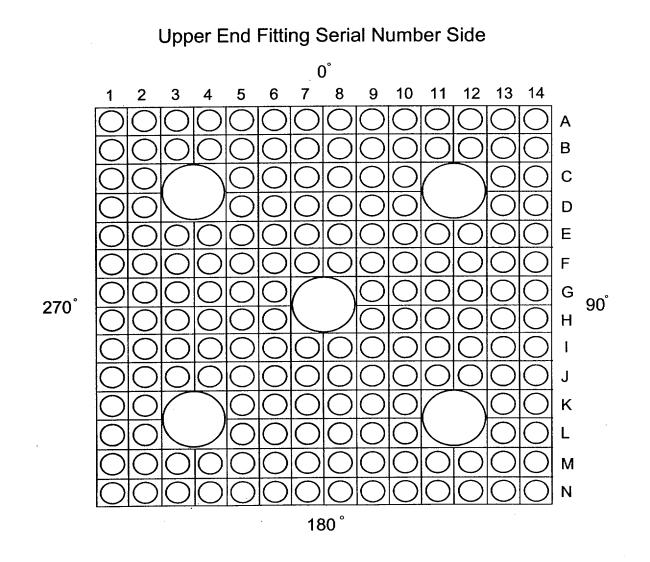


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Observed Blisters on [

] Rods

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Calvert Cliffs Fuel Assembly Schematic

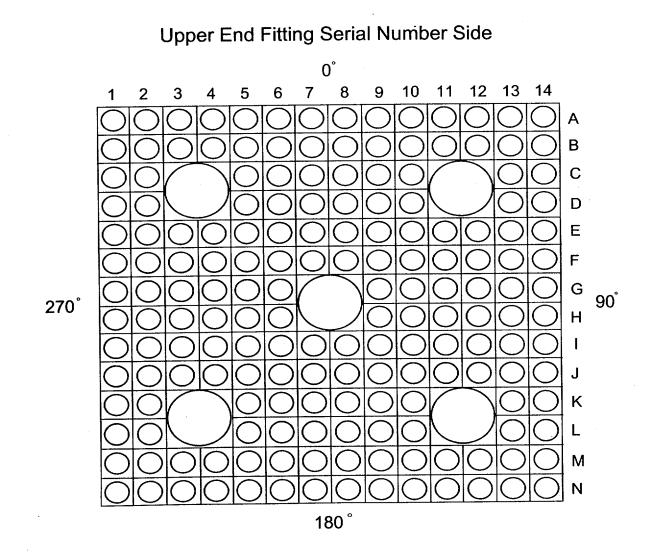


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Fraction of Examined [

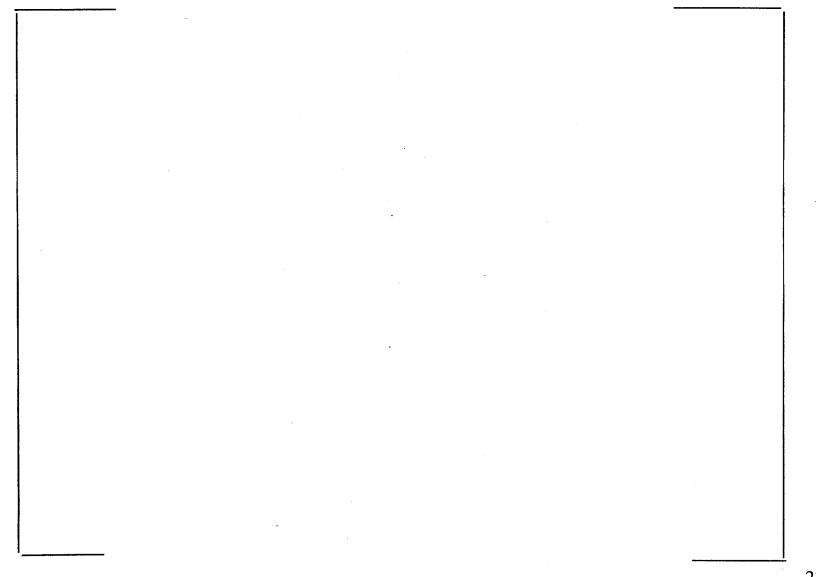


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Corrosion Performance of C2N High Duty Fuel Rods

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Comparison of Measured to Predicted Oxide Using Current Model

Summary Of Observations

- Low Duty Fuel Exhibits Expected Corrosion Behavior
- High Duty Fuel Exhibits Variable Behavior
- Some Populations of Rods Exhibit Higher Than Expected Corrosion and Blistering/ Spalling Behavior

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Outline

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- Describe Inspections and Observations
- Describe Immediate Actions
- Describe Longer Term Actions
- Summarize

Immediate Actions Taken

- Voluntary LER
- Root Cause Evaluation Initiated
- Operability Evaluation Performed to Support Current Cycles of Operation

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Root Cause Conclusions

- Factors Such as [] Not Identified as Primary Contributors
- Factors Affecting Fuel Duty (Time and Cladding Temperature) Are Primary Contributors

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Factors Affecting Fuel Duty

- Improved Operating History
- Reduced RCS Flow Due to Plugged Steam Generator Tubes
- Rod Location Within The Assembly
- Rod Power and Adjacent Rod Power
- Subcooled Boiling
- T-H Effects Due to Geometry
- Others

Operability Evaluation

- No Concern For Normal Operation
- Addressed Accidents and Transients

Operability Evaluation - Accidents and Transients

- Effect of [
- Effect of [
- Effect of [
- Bottom Line Operability Issue [

PROTOTYPE Test Rods

- Test Rods With High Tin Zr-4 Clad/Modified Pellet Designs
 - Irradiated for 5 Cycles, Discharged 1988
- Subset of Rods Examined in Hot Cell (Rod Average Burnups of [] GWD/MTU)

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Mechanical Property Tests Indicate

Photograph not provided in handout

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[] Evaluation for Operability

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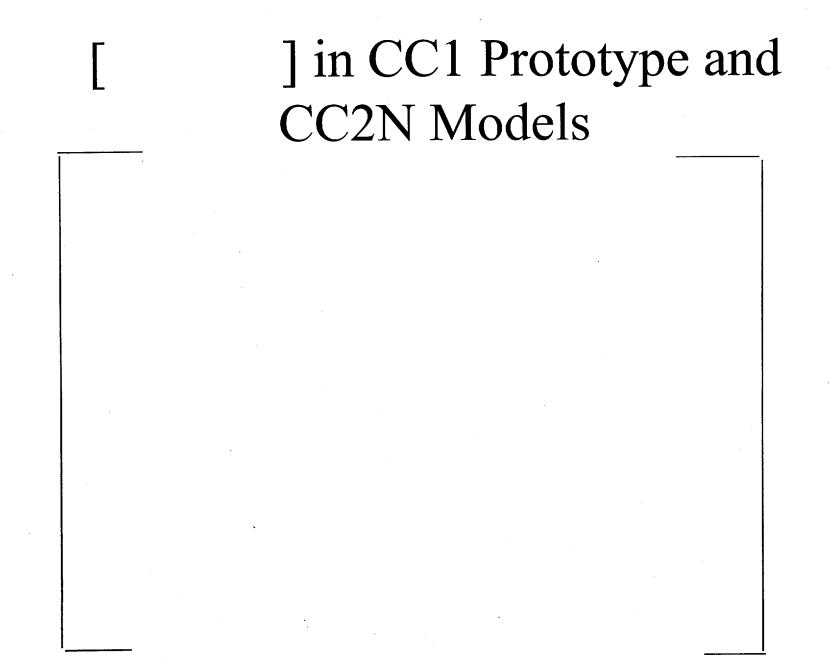
Operability - Accidents and Transients

[] Demand Calculated at [
Even Heavily Spalled Prototype Rod [

• CC2N Rod Capability [

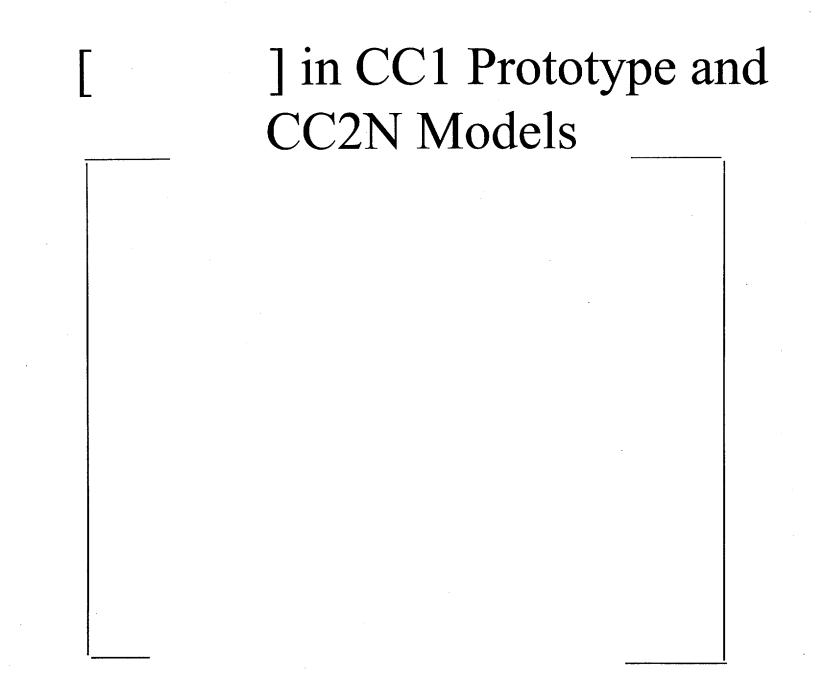
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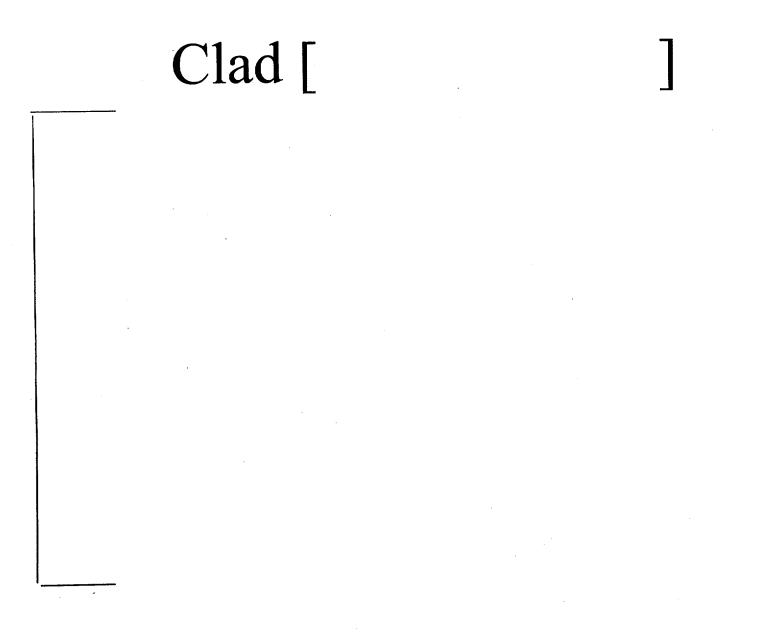
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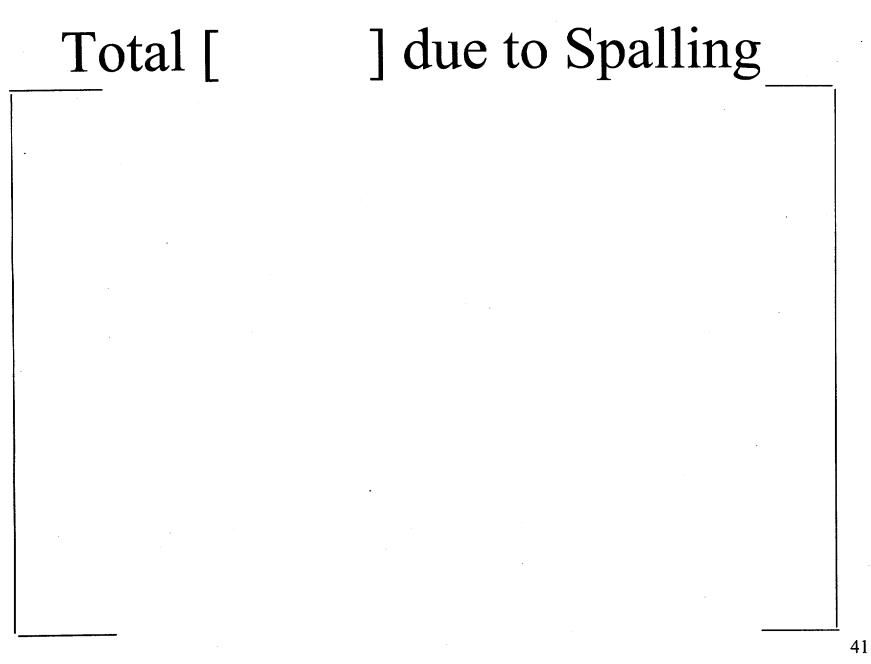


[] for Prototype and CC2N Spalled Rods

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Operability (Continued)

- Current Cycles U1C14 and U2C13
- CC2M Fuel 580/638 EFPD (U2C10/11)
- CC2N Fuel 638/640 EFPD (U2C11/12)
- U1C13/C14 Fuel 590/620 EFPD
- U2C12/C13 Fuel 640/658 EFPD
- Key Parameters [

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Fuel Duty Comparisons

- Fuel Duty Comparisons Were Made Between CC2N and Past & Current Batches
- A Preliminary Fuel Duty Model Was Developed by ABB CENP Which Uses an Improved Corrosion Model
- A Fuel Duty Index Was Evaluated Which is an [Temperature and Time
- Results Show That Fuel Duties are Similar to CC2N for Current Cycles

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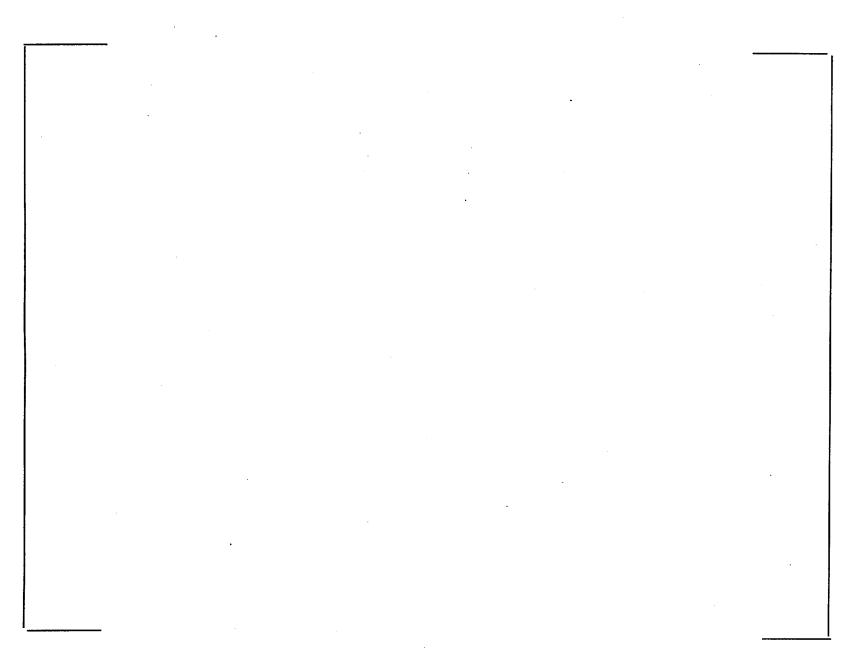
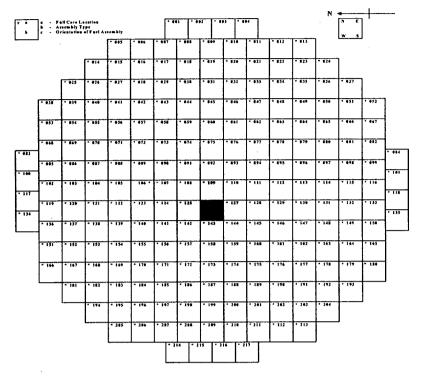


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Fraction of Examined [

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Unit 2 Cycle 12 Core Schematic



High Duty Assembly (Second Cycle of Operation)

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Calvert Cliffs Fuel Assembly Schematic

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Summary of Operability Evaluation

- [] Demand Evaluated
 PROTOTYPE [] Show Heavily
 - Spalled Rod [] Matches Demand
- Current Operating Cores Projected to Have Similar Fuel Duty to CC2N
- Conclusion Current Cores are Operable

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Outline

- Describe Inspections and Observations
- Describe Immediate Actions
- Describe Longer Term Actions
- Summarize

10CFR50.59 Approach for U1C15/U2C14

- Assess Fuel Duty Based on [
- Evaluate Impact of Incremental Increase in Duty on Anticipated Corrosion Behavior Including Blistering/Spalling
- Ensure [
- Acquire Data on CC1R Fuel at EOC14 (Spring 2000) to Further Characterize Phenomenon

Beyond U2C14

• Replacement Steam Generators

- Evaluate TURBO Assembly Design
- Pursue Advanced Cladding Alloy

Summary

- [
- Current Cores Operable
- Subsequent Cores Will Be Handled Under 10CFR50.59
- Longer Term Actions Expected To Mitigate Problem

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Questions

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CIGOO6: PROTOTYPE ROD

Typical Lamination of ZrO₂ Layer

Photo 1

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CIGOOG : PROTOTYPE ROD

Typical Appearance of Region

] Photo 2

Photo 3

ł BE 9NOJ WW 1.5 KOD WIL •

C2N639 ROD M14 91 um

Photo 4

180° FACE, SPANT CaN618 Photo 5