



UNITED STATES
NUCLEAR REGULATORY COMMISSION

WASHINGTON, D.C. 20555-0001

February 15, 2000

Temp = NRR-11
Document
needs to be
Scanned into
Adams
File Center

LICENSEE: Energy Northwest

FACILITY: WNP-2

SUBJECT: SUMMARY OF MEETING WITH ENERGY NORTHWEST REGARDING THE
PROPOSED SECONDARY CONTAINMENT/STANDBY GAS TREATMENT
SUBMITTAL

On January 27, 2000, the Nuclear Regulatory Commission (NRC) staff met with representatives of Energy Northwest to discuss the upcoming secondary containment/standby gas treatment license amendment submittal. The proposed changes would revise the following:

- SR 3.6.1.3.10 increases the secondary containment bypass leakage from .74 standard cubic feet per hour (scfh) to .028 percent/day approximately 9.4 scfh.
- SR 3.6.4.1.1 change the requirement to verify secondary containment pressure is less than .25 inch vacuum water gage to less than 0 inch vacuum water gage.
- SR 3.6.4.1.4 increase the secondary containment drawdown time from 2 minutes to 20 minutes.
- TS 5.5.7 increase the standby gas treatment system flow rate to 5000 cubic feet per minute (cfm).

Energy Northwest withdrew a similar amendment request in July 1999, when the staff identified a calculation error in determining containment release concentration. Due to the extensive review required of the previous submittal, both the staff and the licensee felt that a meeting to discuss the upcoming submittal would be beneficial in shortening the review and avoiding unnecessary requests for additional information.

In order to improve efficiency the same NRC staff members who were involved in the final review for the first submittal were at the meeting and will review the second submittal. Enclosure 1 is a list of the meeting participants. Enclosure 2 is a copy of the slides presented by Energy Northwest.

At the outset of the meeting, Mr. John Arbuckle of Energy Northwest presented an overview of the submittal. The emphasis was on how this submittal has changed from the previous submittal. This submittal includes meteorological data and atmospheric dispersion calculations (X/Q calculations). Leta Brown, of the NRC staff, suggested that it would be useful if the X/Q calculations and an electronic version of the meteorological data were provided for staff review.

Mr. David Studley of Scientech discussed the X/Q calculations including the four release points and the control room intakes. The discussion also covered the application of ARCON 96 Code and the assumptions that were made. The description of the site configuration and of the

000-37

NRC FILE CENTER COPY

control room intakes were useful to the staff in understanding the assumptions that were made. The staff expressed a concern with the vent option used in the ARCON 96 Code that was used to calculate some of the control room atmospheric dispersion factors. It was suggested that an acceptable solution would be to recalculate the vent run cases as a ground release option using ARCON 96.

Mr. Bruce Boyum of Energy Northwest discussed the accidents that were analyzed specifically, main steam line break accident, fuel handling accident, control rod drop accident and loss-of-coolant accident (LOCA). Mr. Boyum stated that the LOCA was the bounding accident. Mr. Mark Blumberg, of the NRC staff, stated that it would be useful to include the calculations for the LOCA analysis and include sufficient information on other accidents so that it can be determined that the LOCA is the bounding accident.

Mr. Studley described the Axident Code, which is the dose analysis code used in the submittal. The Axident Code models the transport of radioactivity to the environment and to the control room. The major assumptions and the reasons for them were discussed.

Mr. Boyum also discussed the release pathways including the use of the Gothic Code to justify the 40 percent mixing assumed in secondary containment. Mr. Richard Lobel, of the NRC staff, said the proposed submittal should include a description of the derivation and use of the flow equation which is the basis for Figure 4 of Attachment 2 to the licensee's October 15, 1996, submittal. In addition, the staff may request input used in reactor building pressure drawdown calculations so that the staff may perform independent calculations. A final decision has not been made.

Mr. Boyum then discussed control room air flows and unfiltered control room in-leakage. Mr. Blumberg stated that licensees have had to verify their unfiltered in-leakage assumptions. The ASTM E741, "Standard Test Methods for Determining Air Change in a Single Zone by Means of a Tracer Gas Dilution," test method is acceptable to the staff as a verification test for unfiltered in-leakage. The licensee could describe their design and propose an alternative test method that would have to be reviewed and approved by the staff.

The NRC staff felt that Energy Northwest did a good job explaining their submittal and that they were receptive to suggestions from the staff.

Jack Cushing, Project Manager, Section 2
Project Directorate IV & Decommissioning
Division of Licensing Project Management
Office of Nuclear Reactor Regulation

DISTRIBUTION:

Docket No. 50-397

Enclosures: 1. List of Meeting Participants
2. Energy Northwest Slides

cc w/encls: See next page

Hard Copy
Central File
PUBLIC
PDIV-2 R/F
JCushing
OGC
ACRS

E-Mail
JZwolinski/SBlack
SRichards
DLange, EDO
EPeyton
RLobel
MBlumberg
LBrown
LSmith, RIV

DOCUMENT NAME: G:\PDIV-2\WNP2\MTS12700.wpd

| To receive a copy of this document, indicate "C" in the box | | | | | |
|---|-------------------|---|--------------------|---|-------------------|
| OFFICE | PDIV-2/PM | C | PDIV-2/LA | C | PDIV-2/SC |
| NAME | JCushing:lcc | | EPeyton <i>esp</i> | | SDembek <i>SD</i> |
| DATE | <i>je 2/14/00</i> | | <i>2/14/00</i> | | <i>2/14/00</i> |

OFFICIAL RECORD COPY

*Temp = NRR-111
Needs to be
Scanned into
Calendar*

control room intakes were useful to the staff in understanding the assumptions that were made. The staff expressed a concern with the vent option used in the ARCON 96 Code that was used to calculate some of the control room atmospheric dispersion factors. It was suggested that an acceptable solution would be to recalculate the vent run cases as a ground release option using ARCON 96.

Mr. Bruce Boyum of Energy Northwest discussed the accidents that were analyzed specifically, main steam line break accident, fuel handling accident, control rod drop accident and loss-of-coolant accident (LOCA). Mr. Boyum stated that the LOCA was the bounding accident. Mr. Mark Blumberg, of the NRC staff, stated that it would be useful to include the calculations for the LOCA analysis and include sufficient information on other accidents so that it can be determined that the LOCA is the bounding accident.

Mr. Studley described the Axident Code, which is the dose analysis code used in the submittal. The Axident Code models the transport of radioactivity to the environment and to the control room. The major assumptions and the reasons for them were discussed.

Mr. Boyum also discussed the release pathways including the use of the Gothic Code to justify the 40 percent mixing assumed in secondary containment. Mr. Richard Lobel, of the NRC staff, said the proposed submittal should include a description of the derivation and use of the flow equation which is the basis for Figure 4 of Attachment 2 to the licensee's October 15, 1996, submittal. In addition, the staff may request input used in reactor building pressure drawdown calculations so that the staff may perform independent calculations. A final decision has not been made.

Mr. Boyum then discussed control room air flows and unfiltered control room in-leakage. Mr. Blumberg stated that licensees have had to verify their unfiltered in-leakage assumptions. The ASTM E741, "Standard Test Methods for Determining Air Change in a Single Zone by Means of a Tracer Gas Dilution," test method is acceptable to the staff as a verification test for unfiltered in-leakage. The licensee could describe their design and propose an alternative test method that would have to be reviewed and approved by the staff.

The NRC staff felt that Energy Northwest did a good job explaining their submittal and that they were receptive to suggestions from the staff.



Jack Cushing, Project Manager, Section 2
Project Directorate IV & Decommissioning
Division of Licensing Project Management
Office of Nuclear Reactor Regulation

Docket No. 50-397

Enclosures: 1. List of Meeting Participants
2. Licensee's Slides

cc w/encls: See next page

WNP-2

cc:

Mr. Greg O. Smith (Mail Drop 927M)
Vice President, Generation
Energy Northwest
P. O. Box 968
Richland, Washington 99352-0968

Mr. Albert E. Mouncer (Mail Drop 1396)
Chief Counsel
Energy Northwest
P.O. Box 968
Richland, Washington 99352-0968

Ms. Deborah J. Ross, Chairman
Energy Facility Site Evaluation Council
P. O. Box 43172
Olympia, Washington 98504-3172

Mr. D. W. Coleman (Mail Drop PE20)
Manager, Regulatory Affairs
Energy Northwest
P.O. Box 968
Richland, Washington 99352-0968

Mr. Paul Inserra (Mail Drop PE20)
Manager, Licensing
Energy Northwest
P.O. Box 968
Richland, Washington 99352-0968

Regional Administrator, Region IV
U.S. Nuclear Regulatory Commission
Harris Tower & Pavilion
611 Ryan Plaza Drive, Suite 400
Arlington, Texas 76011-8064

Chairman
Benton County Board of Commissioners
P.O. Box 69
Prosser, Washington 99350-0190

Senior Resident Inspector
U.S. Nuclear Regulatory Commission
P.O. Box 69
Richland, Washington 99352-0069

Mr. Rodney L. Webring (Mail Drop PE08)
Vice President, Operations Support/PIO
Energy Northwest
P. O. Box 968
Richland, Washington 99352-0968

Thomas C. Poindexter, Esq.
Winston & Strawn
1400 L Street, N.W.
Washington, DC 20005-3502

Mr. Bob Nichols
Executive Policy Division
Office of the Governor
P.O. Box 43113
Olympia, Washington 98504-3113

Mr. J. V. Parrish
Chief Executive Officer
Energy Northwest
P.O. Box 968 (Mail Drop 1023)
Richland, WA 99352-0968

ENERGY NORTHWEST

MEETING PARTICIPANTS

JANUARY 27, 2000

ENERGY NORTHWEST

Douglas Coleman
Bruce Boyum
John Bekahazi
Linda Woolsley
John Arbuckle

SCIENTECH-NUS

David Studley

NRC

Jack Cushing
Steve Dembek
Mark Blumberg
Richard Lobel
Leta Brown

ENERGY NORTHWEST
Secondary Containment/SGT Submittal Presentation

Introduction

(John Arbuckle)

Meteorological Data And X/Q Calculations

(John Arbuckle and Dave Studley)

Dose Analysis And Results

(Bruce Boyum and Dave Studley)

Summary

(Bruce Boyum)

INTRODUCTION

- Initial Problem
- Submittal History
- Analysis Problem/TS Retraction/JCO-FAO Impact
- Comparison of Key SGT Parameters
- Technical Specification Changes
- Submittal Content

INITIAL PROBLEM

- Under Certain Post-Accident Meteorological Conditions, WNP-2 could not Develop 0.25-inch Negative Differential Pressure Within 120 Seconds
- Therefore, a Revised Design Basis and Dose Analysis was Provided. JCO (FAO) Prepared and Submitted to Staff.

SUBMITTAL HISTORY

- October 1996
Technical Specification Amendment Request

- December 1997 – June 1999
Formally Responded to Three RAIs

ANALYSIS PROBLEM

Analysis Problem/TS Retraction/JCO-FAO Impact

July 1999

Withdrew Technical Amendment Request – Discovery of a Nonconservative Error in Determining Containment Release Concentration During Resolution of Proposed RAI 4

No Impact on JCO-FAO, Current Design Basis, Technical Specifications or Recent Analyses

COMPARISON OF KEY SGT PARAMETERS

| <u>Key Parameter</u> | <u>Original Design</u> | <u>Current Design (JCO-FAO)</u> | <u>Proposed Design</u> |
|----------------------|----------------------------|-------------------------------------|----------------------------|
| Drawdown Time | 2 minutes | 10 minutes | 20 minutes |
| SC Leakage | 2240 cfm | 1475 cfm | 2240 cfm |
| SGT Flow | 4457 cfm | 5385 – 5850 cfm | 5000 cfm |

TECHNICAL SPECIFICATIONS

- Proposed Technical Specification Changes

- SR 3.6.1.3.10 Increase Secondary Containment Bypass Leakage from 0.74 scfh to (0.028%/day) *Consistent with 11/12/10*
(9.4 scfh)
- SR 3.6.4.1.1 Change the Surveillance Requirement to Verify Every 24 Hours that the Pressure Within Secondary Containment is <0 inch (vs 0.25 inch) *(Consistent with 11/12/10)*
of Vacuum Water Gauge
- SR 3.6.4.1.4 Increase Secondary Containment Drawdown Time from 120 seconds to 20 minutes
- 5.5.7.2.A Increase Standby Gas Treatment System Flow Rate from 4457 cfm to 5000 cfm

SUBMITTAL CONTENT

- Detailed History - Supersedes Previous Submittals
- Responses to RAIs Incorporated
- Design Basis Meteorology and X/Q Values *including technical input maps*
- Accidents Analyzed - LOCA in Detail, FHA, MSLB and CRDA
- GOTHIC Model and Benchmarking Efforts
- Discussion of Standby Gas Treatment System
- Evaluation of Significant Hazards
- Environmental Considerations Evaluation
- Marked-Up and Typed Technical Specifications
- Marked-Up Technical Specification Bases - For Info Only

METEOROLOGICAL DATA AND X/Q CALCULATIONS

- Description of Met Tower, Terrain, and Instrumentation
- Data Used (6yrs)
- ARCON96
 1. Description of Release Points and Control Room Intakes
 2. Application of ARCON96 at WNP-2
 3. Comparison With JCO-FAO and Power Uprate

DESCRIPTION OF MET TOWER, TERRAIN, AND INSTRUMENTATION

- Meteorological Tower Consists of a 240-ft Structure with a 5-ft Extension Mast
- The Tower is Triangular in Shape and of Open Lattice Construction to Minimize Tower Interference with Meteorological Measurements
- Wind Speed and Direction is Monitored by Separate Channels at the 33-ft and 245-ft Elevations
- A Single Channel Provides Air Temperature Difference Between 33-ft and 245-ft Elevations

DESCRIPTION OF MET TOWER, TERRAIN, AND INSTRUMENTATION

- Siting of Instrumentation with Respect to Meteorological Tower and Surrounding Vegetation is Very Good
- The Base of the Tower Maintained as Natural Vegetation
- Area Around the Tower is Open Terrain with no Natural or Man-Made Obstructions to Impact Data Being Collected

DATA USED (6YRS)

- Site-specific Meteorological (Temperature & Wind Speed) Data were used for a Six-year Span from January 1, 1984, to January 1, 1990
- A Corresponding Calculation Was Performed and a Curve was Generated which Encompasses a Minimum of 96.1 Percent of all WNP-2 Weather Conditions
- Data Checked for Reasonableness
- The Curve Excludes Approximately Four Percent as a Conservative Approximation of 95%/5%

DATA USED (6YRS)

- Winter Cases Yielded Longer Drawdown Times than Summer Cases
- Limiting Case Very Conservative - Atmospheric Temperature of 0°F, no Wind, Standby Service Water System Spray Pond Temperature 77°F, Division 2 Electrical Power (i.e., Division 1 Not in Operation), One Train of Standby Gas Treatment System in Operation, and 50% Room Cooler Efficiency
- Case Resulted in a Drawdown Time of 711 Seconds (11.85 Minutes)

DATA USED (6YRS)

Zero Wind Speed and Zero Degrees Temperature used Because Temperature Impact on Differential Pressure is Prominent Factor, due to the Higher Differential Temperature Between Inside and Outside Temperatures

FTP
6.3

X/Q CALCULATIONS

- ARCON96

1. Description of Release Points and Control Room Intakes
2. Application of ARCON96 at WNP-2
3. Comparison with JCO-FAO and Power Uprate

X/Q CALCULATIONS

- **ARCON96**
- ARCON96 used to Determine X/Q values for Three Control Room Intakes and Four Release Points
- Utilized the Same Time Period/plant Specific Data as Used in the Drawdown Analysis
- CR Intakes – Local and Two Remote Intakes

1.000 6/2/14

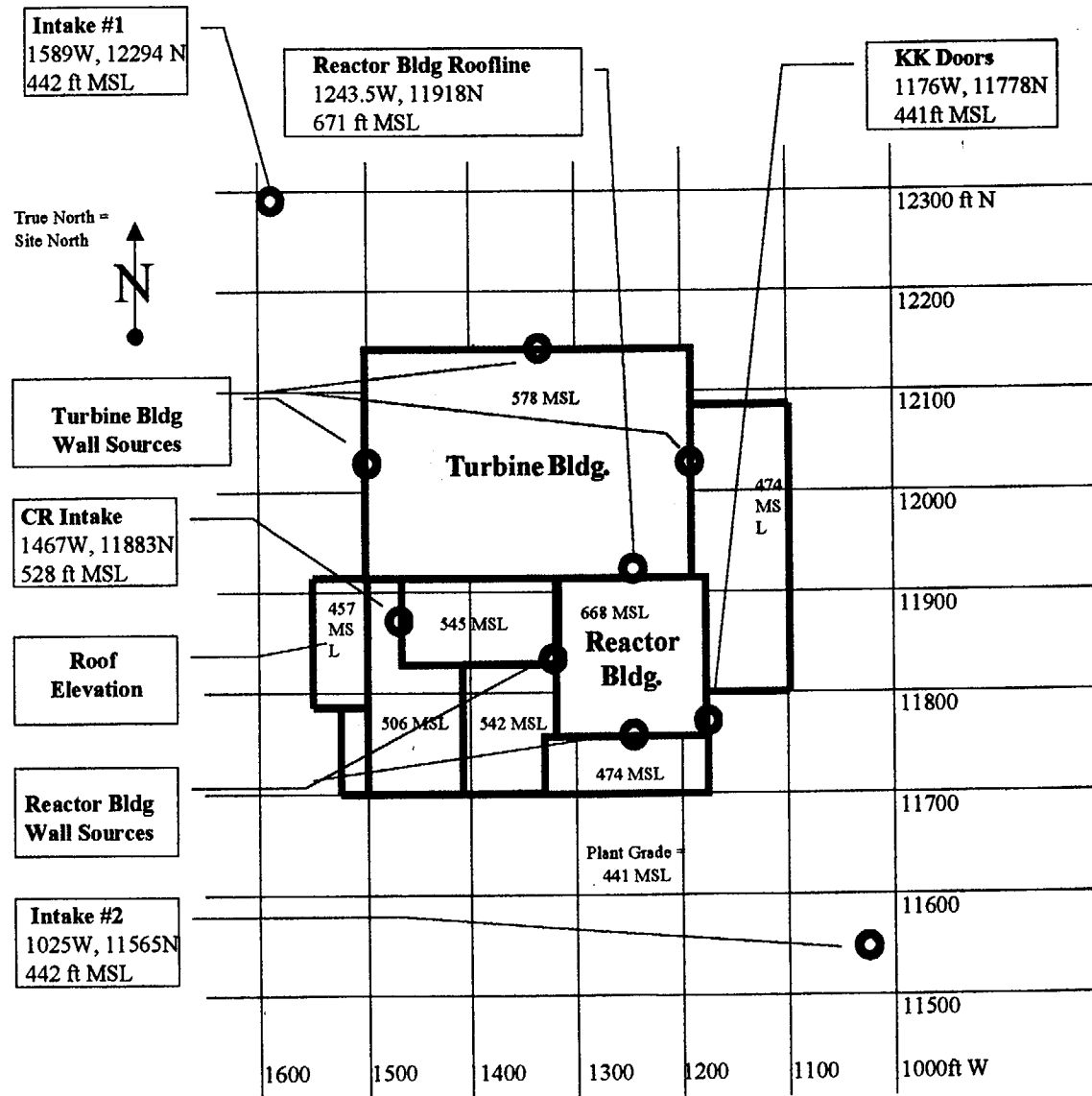
X/Q CALCULATIONS

- Release Points Considered
- **Turbine Building Walls** – Release from Turbine Building Walls to be Used with Events such as CRDAs
- **Reactor Building Walls** – Release from Reactor Building Walls to be Used During Drawdown Period and Secondary Bypass Leakage
- **Reactor Building Roofline (Stack) Release** – Vent Release from Reactor Building Roof Used for SGTS Releases
- **Reactor Building (King Kong) Doors** - Release from Reactor Building Grade Area

X/Q CALCULATIONS - ARCON96 - SITE CONFIGURATION

SEE NEXT SLIDE

X/Q Calculations - ARCON96 - Site Configuration



X/Q CALCULATIONS

- Application of ARCON96
- Analyzed each of the four Release Paths for each of the Three Intakes (i.e., 12 Scenarios)
- Analyzed all 12 Scenarios for all 6 Years
- The Maximum Value of the 6 Years was Chosen for each Time Period (i.e., not just the Maximum Year but the Maximum Value of each Time Step)
- Local Intake not Used for LOCA due to the Presence of an Automatic Isolation Signal

→ conservative
worst pt in
each time st.
of year

X/Q CALCULATIONS

- Application of ARCON96
- Between 0 to 3 Hours, no Credit for Operator Action – Used Average of the two Remote Intakes *credit is not already there for manual action*
- From 3 Hours to the 30 Days, Credit for Operator Action – Used the Lower of the two X/Qs Calculated for the Remote Intakes *Operator action in 30 day period - twice. Done in operator's control room for manual action*
- Very Conservative Treatment – With the Presence of two Remote Intakes, the Plant will be able to Switch to the Upwind Intake and in Effect Preclude the Introduction of Activity During the Accident

X/Q CALCULATIONS

SEE NEXT SLIDE

X/Q Calculations

ARCON96 Results and Comparison with Original CR X/Qs for UFSAR

| Time Period | X/Q Calculated with ARCON 96 (s/m ³) | X/Q Used for UFSAR Analysis (s/m ³) | Ratio of ARCON 96 Value to UFSAR Value |
|-----------------------|--|---|--|
| Ground Release | | | |
| 0 - 2 hr | 9.94E-5 | 2.17E-4 | 45.81% |
| 2 - 3 hr | 9.91E-5 | 5.43E-5 | 182.50% |
| 3 - 8 hr | 7.16E-5 | 4.49E-5 | 159.47% |
| 8 - 24 hr | 4.37E-5 | 3.55E-5 | 123.10% |
| 1 - 4 days | 2.35E-5 | 1.67E-5 | 140.72% |
| 4 - 30 days | 1.56E-5 | 1.67E-5 | 93.41% |
| SGTS Release | | | |
| 0 - 2 hr | 2.54E-4 | 3.77E-4 | 67.37% |
| 2 - 3 hr | 1.70E-4 | 9.43E-5 | 180.28% |
| 3 - 8 hr | 8.15E-5 | 7.80E-5 | 104.49% |
| 8 - 24 hr | 3.20E-5 | 6.17E-5 | 51.86% |
| 1 - 4 days | 2.26E-5 | 2.90E-5 | 77.93% |
| 4 - 30 days | 1.90E-5 | 2.90E-5 | 65.52% |

DOSE ANALYSIS AND RESULTS

- Accidents Analyzed for Radiological Consequences
- AXIDENT Code
 1. How Applied
 2. Where used Before
- Summary of LOCA Major Assumptions
- Changes from Original Design and Previous Submittal
- LOCA Results

Bruce Forsgren

ACCIDENTS ANALYZED

- Main Steam Line Break (MSLB)
- Fuel Handling Accident (FHA)
- Control Rod Drop Accident (CRDA)
- Loss Of Coolant Accident (LOCA)

AXIDENT CODE

Dave Stalley Scientist

- **Dose Analysis Code** – Radiological Consequences of the Spectrum of Design Basis Accidents were Analyzed using the SCIENTECH-NUS AXIDENT Code
- **Code Description** - AXIDENT Models the Transport of Radioactivity to the Environment and to the Control Room. This Code Includes the time Dependent Effects of Containment Sprays, Recirculation, Purge and Intake Filters, Atmospheric Dispersion, Natural Decay, etc. The Code is Based on the Explicit Solution of the Integrated Activity in a Receptor Volume.

AXIDENT CODE

- **Industry Experience/Usage of the AXIDENT Code –**
- Developed in the early 70's to Support the Licensing and Licensing Reviews of both U.S. and International Commercial Nuclear Power Plants. Developed to fill the Void in Codes Available to Assess the Emerging Issue at the time – Control Room Habitability.
- General Industry Usage
 - Used to Support Licensing Submittals in the 70's
 - Used for a Number of Plants in Support of the Post-TMI Action Item
 - Used Throughout the 80's and 90's to Resolve Control Room Habitability and Accident Analyses Issues

AXIDENT CODE

SCIENTECH Experience

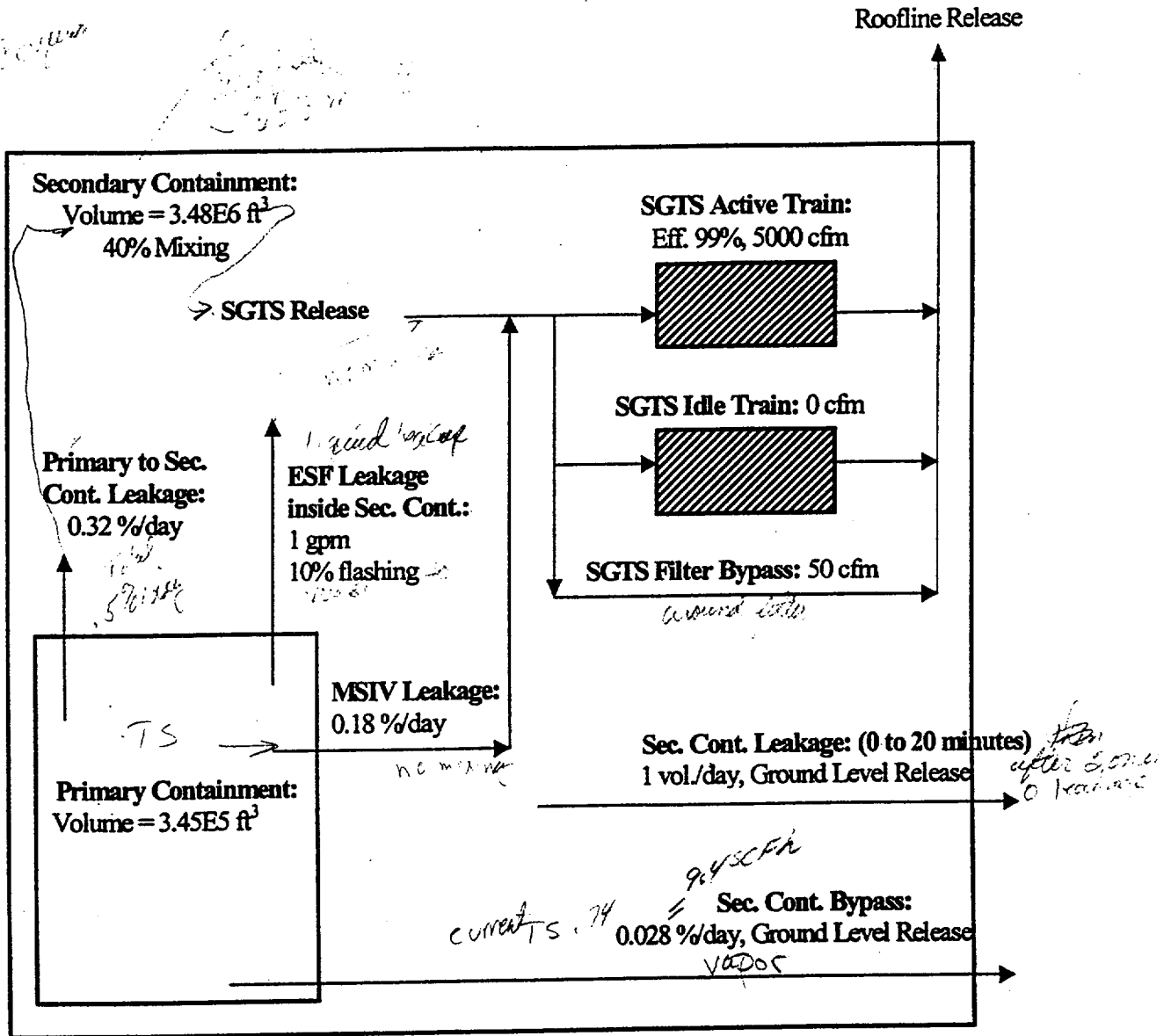
- Successfully Benchmarked the Previous Results Generated by other Codes which Compute the Integrated/exact Solution (i.e., Bechtel's LOCADOSE and S&L's PostDBA)
- Over the Years, Thousands of Cases have been run on the AXIDENT Code. In all Cases, the Results have Trended as Expected. The Results have also Consistently been in Close Agreement with the Steady State Murphy/Campe Equations.

AXIDENT CODE

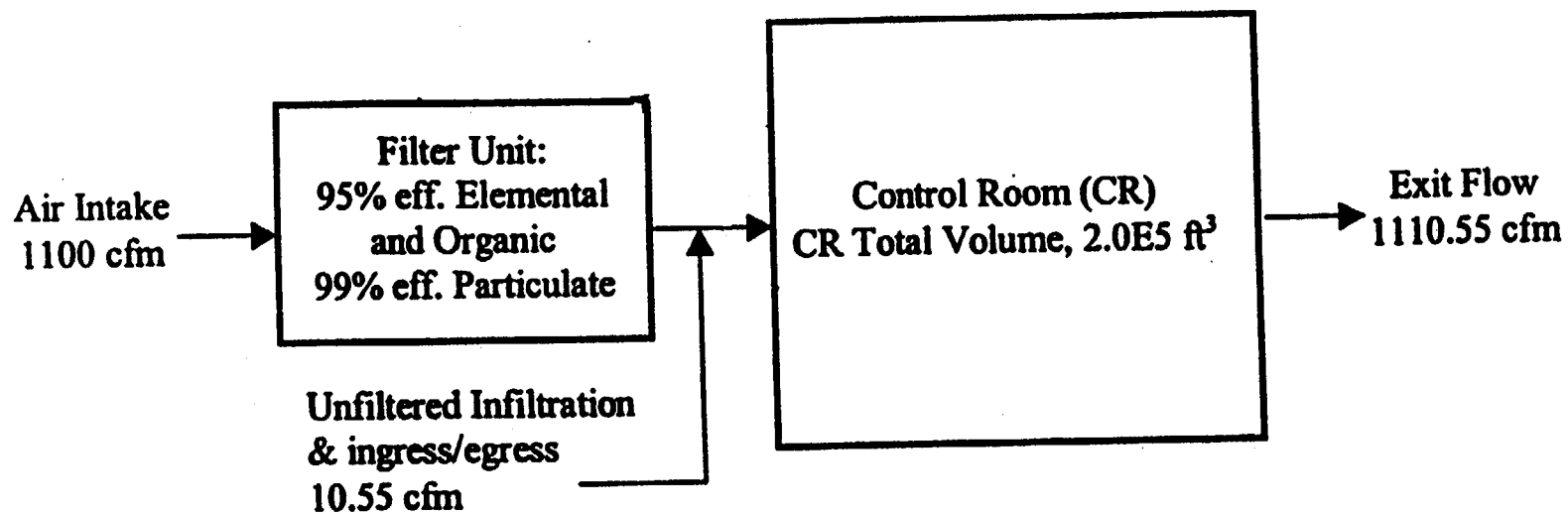
Recent Calculations Submitted to the NRC Include:

- Control Room and Offsite Dose Calculations to Support the FPC Crystal River Restart
- CRDA and MSLB Analyses for the CP&L Brunswick Station's Power Uprate Effort
- Reanalysis Effort for the Cooper Station – Pending Review

RELEASE PATHWAYS



CONTROL ROOM AIR FLOWS



MAJOR ASSUMPTIONS

Base

- AXIDENT Code used for Dose Analysis
- Source Term Release Per TID-14844 (102% Power Level)
 - 100 % Noble Gases
 - 25 % Halogens (50% ESF Leakage)
 - 91% Elemental
 - 5 % Particulate
 - 4 % Organic
- Dose Conversion Factors in Accordance with ICRP 30

MAJOR ASSUMPTIONS

Bruce Boyer

- Instantaneous Mixing in Primary Containment
- Release from Containment of .5%/day Total
 - .32%/day Containment Leakage
 - .18%/day MSIV Leakage
- No Suppression Pool Scrubbing Credited

MAJOR ASSUMPTIONS

- SGT Filter Efficiency
 - 99% Efficient for Halogens
 - 0 % Efficient for Noble Gases
- SGT Flow:
 - 5000 cfm Single Train
 - 50 cfm Bypass Leakage
- Control Room Filter Efficiency
 - 95% Efficient for Elemental and Organic Iodine
 - 99% Efficient for Particulate Iodine

MAJOR ASSUMPTIONS

- Secondary Containment Drawdown Time of 20 Minutes
- During Drawdown Time:
 - No SGT Filtration Credited
 - Secondary Containment Leakage at a Rate of 1 Volume/day
- 40% Mixing in Secondary Containment for Entire Scenario

MAJOR ASSUMPTIONS

- ESF Leakage Into Secondary Containment:
 - 1 gpm
 - 10% Flashing Fraction
 - 50% Core Iodine Source Term
- Control Room Unfiltered Inleakage:
 - 10 scfm Ingress/egress
 - .55 scfm Infiltration
- Secondary Containment Bypass Leakage of .028%/day (9.4 scfh)
- New X/Q Values

DOSE ANALYSIS METHODOLOGY MAJOR CHANGES

| <u>ITEM</u> | <u>CURRENT DESIGN</u> | <u>PREVIOUS SUBMITTAL</u> | <u>PROPOSED DESIGN</u> |
|---------------------------|---------------------------|-------------------------------|----------------------------|
| Drawdown Time | 5 Min | 20 Min | 20 Min |
| Sec. Ctmt Mixing | None | 40% Vol. | 40% Vol. |
| ESF Leakage | --- | None | 1 GPM |
| SGT Filter Bypass | 14 cfm | 14 cfm | 50 cfm |
| Bypass Leakage (% Day) | .00209 174 | .054* 1895 | .028 94 |

LOCA ANALYSIS RESULTS

| | CALC. <u>(REM)</u> | LIMIT <u>(REM)</u> |
|----------------|-----------------------|-----------------------|
| CR Whole Body | 0.4 | 5 |
| CR Thyroid | 28.1 | 30 |
| CR Beta | 6.8 | 30 |
| EAB Whole Body | 3.7 | 25 |
| EAB Thyroid | 56.6 | 300 |
| LPZ Whole Body | 3.4 | 25 |
| LPZ Thyroid | 131 | 300 |

LOCA DOSE BY PATH

| RELEASE PATH | <u>CONTROL ROOM</u> <u>THYROID</u> | <u>ROOM</u> <u>W. BODY</u> | <u>LPZ</u> <u>THYROID</u> | <u>W.BODY</u> |
|----------------------|---------------------------------------|-------------------------------|------------------------------|---------------|
| Sec. Ctmt Bypass | 21 | .02 | 101 | 0.5 |
| Sec. Ctmt Leakage | .02 | 8E-5 | 0.2 | 4E-3 |
| Sec. Ctmt SGT Rel. | 4.2 | .16 | 16 | 1.2 |
| ESF Leakage Sec.Ctmt | 0.3 | 1E-5 | 1.2 | 2E-3 |
| MSIV Leakage | 3.0 | .18 | 13 | 1.7 |
| TOTAL | 28.1 | 0.4 | 131 | 3.4 |

CONTAINMENT RELEASE IMPACT

(.04%/day Sec Ctmt Bypass Leakage)

| RELEASE PATH | CR THYROID DOSE (REM) | |
|---------------------|-----------------------|----------------|
| | <u>.32%/DAY</u> | <u>.5%/DAY</u> |
| Sec Ctmt Bypass | 29 | 29 |
| Sec Ctmt Leakage | .02 | .03 |
| Sec Ctmt SGT Rel. | 4.2 | 6.5 |
| ESF Leak (Sec Ctmt) | 0.3 | 0.3 |
| MSIV Leakage | 3.0 | 3.0 |
| TOTAL | 36.9 | 39.2 |

EFFECT OF RELEASE ELEVATION

| DESCRIPTION | <u>DOSE (REM)</u> |
|--|-------------------|
| Ground Release = 100% Roofline Release = 0% | 39.2 |
| Ground Release = 60% Roofline Release = 40% | 39.6 |
| Ground Release = 50% Roofline Release = 50% | 39.7 |
| Ground Release = 0% Roofline Release = 100% | 39.2 |
| • Based on Thyroid Dose in Control Room Assuming .5%/day Containment Leakage and .04%/day Secondary Containment Bypass | |

EFFECT OF SGT FLOWRATE

| <u>DESCRIPTION</u> | <u>DOSE (REM)</u> | |
|---|-------------------|---------------|
| | <u>THYROID</u> | <u>W.BODY</u> |
| 4K cfm for 30 Days | 37.3 | .357 |
| 5K cfm for 30 Days | 36.9 | .369 |
| 10K cfm for 30 Days (20 Min Drawdn) | 37.3 | .409 |
| 10K cfm for 30 Days (10 Min Drawdn) | 37.3 | .409 |
| 10K cfm for 1 Hr Then 4K cfm 30 Days | 37.3 | .362 |

Based On .32%/day Ctmt Leakage and .04%/day Sec Ctmt Bypass
Leakage

SUMMARY

- Dose Analysis Meets 10CFR50 and 10CFR100 Limits
- No Hardware Changes Necessary Beyond Those Completed in Support of the JCO-FAO
- Tech Spec Submittal to be Made in February
- FSAR Changes will be Implemented Following Approval of Tech Spec Submittal
- FSAR Changes Include:
 - Accident Analysis and Doses
 - Control Room Habitability Analysis
 - Secondary Containment Description
 - Description of SGTS and REA
- JCO-FAO will be Closed Following Approval of Tech Spec Submittal