



Tennessee Valley Authority, Post Office Box 2000, Soddy-Daisy, Tennessee 37379

March 3, 2000

U.S. Nuclear Regulatory Commission  
ATTN: Document Control Desk  
Washington, D.C. 20555

Gentlemen:

In the Matter of ) Docket No. 50-327  
Tennessee Valley Authority )

**SEQUOYAH NUCLEAR PLANT (SQN) - UNIT 1 CORE OPERATING LIMITS  
REPORT (COLR)**

In accordance with SQN Unit 1 Technical Specification  
6.9.1.14.c, enclosed is the Unit 1 Cycle 11 COLR.

Please direct questions concerning this issue to me at  
(423) 843-7170 or J. D. Smith at (423) 843-6672.

Sincerely,

Pedro Salas  
Licensing and Industry Affairs Manager

Enclosure  
cc: See page 2

A001

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ENCLOSURE

SEQUOYAH NUCLEAR PLANT UNIT 1 CYCLE 11  
CORE OPERATING LIMITS REPORT  
REVISION 0

**LICENSING TRANSMITTAL TO NRC  
SUMMARY AND CONCURRENCE SHEET**

**THE PURPOSE OF THIS CONCURRENCE SHEET IS TO ASSURE THE ACCURACY AND COMPLETENESS OF TVA SUBMITTALS TO THE NRC.**

DATE _____ DATE DUE NRC <u>04/15/2000 - C</u>			
SUBMITTAL PREPARED BY <u>J. W. Proffitt</u>			
SUBJECT: <u>Sequoyah Nuclear Plant (SQN) - Unit 1 Core Operating Limits Report (COLR)</u>			
PURPOSE/SUMMARY <u>Transmit to NRC the latest COLR revision.</u>			
RESPONDS TO _____		(RIMS NO.) _____	
NEW COMMITMENTS <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO			
INDEPENDENT REVIEW _____		DATE: _____	
LICENSING BASIS CHANGE - If this submittal requires a change to the licensing basis, a change has been initiated in accordance with NADP-7. _____ DATE _____			
A concurrence signature reflects that the signatory has assured that the submittal is appropriate and consistent with TVA Policy, applicable commitments are approved for implementation and supporting documentation for submittal completeness and accuracy has been prepared.			
<b>CONCURRENCE (3)</b>			
<b>NAME</b>	<b>ORGANIZATION</b>	<b>SIGNATURE</b>	<b>DATE</b>
<u>D. L Koehl</u>	<u>SQN Plant Manager</u>	_____	_____
10CFR 50.54(f) oath or affirmation required [ ] Yes [ ] No [ X ] N/A			
<u>J. D. Smith</u>	<u>SQN Licensing Supv.</u>	_____	_____
<u>J. W. Proffitt</u>	<u>SQN Lic &amp; IA</u>	_____	_____

I: license / worddoc / Unit 1 Cycle 11 COLR  
JWP:PMB

L 36 000217 800

COLR FOR SEQUOYAH UNIT 1 CYCLE 11

QA RECORD

SEQUOYAH NUCLEAR PLANT UNIT 1, CYCLE 11

REVISION 0

February 2000

Prepared:

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Nuclear Fuel / Date

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Derry Blair / 2-22-2000  
Reactor Engineering Supervisor / Date

A. Butterworth / 2-22-2000  
Operations Manager / Date

A. Butterworth / 2-24-2000  
PORC Chairman / Date

Revision 0

Pages affected \_\_\_\_\_

Reason for Revision \_\_\_\_\_

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

## COLR FOR SEQUOYAH UNIT 1 CYCLE 11

### 1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Sequoyah Unit 1 Cycle 11 has been prepared in accordance with the requirements of Technical Specification (TS) 6.9.1.14.

The TSs affected by this report are listed below:

TABLE 2.2-1  $f_1$  ( $\Delta I$ ) trip reset function for OT $\Delta$ T Trip (QTNL, QTPL) and rates of trip setpoint decrease per percent  $\Delta I$  (QTNS, QTPS)

TABLE 2.2-1  $f_2$  ( $\Delta I$ ) trip reset function for OP $\Delta$ T Trip (QPNL, QPPL) and rates of trip setpoint decrease per percent  $\Delta I$  (QPNS, QPPS)

3/4.1.1.3 Moderator Temperature Coefficient (MTC)

3/4.1.3.5 Shutdown Rod Insertion Limit

3/4.1.3.6 Control Rod Insertion Limits

3/4.2.1 Axial Flux Difference (AFD)

3/4.2.2 Heat Flux Hot Channel Factor ( $F_Q$  (X,Y,Z))

3/4.2.3 Nuclear Enthalpy Rise Hot Channel Factor ( $F_{\Delta H}$  (X,Y))

### 2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in section 1.0 are presented in the following subsections. These limits have been developed using the NRC approved methodologies specified in TS 6.9.1.14.

The following abbreviations are used in this section:

BOL stands for Beginning of Cycle Life  
ARO stands for All Rods Out  
HZP stands for Hot Zero THERMAL POWER  
EOL stands for End of Cycle Life  
RTP stands for RATED THERMAL POWER

#### 2.1 Moderator Temperature Coefficient - MTC (Specification 3/4.1.1.3)

2.1.1 The MTC limits are:

The BOL/ARO/HZP-MTC shall be less positive than 0  $\Delta k/k/^\circ F$  (BOL limit). With the measured BOL/ARO/HZP-MTC more positive than 0  $\Delta k/k/^\circ F$  (as-measured MTC limit), establish control rod withdrawal limits to ensure the MTC remains less positive than 0  $\Delta k/k/^\circ F$  for all times in core life.

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The EOL/ARO/RTP-MTC shall be less negative than or equal to  $-4.5 \times 10^{-4} \Delta k/k/^\circ F$ .

2.1.2 The 300 ppm surveillance limit is:

The measured 300 ppm/ARO/RTP-MTC should be less negative than or equal to  $-3.75 \times 10^{-4} \Delta k/k/^\circ F$ .

2.2 Shutdown Rod Insertion Limit (Specification 3/4.1.3.5)

2.2.1 The shutdown rods shall be withdrawn to a position as defined below:

<u>Cycle Burnup (MWD/MTU)</u>	<u>Steps Withdrawn</u>
$\leq 4,000$	$\geq 225$ to $\leq 231$
$> 4,000$ to $< 14,000$	$\geq 222$ to $\leq 231$
$\geq 14,000$	$\geq 225$ to $\leq 231$

2.3 Control Rod Insertion Limits (Specification 3/4.1.3.6)

2.3.1 The control rod banks shall be limited in physical insertion as shown in Figure 1.

2.4 Axial Flux Difference - AFD (Specification 3/4.2.1)

2.4.1 The axial flux difference (AFD) limits ( $AFD^{Limit}$ ) are provided in Figure 2.

2.5 Heat Flux Hot Channel Factor -  $F_Q(X,Y,Z)$  (Specification 3/4.2.2)

$F_Q(X,Y,Z)$  shall be limited by the following relationships:

$$F_Q(X,Y,Z) \leq \frac{F_Q^{RTP}}{P} * K(Z) \quad \text{for } P > 0.5$$

$$F_Q(X,Y,Z) \leq \frac{F_Q^{RTP}}{0.5} * K(Z) \quad \text{for } P \leq 0.5$$

$$\text{where } P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$$

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2.5.1  $F_Q^{RTP} = 2.50$

2.5.2  $K(Z)$  is provided in Figure 3

The following parameters are required for core monitoring per the Surveillance Requirements of Specification 3/4.2.2:

2.5.3  $NSLOPE^{AFD} = 1.15$

where  $NSLOPE^{AFD}$  = Negative AFD limit adjustment required to compensate for each 1% that  $F_Q(X,Y,Z)$  exceeds BQDES.

2.5.4  $PSLOPE^{AFD} = 1.08$

where  $PSLOPE^{AFD}$  = Positive AFD limit adjustment required to compensate for each 1% that  $F_Q(X,Y,Z)$  exceeds BQDES.

2.5.5  $NSLOPE^{f_2(\Delta I)} = 1.40$

where  $NSLOPE^{f_2(\Delta I)}$  Adjustment to negative OPΔT  $f_2(\Delta I)$  limit required to compensate for each 1% that  $F_Q(X,Y,Z)$  exceeds BCDES.

2.5.6  $PSLOPE^{f_2(\Delta I)} = 1.63$

where  $PSLOPE^{f_2(\Delta I)}$  Adjustment to positive OPΔT  $f_2(\Delta I)$  limit required to compensate for each 1% that  $F_Q(X,Y,Z)$  exceeds BCDES.

2.5.7  $BQNOM(X,Y,Z) =$  Nominal design peaking factor, increased by an allowance for the expected deviation between the nominal design power distribution and the measurement.

2.5.8  $BQDES(X,Y,Z) =$  Maximum allowable design peaking factor which ensures that the  $F_Q(X,Y,Z)$  limit will be preserved for operation within the LCO limits, including allowances for calculational and measurement uncertainties.

2.5.9  $BCDES(X,Y,Z) =$  Maximum allowable design peaking factor which ensures that the centerline fuel melt limit will be preserved for operation within the LCO limits, including allowances for calculational and measurement uncertainties.

$BQNOM(X,Y,Z)$ ,  $BQDES(X,Y,Z)$ , and  $BCDES(X,Y,Z)$  data bases are provided for input to the plant power distribution analysis codes on a cycle specific basis and are determined using the methodology for core limit generation described in the references in Specification 6.9.1.14.



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2.5.10 The increase in  $F_Q^M(X, Y, Z)$  for compliance with the 4.2.2.2.e Surveillance Requirements is defined as follows:

For cycle burnups $\leq 7128$ MWd/MTU	2.0%
For cycle burnups $> 7128$ MWd/MTU to $\leq 7774$ MWd/MTU	3.0%
For cycle burnups $> 7774$ MWd/MTU to $\leq 9171$ MWd/MTU	4.0%
For cycle burnups $> 9171$ MWd/MTU to $\leq 9494$ MWd/MTU	3.0%
For cycle burnups $> 9494$ MWd/MTU	2.0%

2.6 Nuclear Enthalpy Rise Hot Channel Factor -  $F_{\Delta H}(X, Y)$  (Specification 3/4.2.3)

$F_{\Delta H}(X, Y)$  shall be limited by the following relationship:

$$F_{\Delta H}(X, Y) \leq \text{MAP}(X, Y, Z) / \text{AXIAL}(X, Y)$$

2.6.1  $\text{MAP}(X, Y, Z)$  is provided in Table 1.

$\text{AXIAL}(X, Y)$  is the axial peak from the normalized axial power shape.

The following parameters are required for core monitoring per the Surveillance Requirements of Specification 3/4.2.3:

$$F_{\Delta HR}^M(X, Y) \leq \text{BHNOM}(X, Y)$$

$$\text{where } F_{\Delta HR}^M(X, Y) = F_{\Delta H}(X, Y) / \text{MAP}^M / \text{AXIAL}(X, Y)$$

$F_{\Delta H}(X, Y)$  is the measured radial peak at location X, Y.

$\text{MAP}^M$  is the value of  $\text{MAP}(X, Y, Z)$  obtained from Table 1 for the measured peak.

2.6.2  $\text{BHNOM}(X, Y) =$  nominal design radial peaking factor, increased by an allowance for the expected deviation between the nominal design power distribution and the measurement.

2.6.3  $\text{BHDES}(X, Y) =$  maximum allowable design radial peaking factor which ensures that the  $F_{\Delta H}(X, Y)$  limit will be preserved for operation within the LCO limits, including allowances for calculational and measurement uncertainties.

2.6.4  $\text{BRDES}(X, Y) =$  maximum allowable design radial peaking factor which ensures that the steady state DNBR limit will be preserved for operation within the LCO limits, including allowances for calculational and measurement uncertainties.

$\text{BHNOM}(X, Y)$ ,  $\text{BHDES}(X, Y)$  and  $\text{BRDES}(X, Y)$  data bases are provided for input to the plant power distribution analysis computer codes on a cycle specific basis and are determined using the methodology for core limit generation described in the references in Specification 6.9.1.14.

2.6.5  $\text{RRH} = 3.34$  when  $0.8 < P \leq 1.0$

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$$RRH = 1.67 \text{ when } P \leq 0.8$$

where RRH = Thermal power reduction required to compensate for each 1% that  $F_{\Delta H}(X,Y)$  exceeds its limit.

$$P = \text{Thermal Power} / \text{Rated Thermal Power}$$

$$2.6.6 \quad TRH = 0.0334 \text{ when } 0.8 < P \leq 1.0$$

$$TRH = 0.0167 \text{ when } P \leq 0.8$$

where TRH = Reduction in  $OT\Delta T K_1$  setpoint required to compensate for each 1%  $F_{\Delta H}(X,Y)$  exceeds its limit.

2.6.7 All cycle burnups shall use a 2% increase in  $F_{\Delta H}^M(X,Y)$  margin for compliance with the 4.2.3.2.d.1 Surveillance Requirement.

### 3.0 REACTOR CORE PROTECTIVE LIMITS

#### 3.1 Trip Reset Term [ $f_1(\Delta I)$ ] for Overtemperature Delta T-Trip (Specification 2.2.1)

The following parameters are required to specify the power level-dependent  $f_1(\Delta I)$  trip reset term limits for the Overtemperature Delta-T trip function:

$$3.1.1 \quad QTNL = -20\%$$

where QTNL = the maximum negative  $\Delta I$  setpoint at rated thermal power at which the trip setpoint is not reduced by the axial power distribution.

$$3.1.2 \quad QTPL = +5\%$$

where QTPL = the maximum positive  $\Delta I$  setpoint at rated thermal power at which the trip setpoint is not reduced by the axial power distribution.

$$3.1.3 \quad QTNS = 2.50\%$$

where QTNS = the percent reduction in Overtemperature Delta-T trip setpoint for each percent that the magnitude of  $\Delta I$  exceeds its negative limit at rated thermal power (QTNL).

$$3.1.4 \quad QTPS = 1.40\%$$

where QTPS = the percent reduction in Overtemperature Delta-T trip setpoint for each percent that the magnitude of  $\Delta I$  exceeds its positive limit at rated thermal power (QTPL).

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### 3.2 Trip Reset Term [ $f_2(\Delta I)$ ] for Overpower Delta-T Trip (Specification 2.2.1)

The following parameters are required to specify the power level-dependent  $f_2(\Delta I)$  trip reset term limits for the Overpower Delta-T trip function:

#### 3.2.1 QPNL = -25%

where QPNL = the maximum negative  $\Delta I$  setpoint at rated thermal power at which the trip setpoint is not reduced by the axial power distribution.

#### 3.2.2 QPPL = +25%

where QPPL = the maximum positive  $\Delta I$  setpoint at rated thermal power at which the trip setpoint is not reduced by the axial power distribution.

#### 3.2.3 QPNS = 1.70%

where QPNS = the percent reduction in Overpower Delta-T trip setpoint for each percent that the magnitude of  $\Delta I$  exceeds its negative limit at rated thermal power (QPNL).

#### 3.2.4 QPPS = 1.70%

where QPPS = the percent reduction in Overpower Delta T trip setpoint for each percent that the magnitude of  $\Delta I$  exceeds its positive limit at rated thermal power (QPPL).

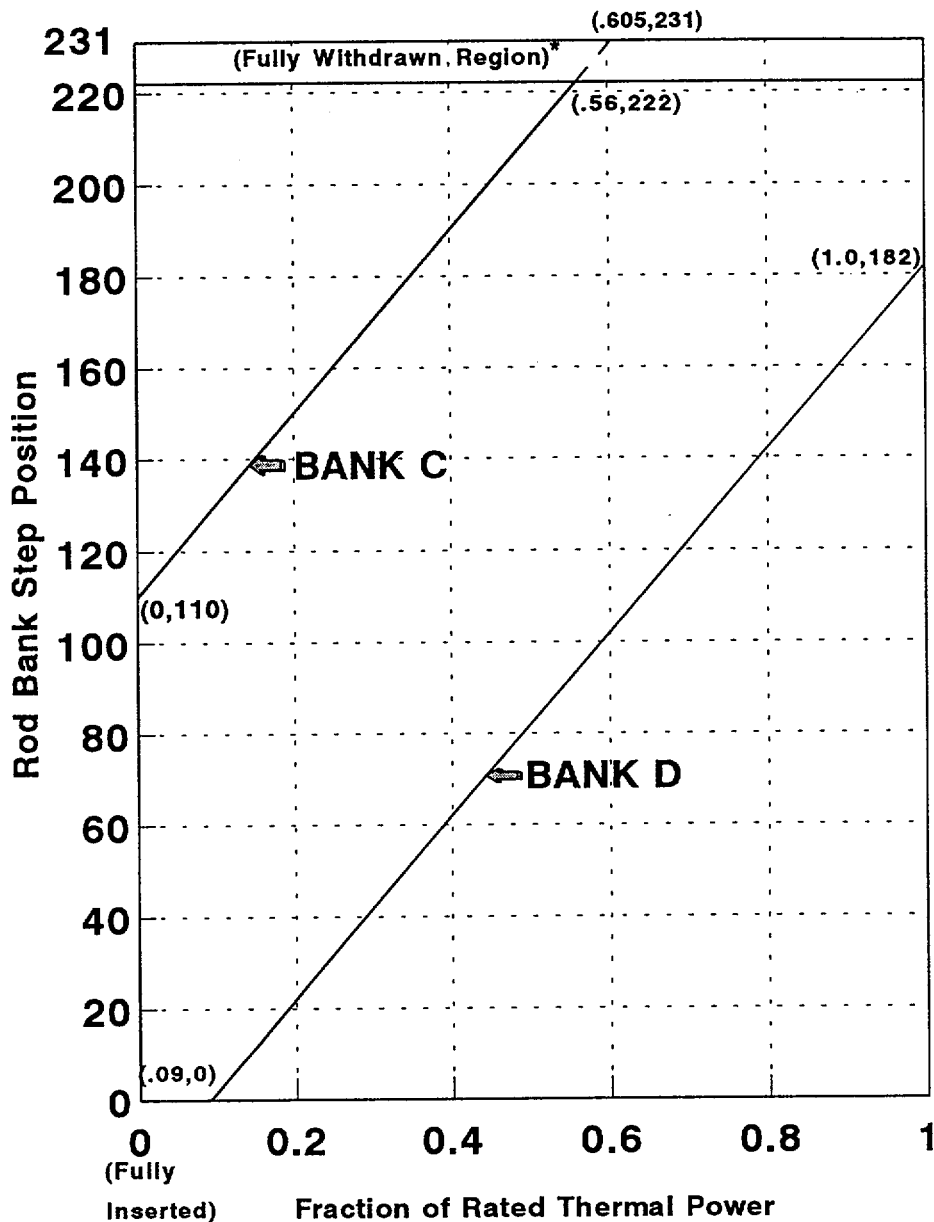
**COLR FOR SEQUOYAH UNIT 1 CYCLE 11**

**Table 1**

**Maximum Allowable Peaking Limits MAP(X,Y,Z)**

<u>Elevation (ft)</u>	<u>AXIAL (X,Y)</u>	<u>MAP (X,Y,Z)</u>
2	1.1	1.970
4		1.966
6		1.958
8		1.945
10		1.917
2	1.2	2.208
4		2.197
6		2.180
8		2.150
10		2.072
2	1.3	2.453
4		2.434
6		2.406
8		2.315
10		2.185
2	1.4	2.702
4		2.672
6		2.572
8		2.429
10		2.288
2	1.5	2.956
4		2.826
6		2.683
8		2.529
10		2.381
2	1.7	3.162
4		3.007
6		2.850
8		2.690
10		2.542
2	1.9	3.283
4		3.133
6		2.982
8		2.821
10		2.685

# COLR For Sequoyah Unit 1 Cycle 11



## FIGURE 1

**Rod Bank Insertion Limits Versus Thermal Power Four Loop Operation**

\* Fully withdrawn region shall be the condition where shutdown and control banks are at a position within the interval of  $\geq 222$  and  $\leq 231$  steps withdrawn, inclusive.

Fully withdrawn shall be the position as defined below,

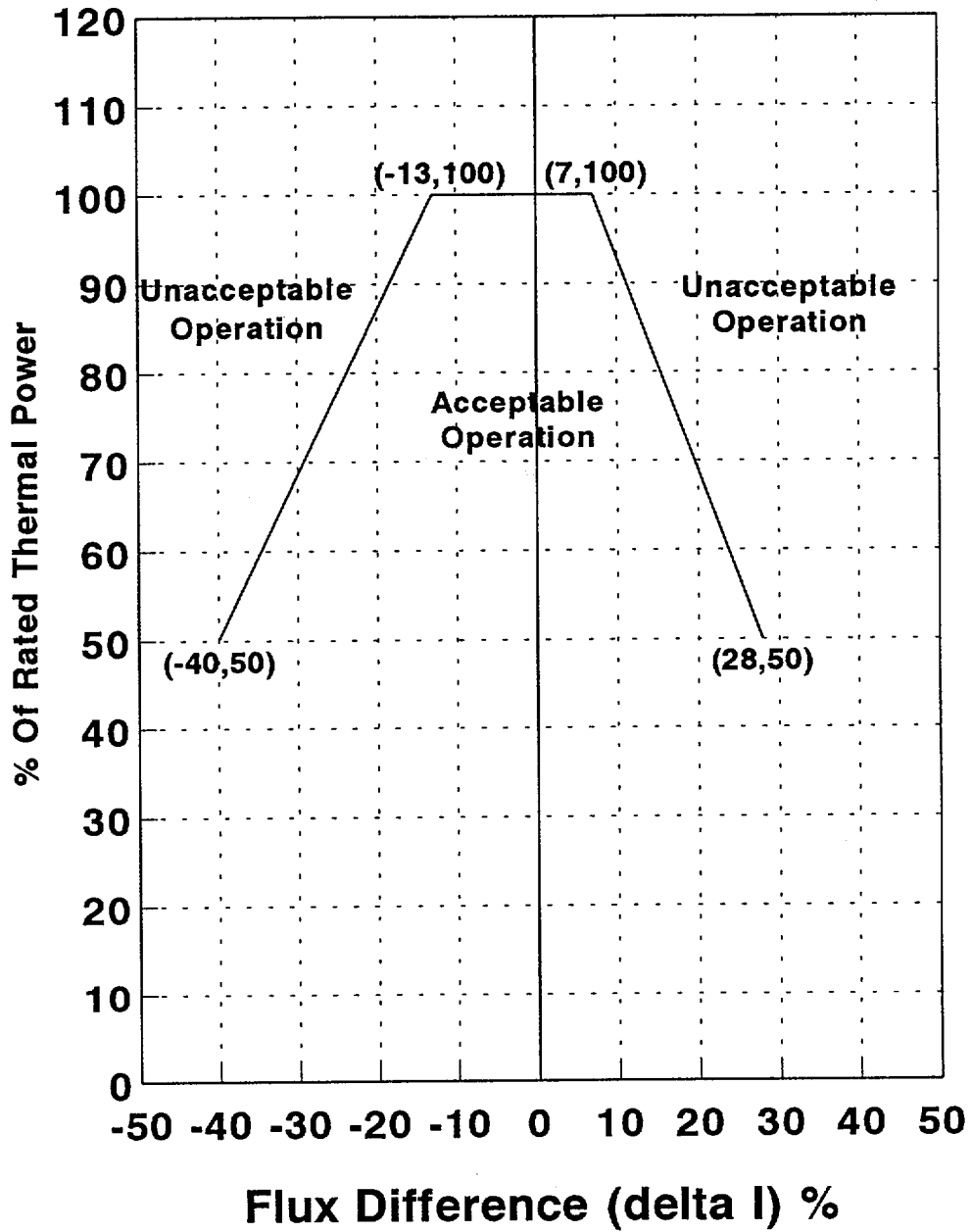
Cycle Burnup (MWd/MTU)

$\leq 4000$   
 $> 4000$  to  $< 14,000$   
 $\geq 14,000$

Step Withdrawn

$\geq 225$  to  $\leq 231$   
 $\geq 222$  to  $\leq 231$   
 $\geq 225$  to  $\leq 231$

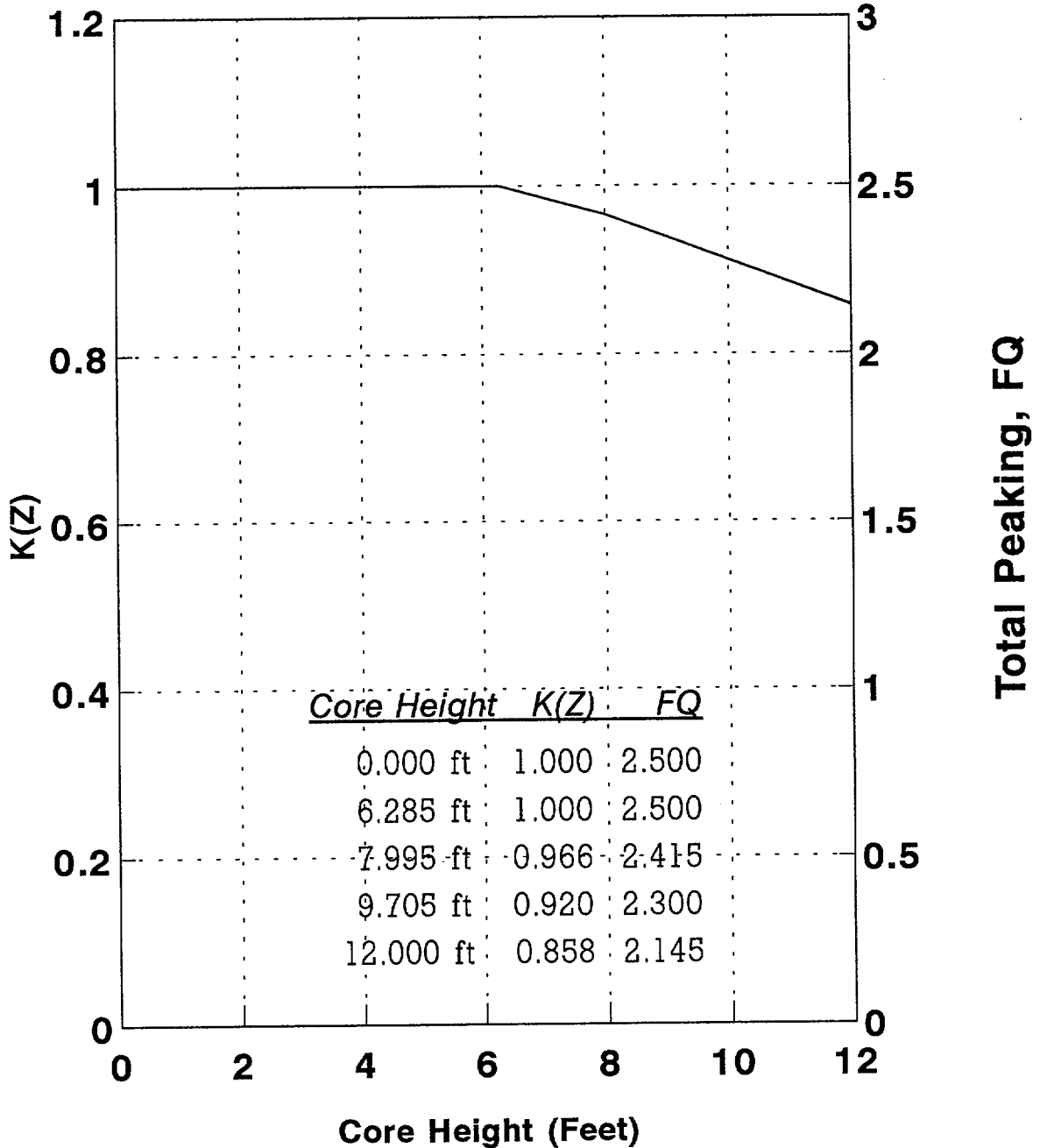
# COLR For Sequoyah Unit 1 Cycle 11



## FIGURE 2

**Axial Flux Difference Limits As  
A Function Of Rated Thermal Power**

# COLR For Sequoyah Unit 1 Cycle 11



**FIGURE 3**

K(Z) - Normalized FQ(X,Y,Z) as a Function of Core Height